

Thirty-Second Task Leaders Meeting
International Energy Agency Implementing Agreement
on Energy Conservation and Emissions Reduction in Combustion
Nara Royal Hotel, Nara, Japan, July 25-29

1.6A.06: Okayama University, Japan

Prof. Eiji Tomita

Dual fuel: Premixed gaseous fuel and diesel direct injection

Effect of component of biomass-based gaseous fuels
on combustion in a super-charged gas engine with
micro-pilot injection



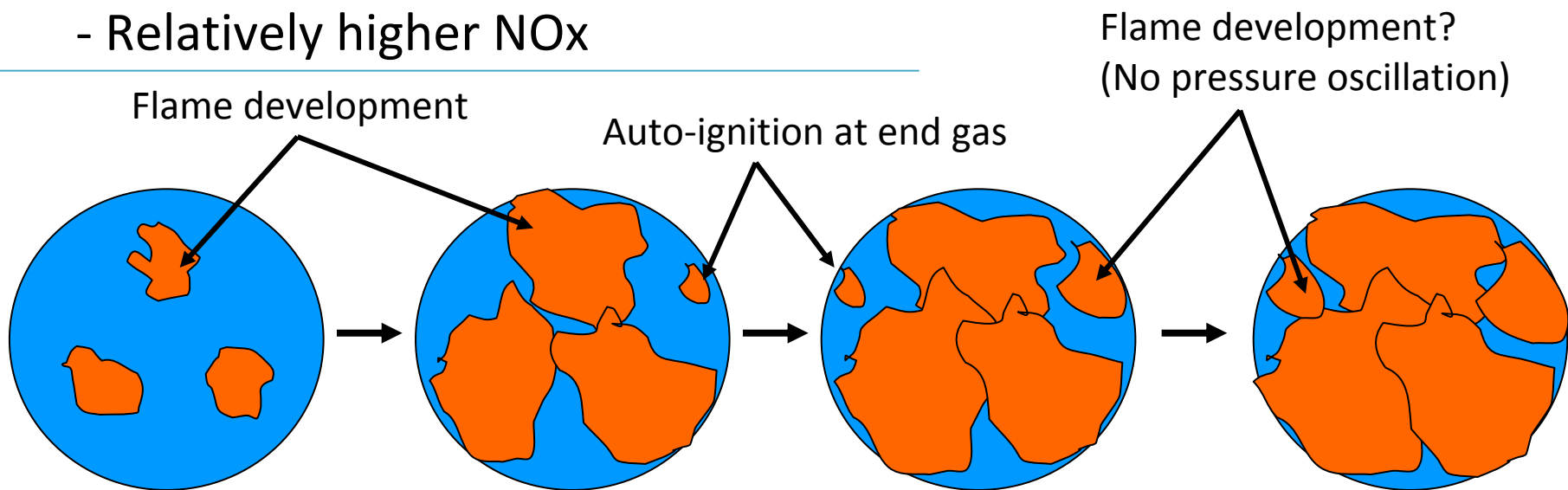
Eiji Tomita,
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Murari Mohon Roy
(Okayama University)

Flame development → auto-ignition without knock
→ other flame developments
or mild auto-ignition

