



Consiglio Nazionale delle Ricerche

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Investigation by optical techniques of the effect of hydrogen addition in rich premixed ethylene-air flames

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Aim of the work

effects of hydrogen addition on:

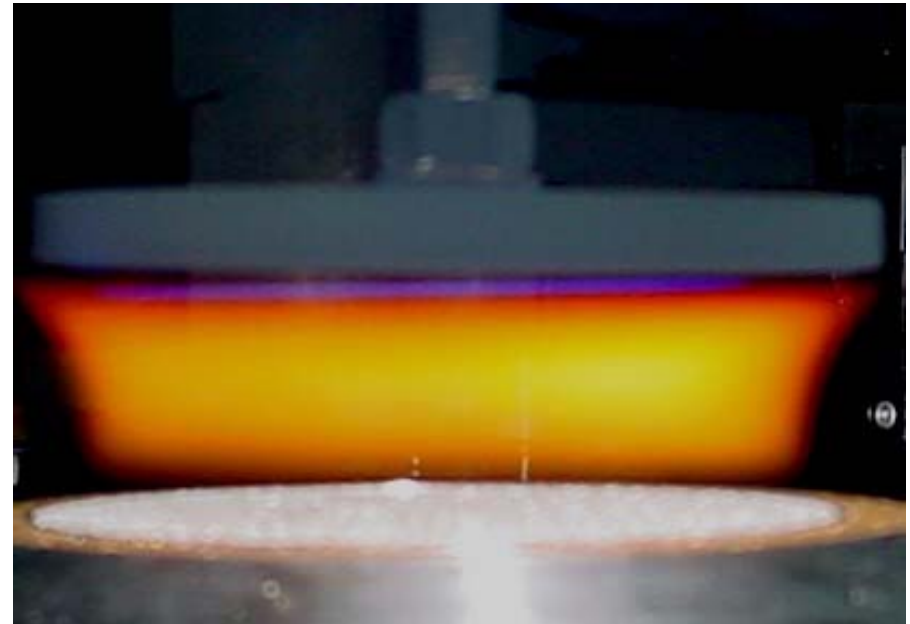
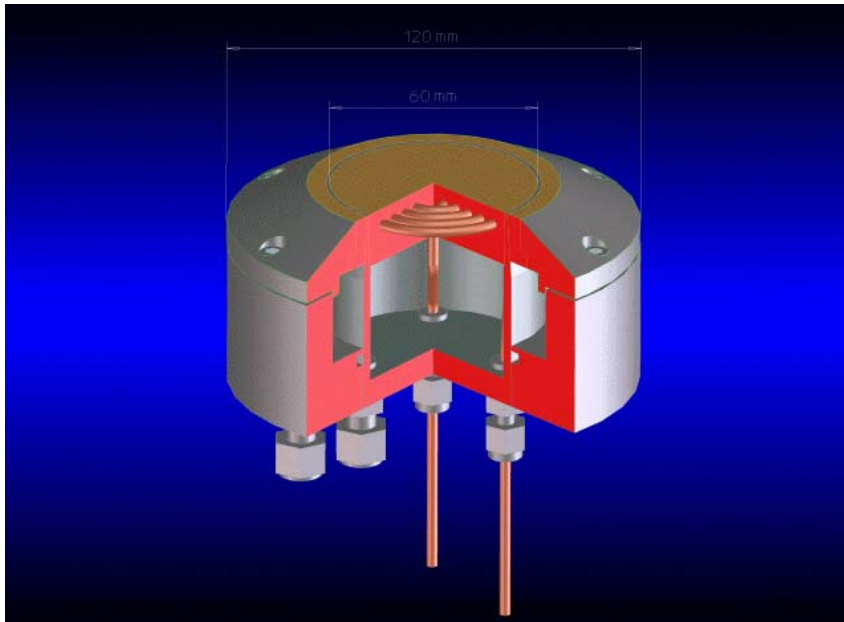
- ✓ **Flame Structure**
- ✓ **Gas Temperature**
- ✓ **Soot content**



Laminar premixed flat flames

McKenna burner

- Bronze porous plug : $\phi = 60 \text{ mm}$
- Co-annular porous bronze ring : $s = 6 \text{ mm}$
- Stabilization plate: $\phi = 60 \text{ mm}$, $H_{AB} = 20 \text{ mm}$





Flame conditions

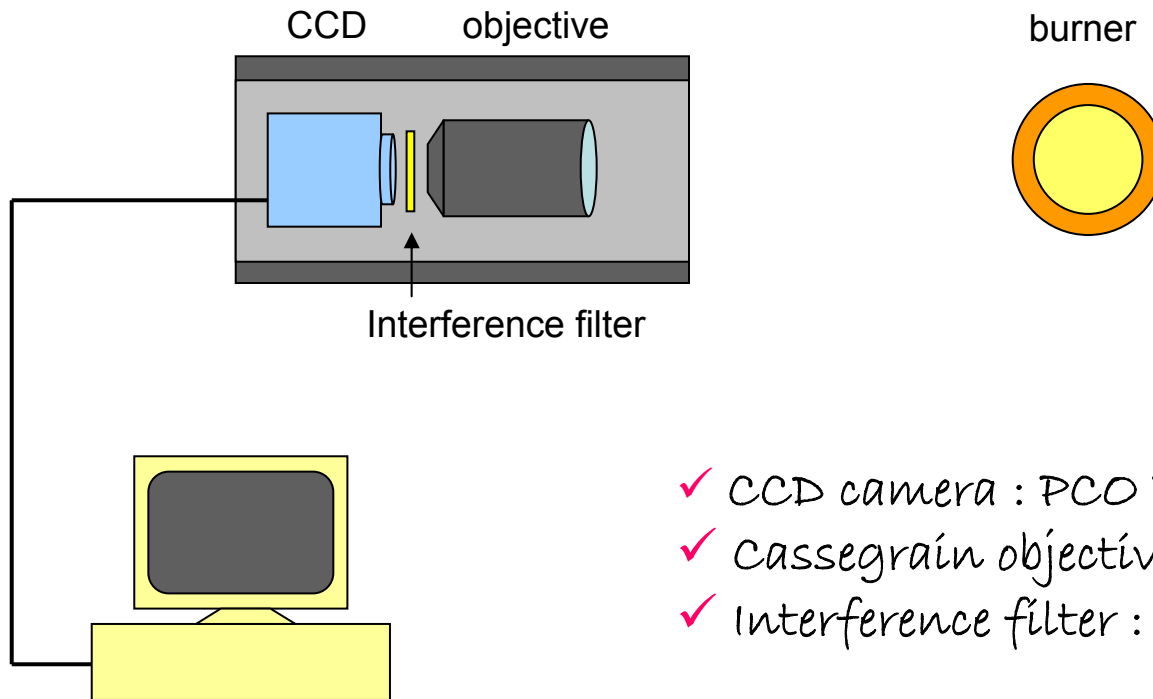
- ✓ total flow rate = 10 l/min
 - ✓ cold gas flow velocities = 5.84 cm/s
 - ✓ C/O ratio = 0.775
- } constant !!!

$\phi = 2.34$ ←

flame	C ₂ H ₄ [l/min]	H ₂ [l/min]	H ₂ /C ₂ H ₄ *100	Air [l/min]	Φ global
A	1.400	0	0	8.60	2.34
B	1.380	0.138	10	8.46	2.425
C	1.360	0.272	20	8.34	2.528
D	1.346	0.404	30	8.25	2.639
E	1.328	0.531	40	8.14	2.761
F	1.310	0.655	50	8.03	2.895

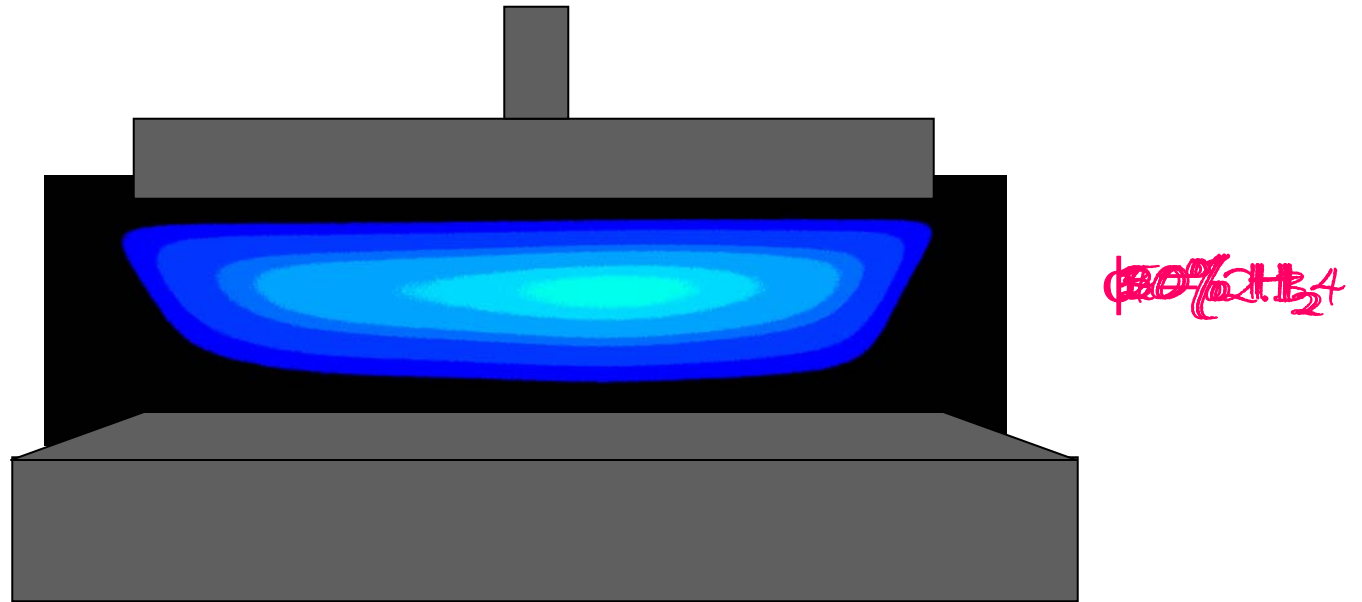
1. Flames Structure

Flames light emission measurements



- ✓ CCD camera : PCO Pixelfly, 12 bit
- ✓ Cassegrain objective : Nikon, 500 mm
- ✓ Interference filter : 647 nm, $\Delta\lambda = 10$ nm

Typical images of the flame emission



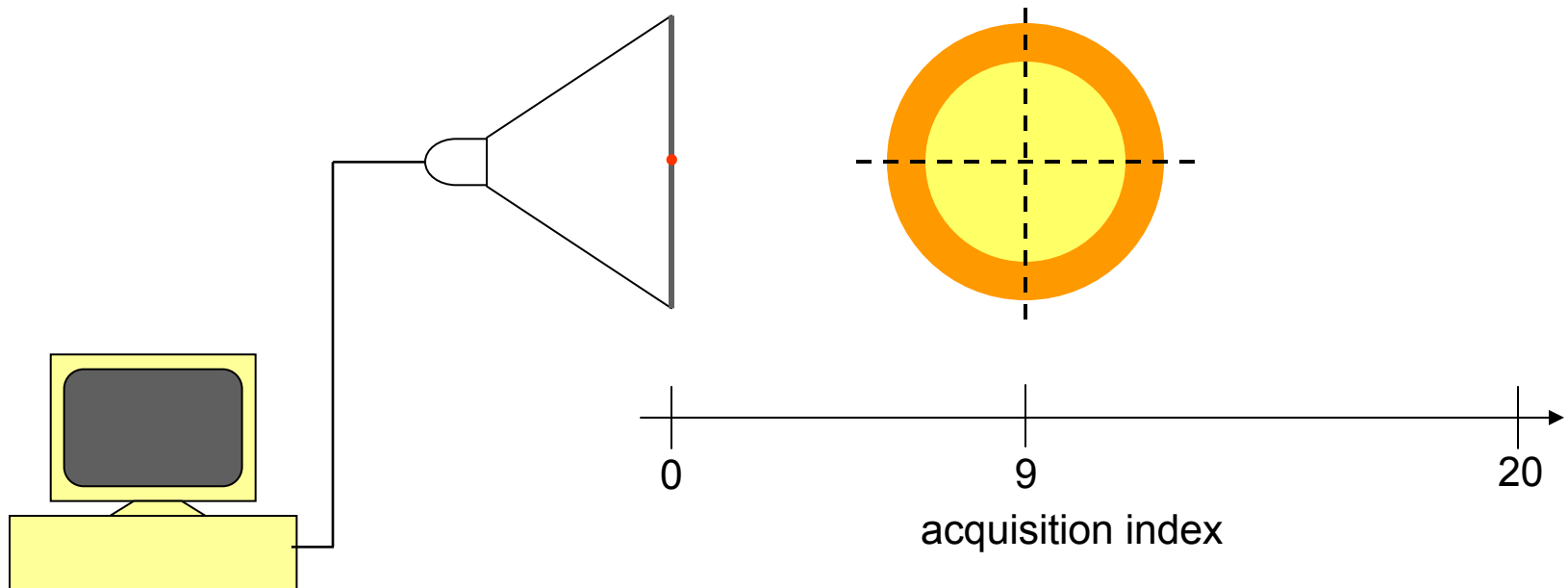
- ✓ quite uniform distribution of flames emission
- ✓ decrease of the emission intensity increasing the hydrogen content.

2. Gas Temperature

Thermocouple measurements

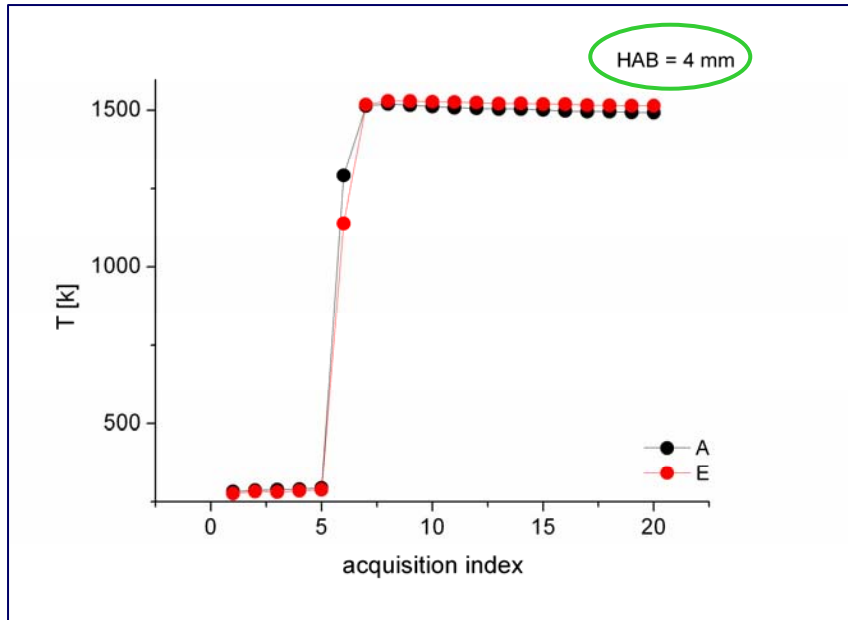
Pt/Pt-Rh(10%) : $d = 127\ \mu\text{m}$, uncoated (fork)

Pt/Pt-Rh(10%) : $d = 50\ \mu\text{m}$, uncoated (in alumina tubing)

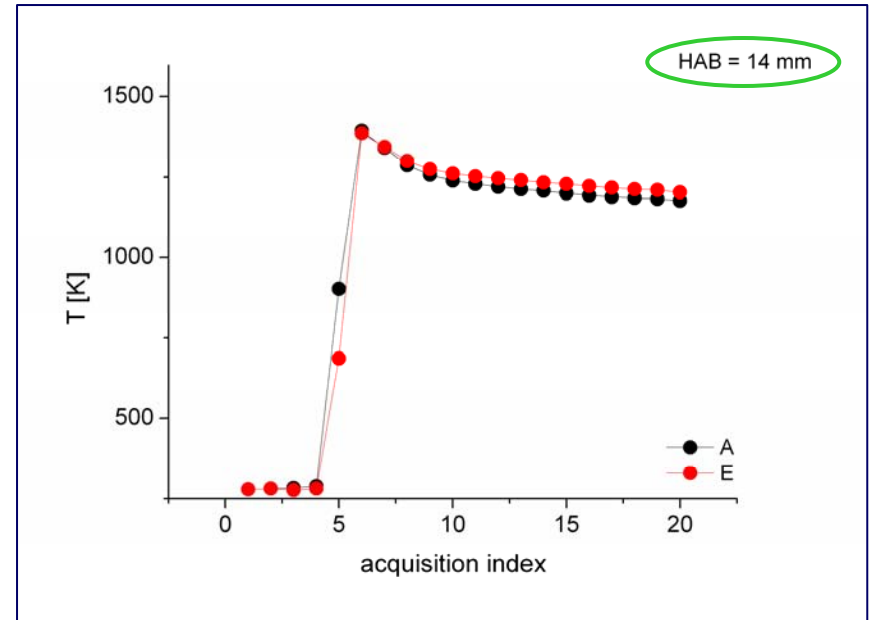




Temperature history of the junction (uncorrected, raw data)



"clean zone"