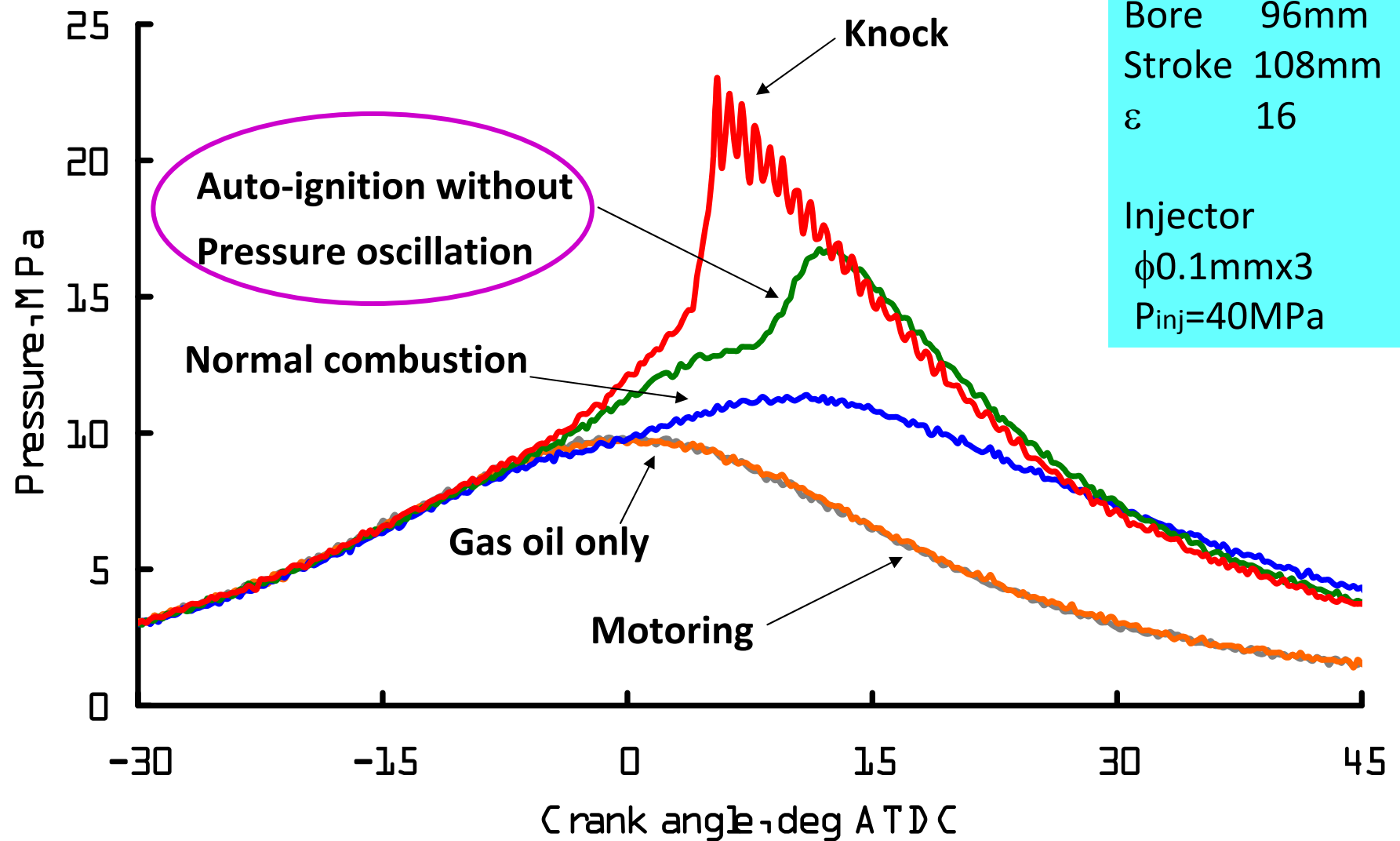
Engine: Lean burn gas engine ignited with diesel fuel (Gas oil)