"sooting zone"

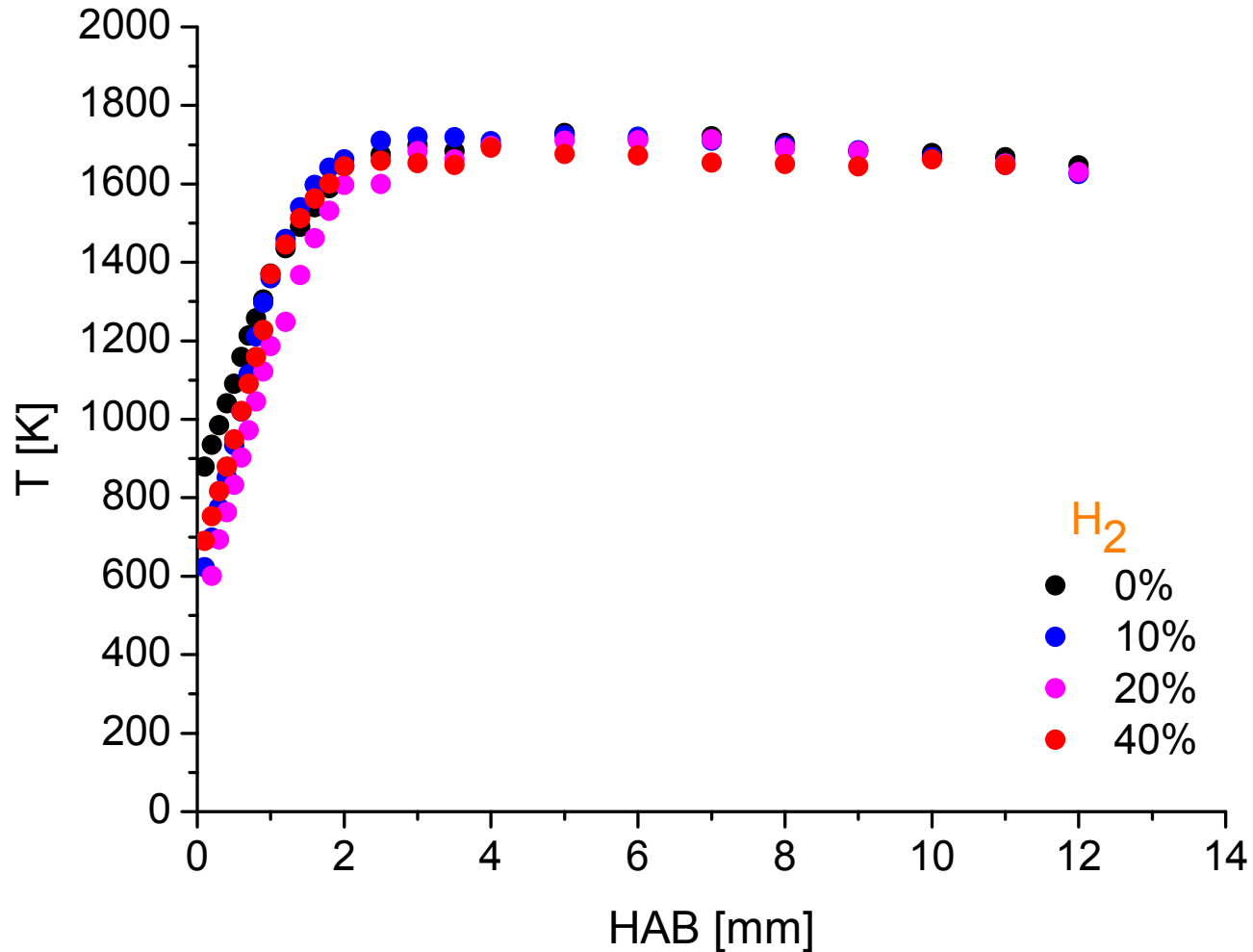
The temperature decrease continuously as soot deposits on the junction



Temperature axial profiles

Pt-Pt/10% Rh : $d_{\text{giunto}} = 50\mu\text{m}$

Correction for radiative losses



Emission technique

✓ Radiation emission from soot

$$I_s = \varepsilon_s(\lambda, f_v) I_{BB}(\lambda, T_s) \tau_{s\lambda}$$

detection efficiency
coefficient can be determined
with a calibrated lamp

$$\varepsilon_s(\lambda, f_v) = 1 - \exp(-K_{abs} L)$$

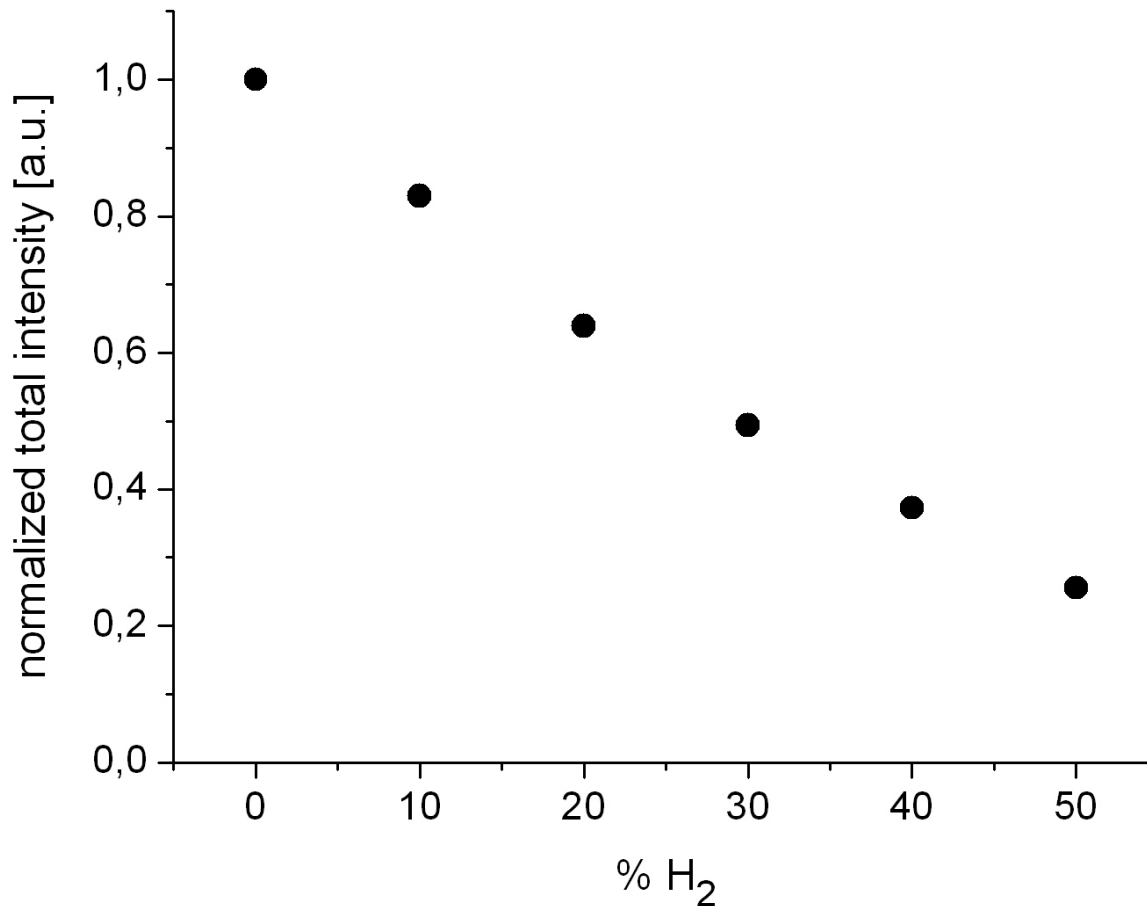
$$K_{abs} = \frac{f_v 6\pi E(m)}{\lambda} = f_v l_{abs}$$

$$\text{If } T_s \text{ without H}_2 \approx T_s \text{ with H}_2 \quad \Rightarrow \quad I_s \div f_v$$

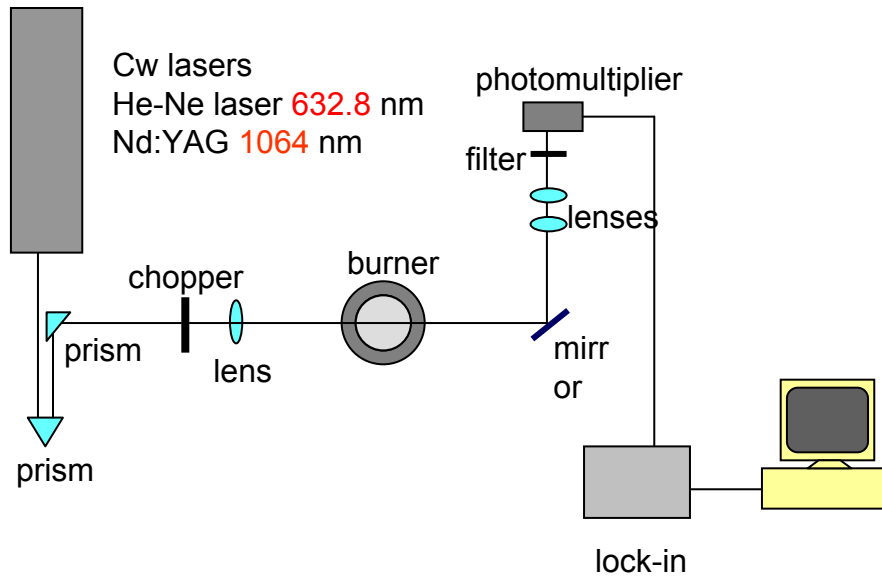
$$\int_V I_s \approx \int_V f_v = \text{total amount of soot}$$



soot reduction by hydrogen addition



Laser Extinction



easy technique, allowing to derive f_v in practical complex system, but it is line-of-sight.