Features

- Higher thermal efficiency
- Lower HC
- Relatively higher NO_x

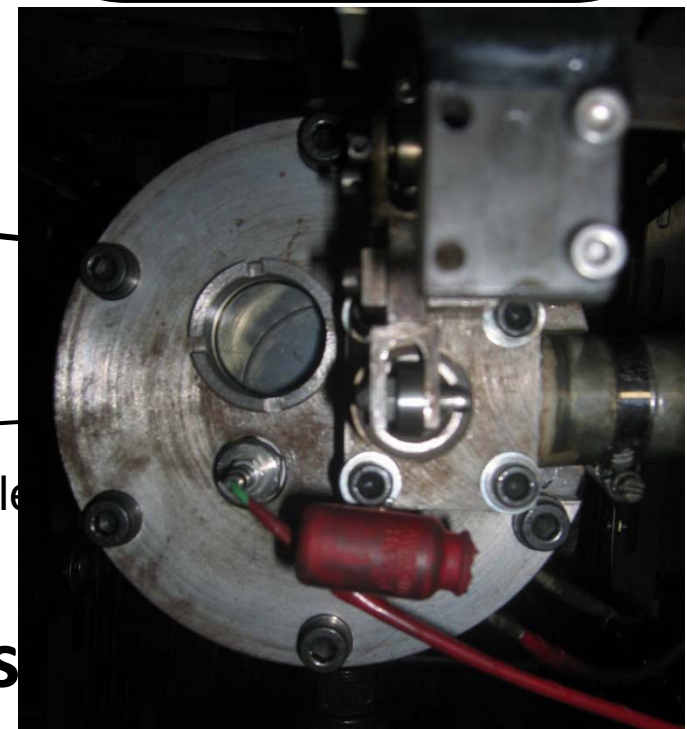
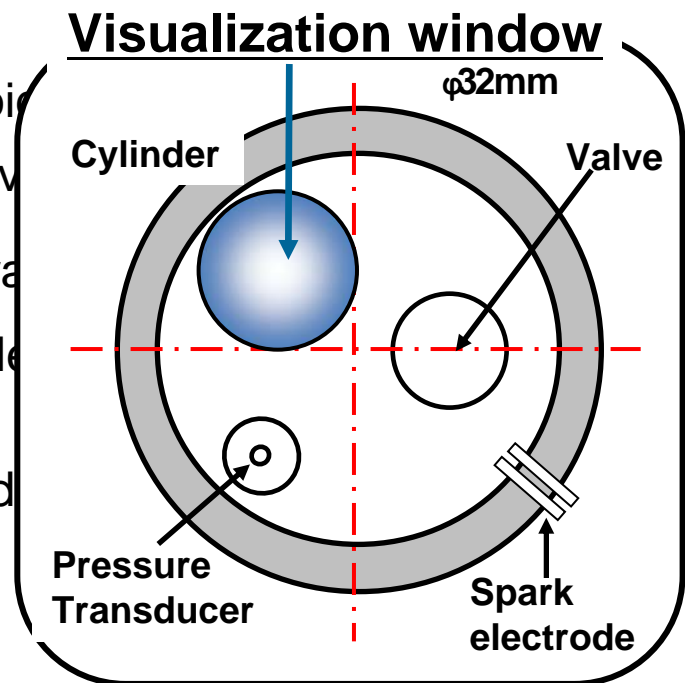
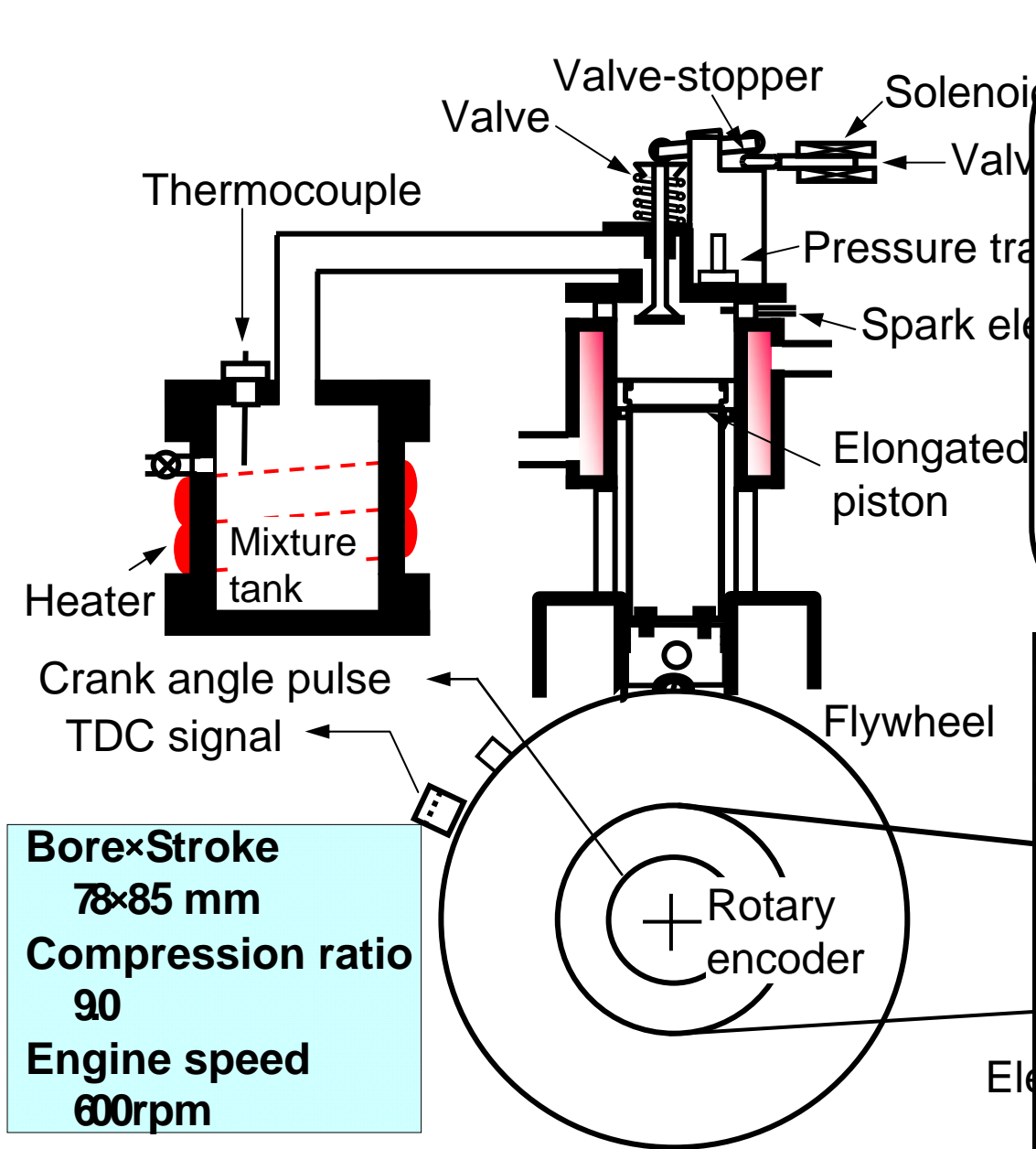