Attention to the wavelength used has to be taken: contribution of other gas-phase species to absorption is possible.

$$\tau_{\lambda} = \ln\left(\frac{I_L}{I_0}\right) = -K_{ext}L$$

$$f_v = \frac{\lambda K_{ext}}{6\pi E(m)}$$

dep. on the refractive index

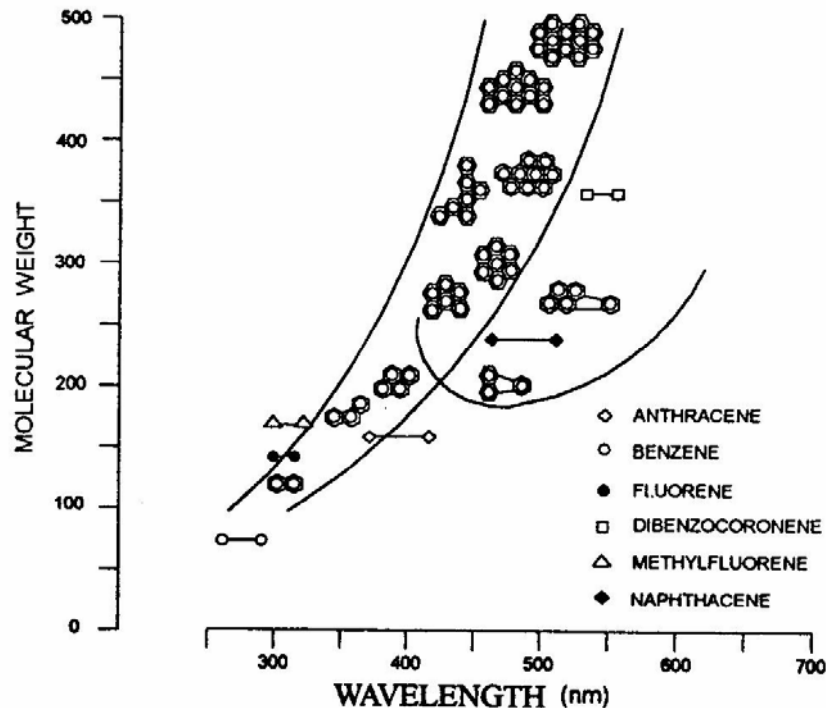


Most of the extinction measurements performed in the past with:

$\lambda = 488 \text{ nm}$ (Ar⁺ laser)

$\lambda = 632.8 \text{ nm}$ (He-Ne laser)

Can be affected by the contribution to absorption from gas phase species, such as PAH's, or other species



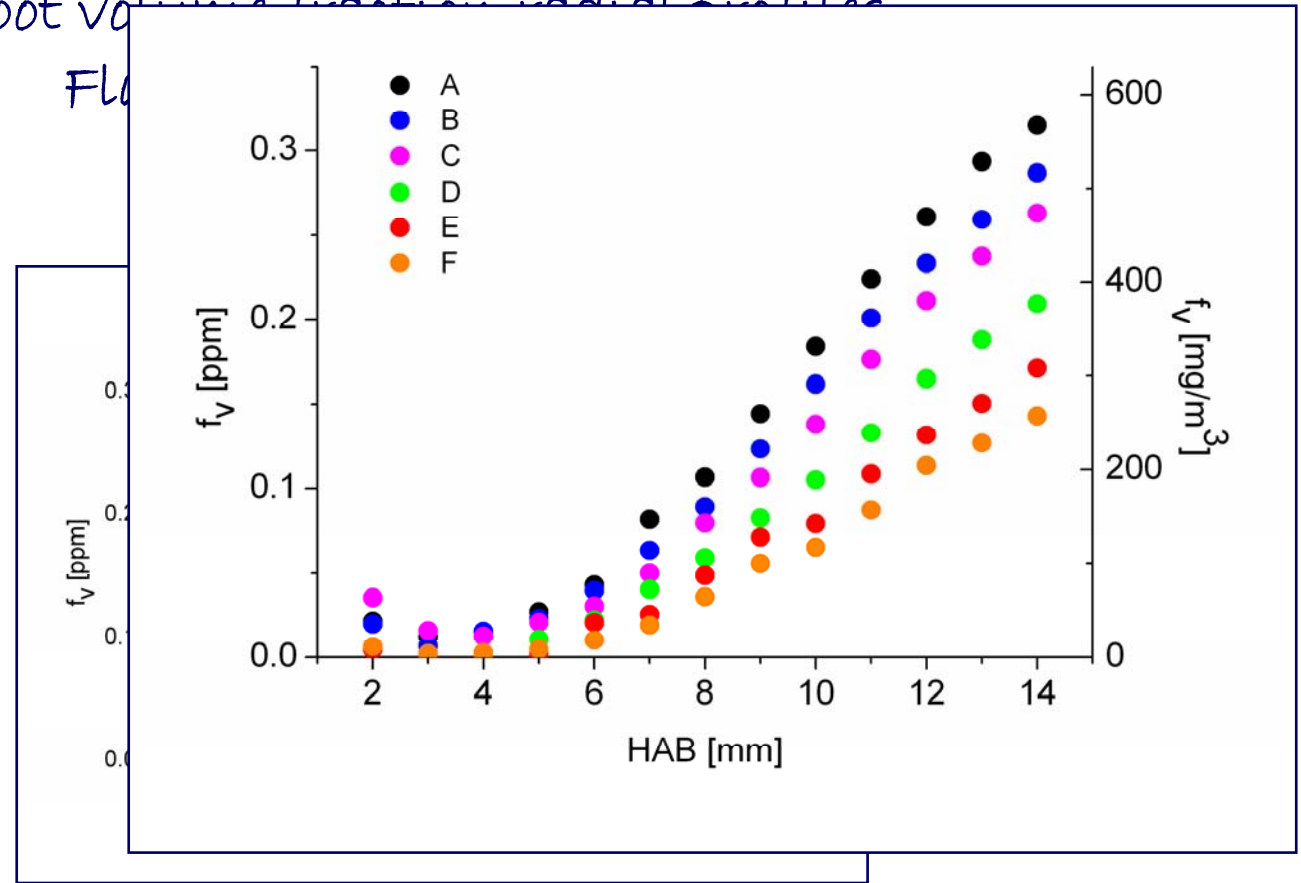
If YES \Rightarrow f_v is overpredicted



We have used also the 1064 nm laser line

Soot volume fraction ($\lambda = 632.8 \text{ nm}$)