Motivation

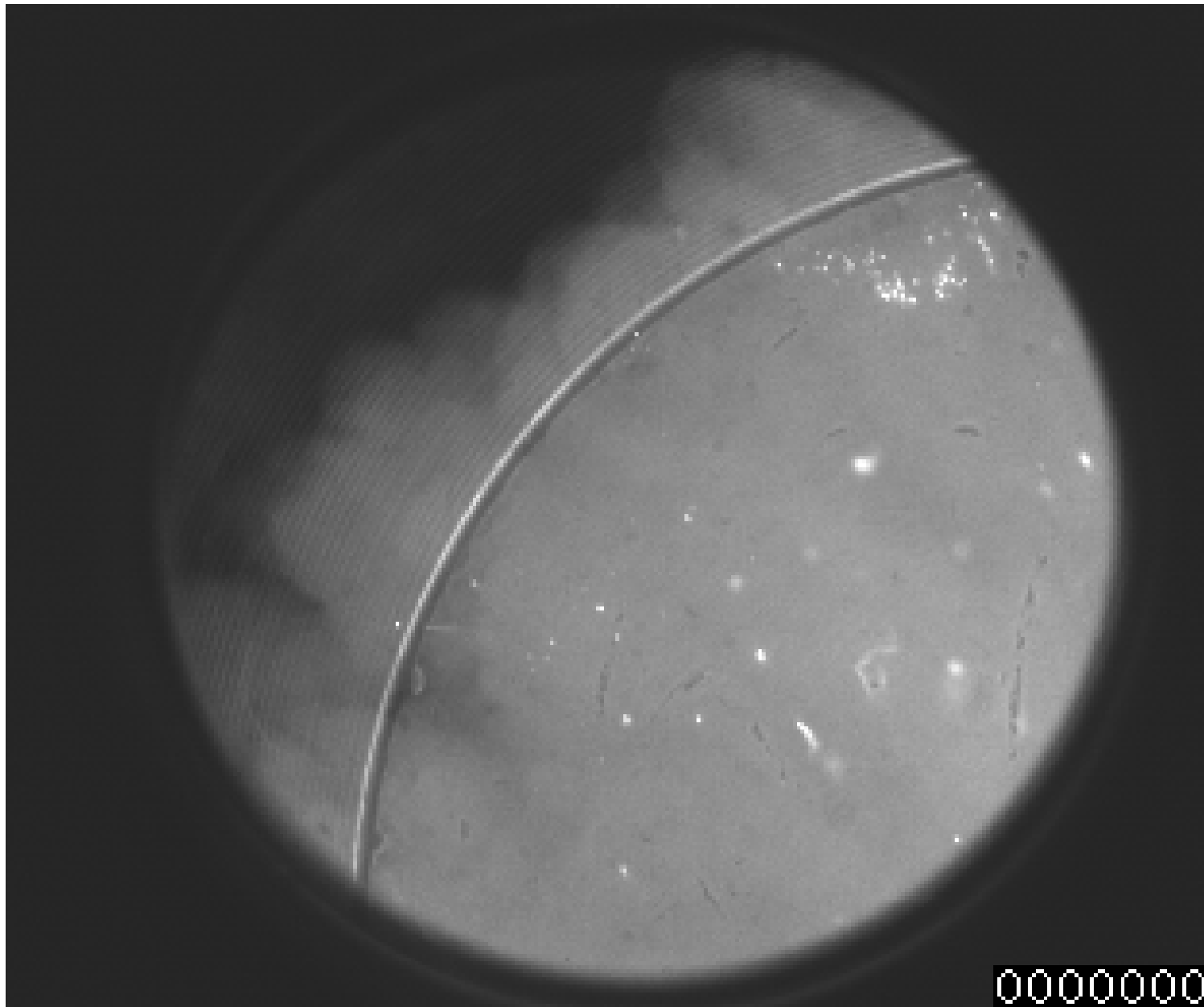


$n=1000\text{rpm}$, Natural gas + diesel fuel $\phi_t=0.6$, $m_{go}=2.0\text{mg/cycle}$, $P_{in}=200\text{kPa}$