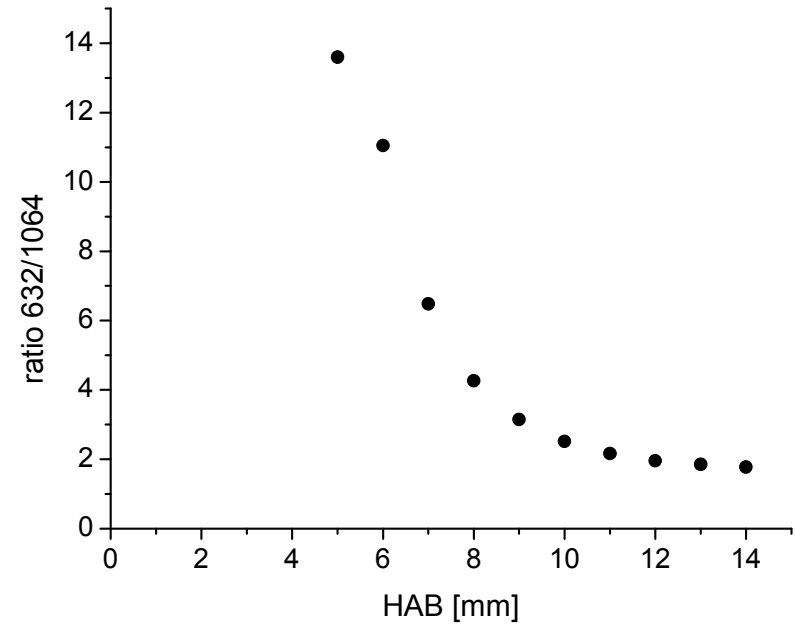
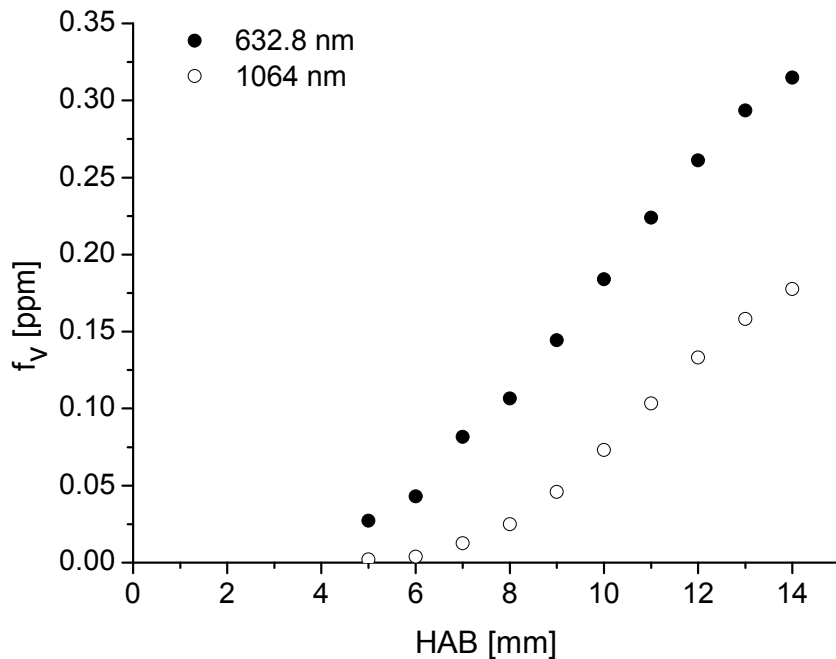
Soot volume fraction radial profiles



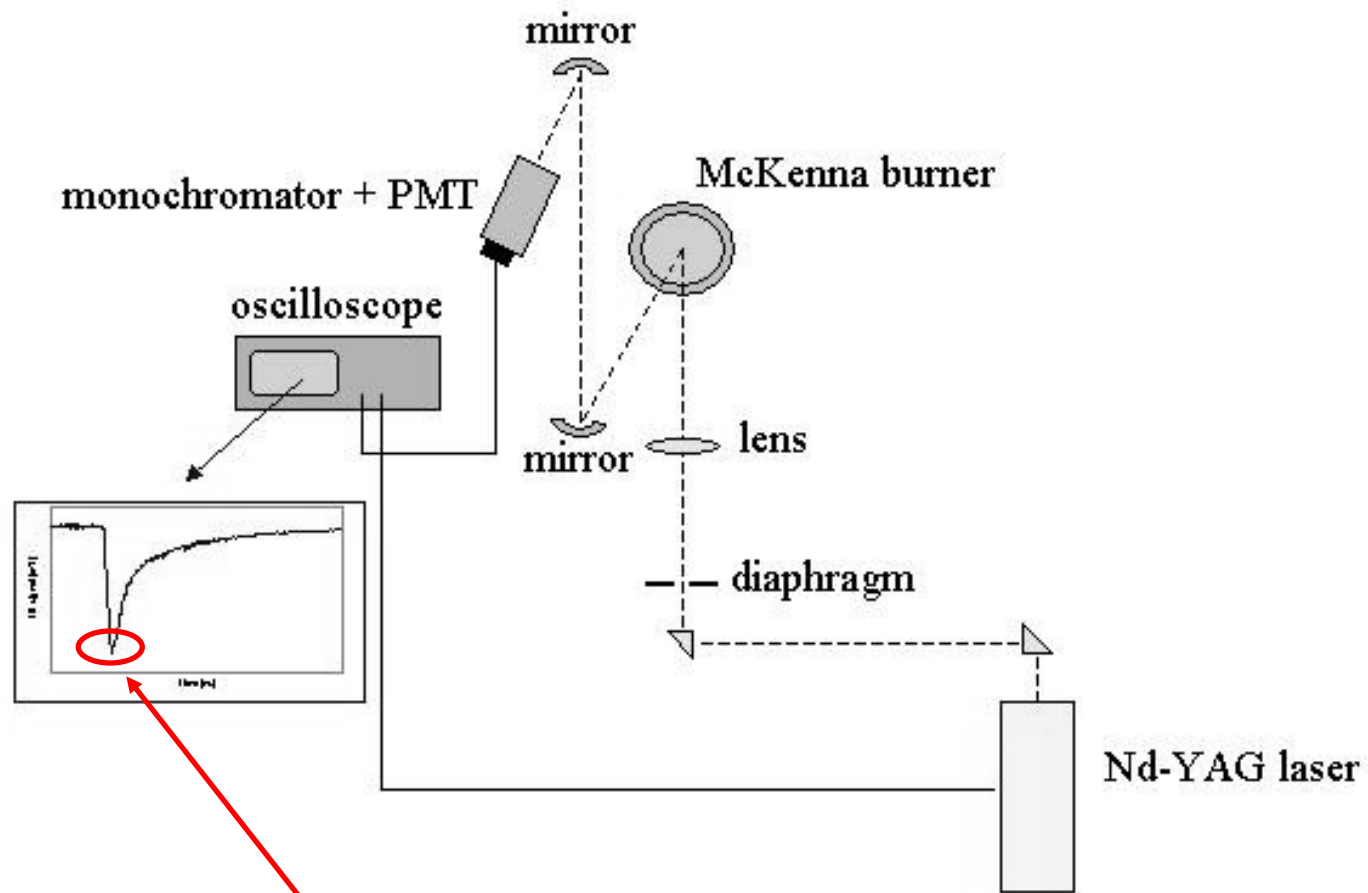
Soot volume fraction axial profiles for all the flames



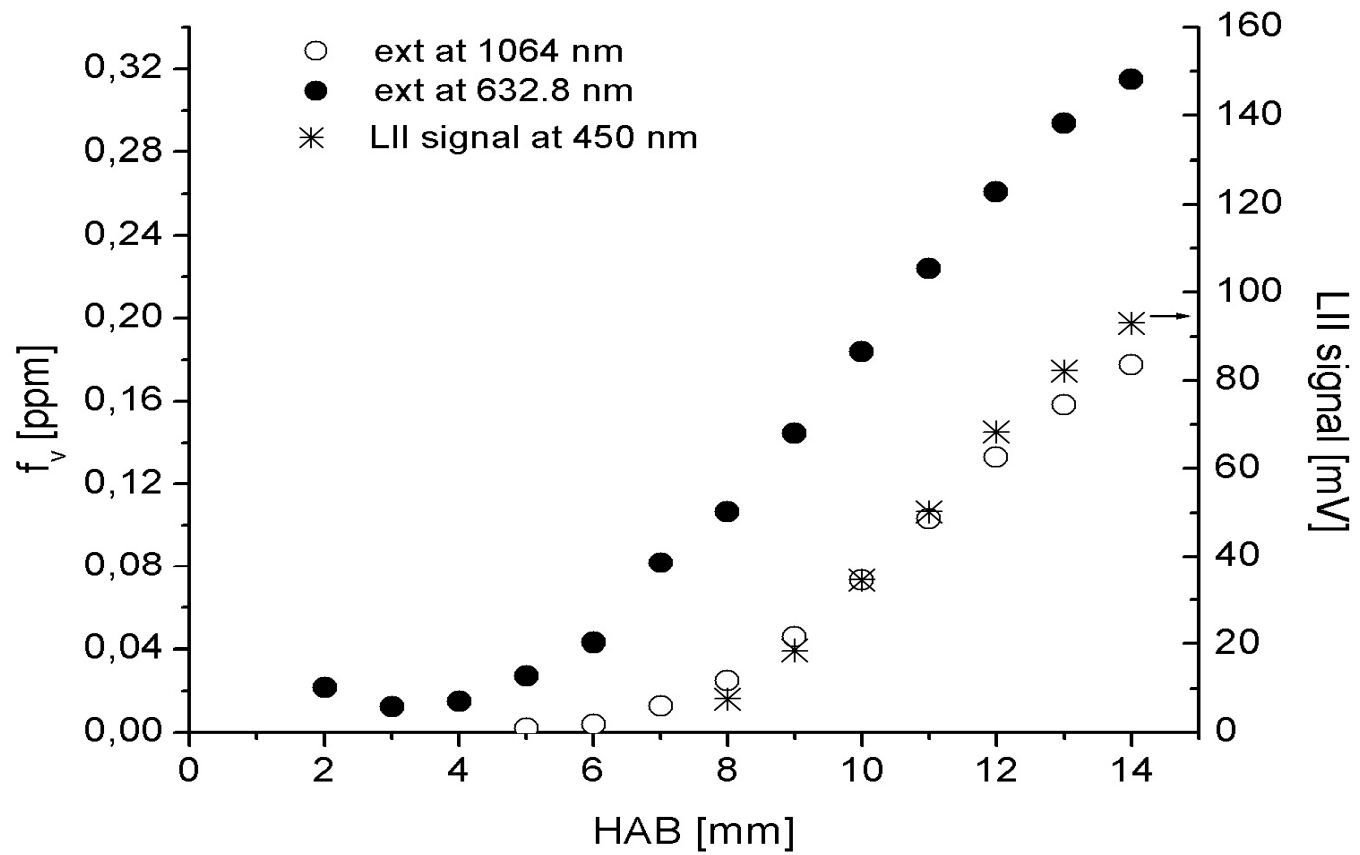
Comparison of results obtained with red or IR laser (ethylene/air: $\Phi = 2.34$)



Laser Induced Incandescence (LII)

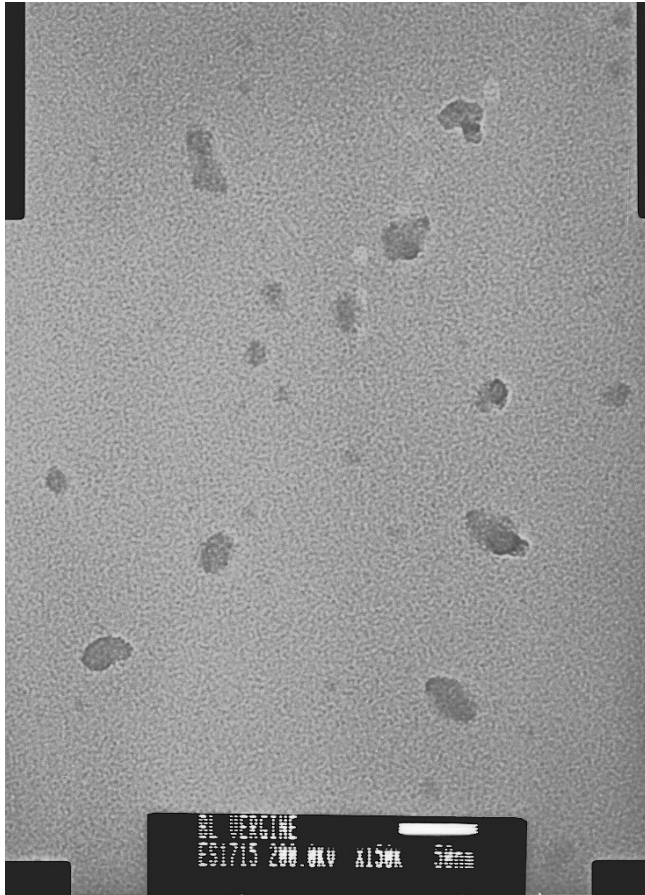


From Melton: **prompt (LII) $\propto N_p dp^x \approx f_v$**
 where $x = 3 + 154 \text{ nm}/\lambda_{\text{det}}$ \Rightarrow is LII signal dependent on dp ?

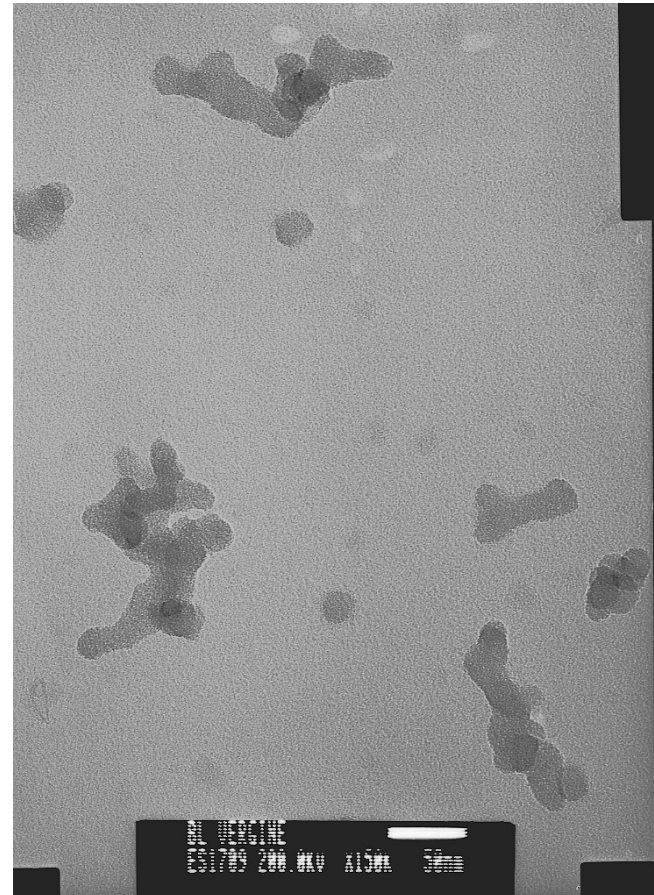


McKenna burner

Thermophoretic sampling and TEM imaging



10 mm

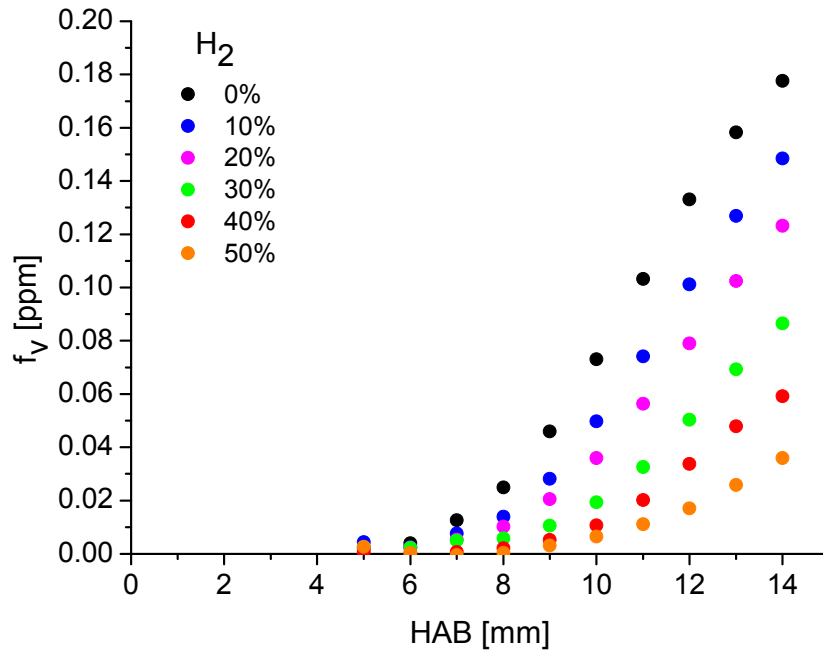


14 mm

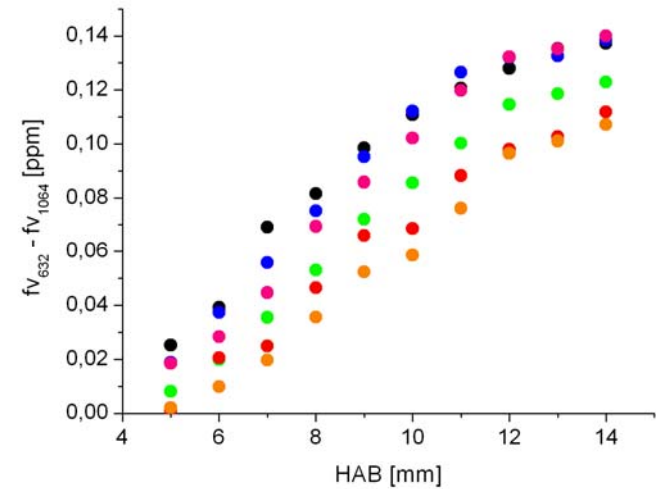


Effects of H_2 addition

Soot volume fraction
($\lambda = 1064 \text{ nm}$)



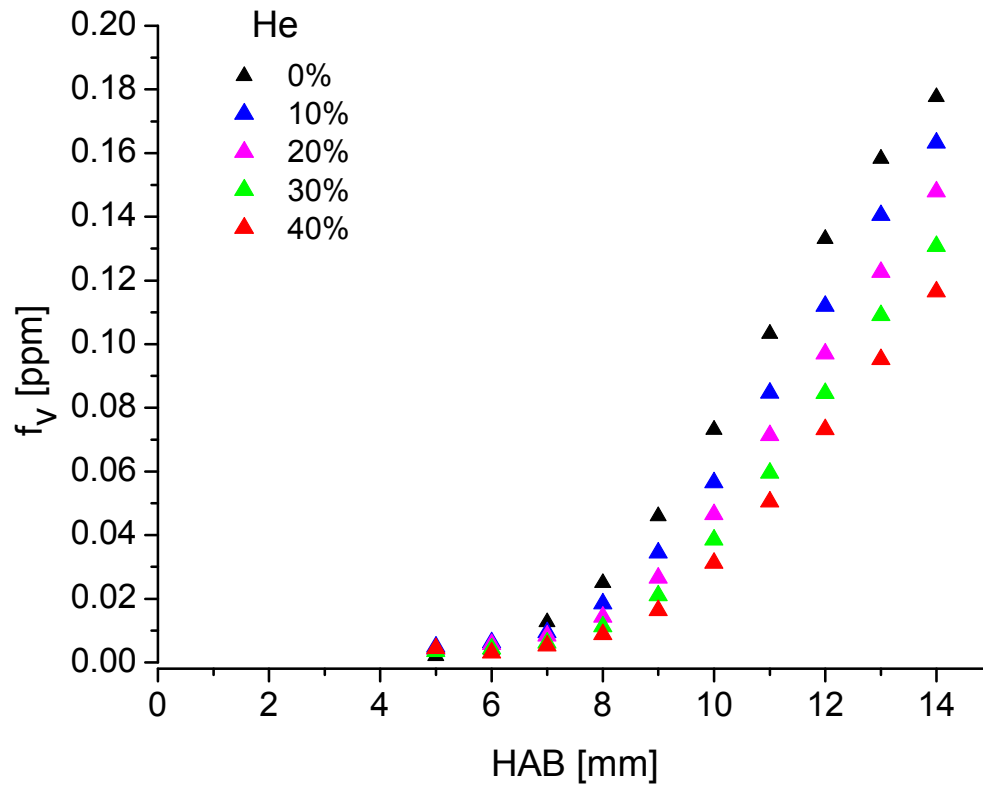
$\Delta f_{v_{632}} - \Delta f_{v_{1064}}$





Effects of He addition

Soot volume fraction
($\lambda = 1064 \text{ nm}$)





Criterion to compare different flames

Total soot load content

Thanks to the flat structure of the flame (regular radial profiles), it is possible to estimate the total soot content for each flame, starting from the corresponding axial profile.

$$\text{Soot load} = \rho_{\text{soot}} \cdot \sum_{HAB=2}^{14} f_v(HAB) \cdot \underbrace{\pi \cdot \left(\frac{L(HAB)}{2} \right)^2 \cdot \Delta HAB}_{\text{Volume}}$$

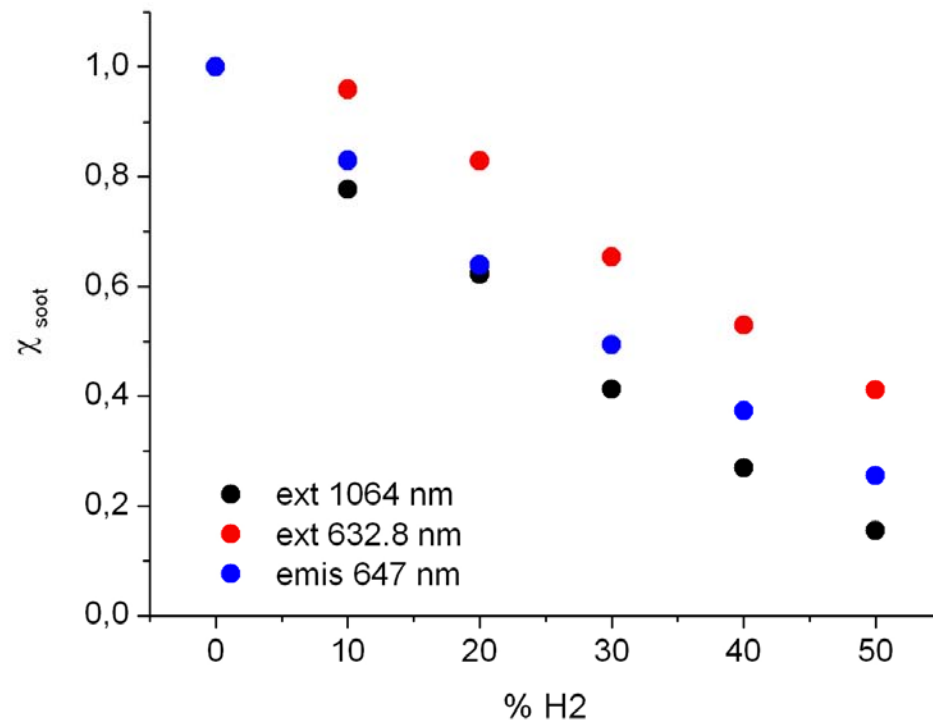
Volume
↓

L (HAB)= flame diameter

As the amount of soot is directly correlated to the amount of C atoms present in the flame, this aspect must be considered to discuss the effect of H_2 on soot production.

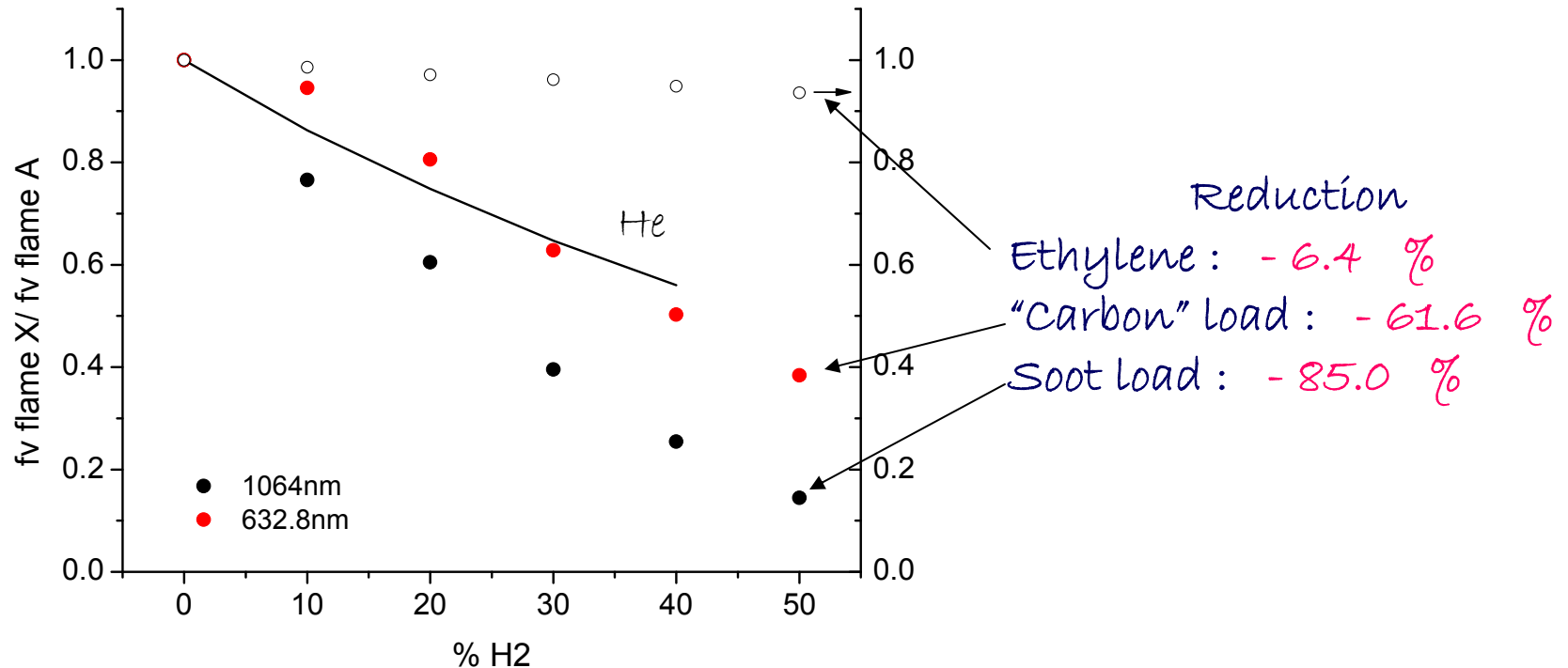
Influence of H_2 addition on the total soot load

Results and Comparison between techniques





Total soot load

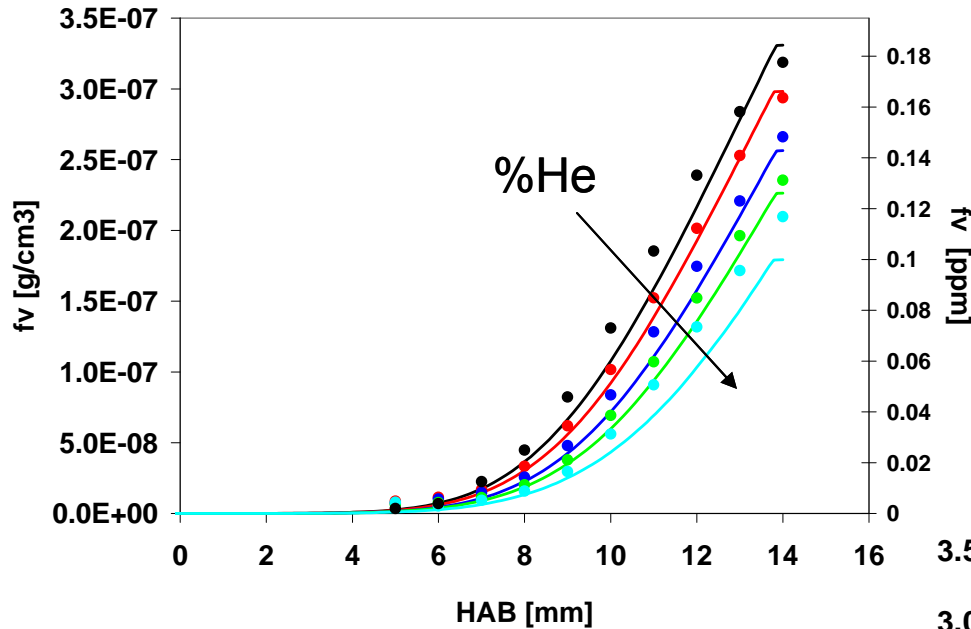


The addition of H₂ causes a decrease in soot load much higher than the decrease in ethylene fraction.



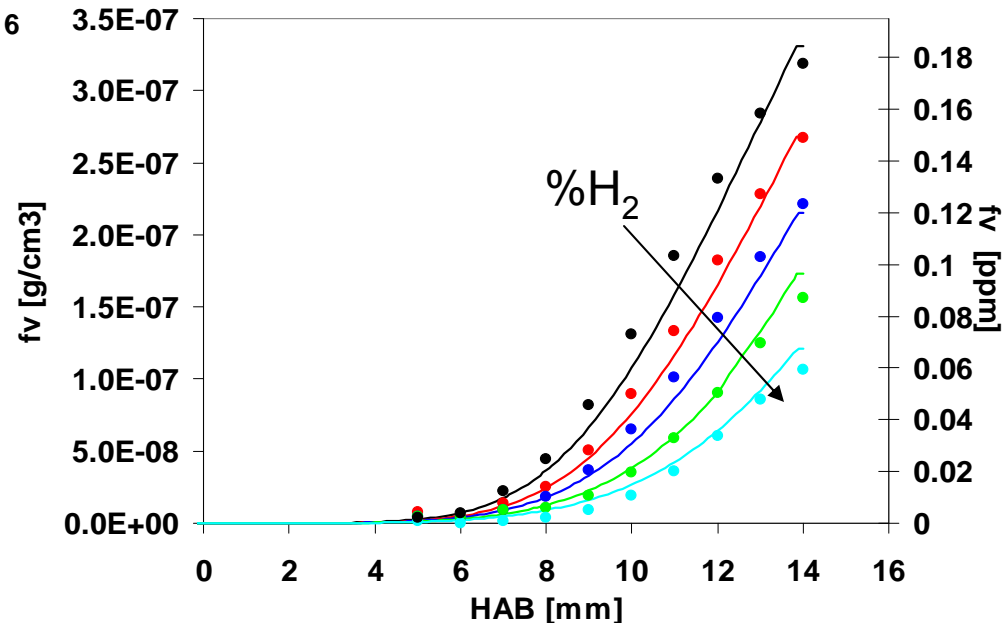
LAMINAR PREMIXED FLAMES -

Comparison with model (M. Sirignano, A. D'Anna)



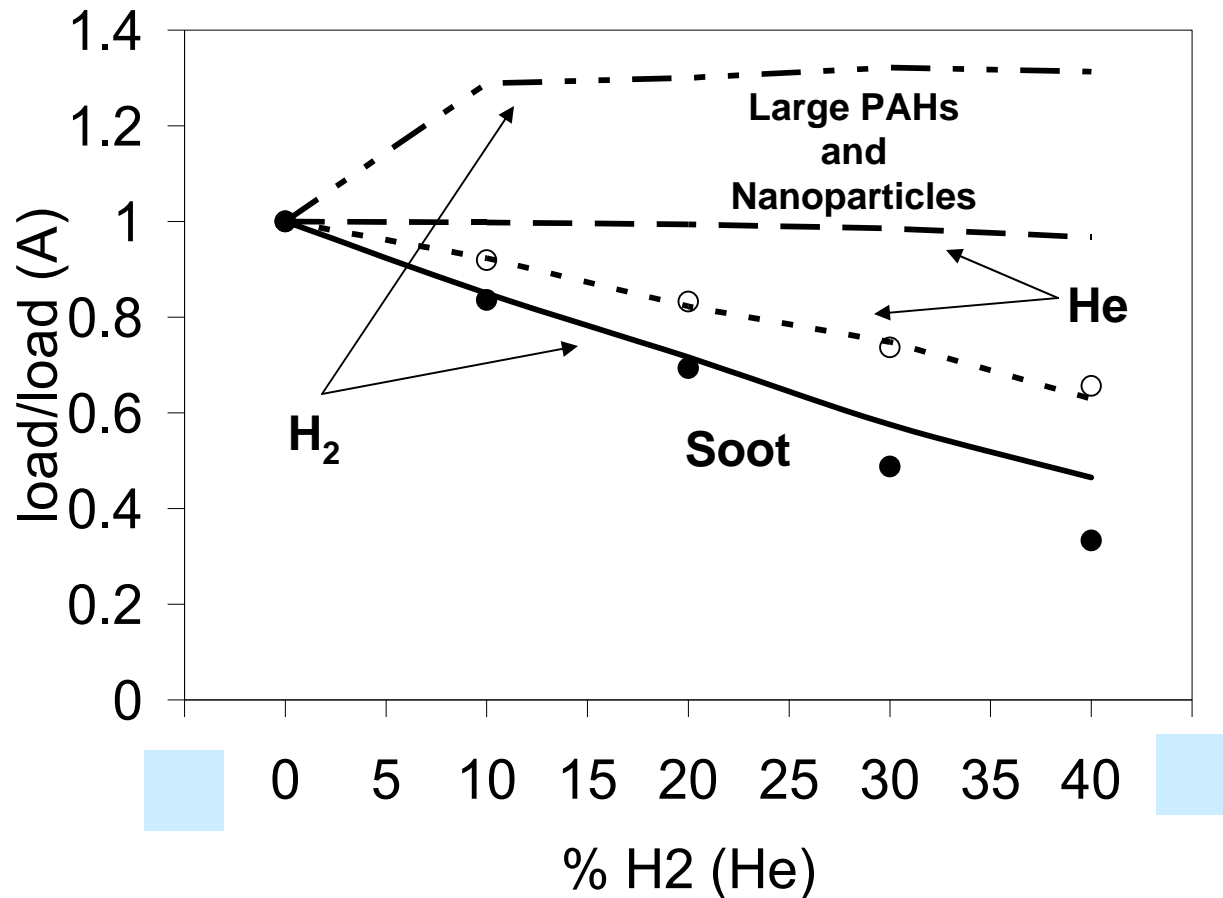
Both diluents
inhibit soot
formation

Soot load decrease is
generally proportional
to percentage of
diluents



LAMINAR PREMIXED FLAMES - RESULTS

(at 14 mm height)



Reduction in soot load more evident with H₂ addition

Enhanced formation of other pollutants as PAHs and Nanoparticles with H₂ addition

Conclusions

1. In rich premixed ethylene-air flames different species are responsible for the absorption at 632.8 nm and 1064 nm. In evaluating the data, careful evaluation of the laser extinction measurements is necessary.
2. Emission measurements can also be affected by emitting species different from “mature” soot.
3. Hydrogen addition to premixed ethylene-air flames has a strong influence in reducing the total amount of soot and of “carbon species”. This is due to the contribution of both a dilution and chemical effects.
4. Enhanced amount of PAHs and nanoparticles with respect to “mature” soot in H_2 flames is also found.