Natural gas engine ignited with pilot diesel fuel

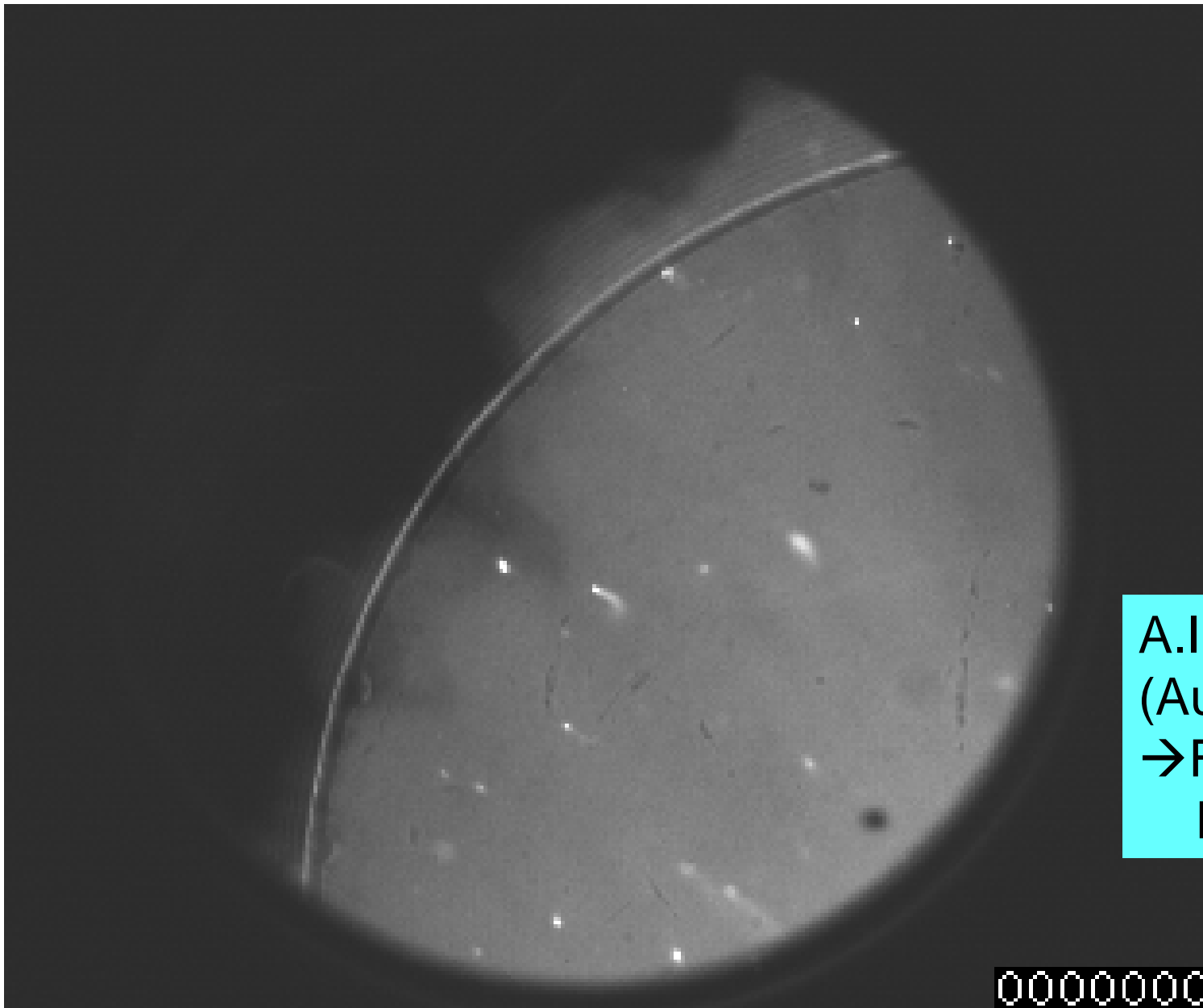


Experimental setup



Knock

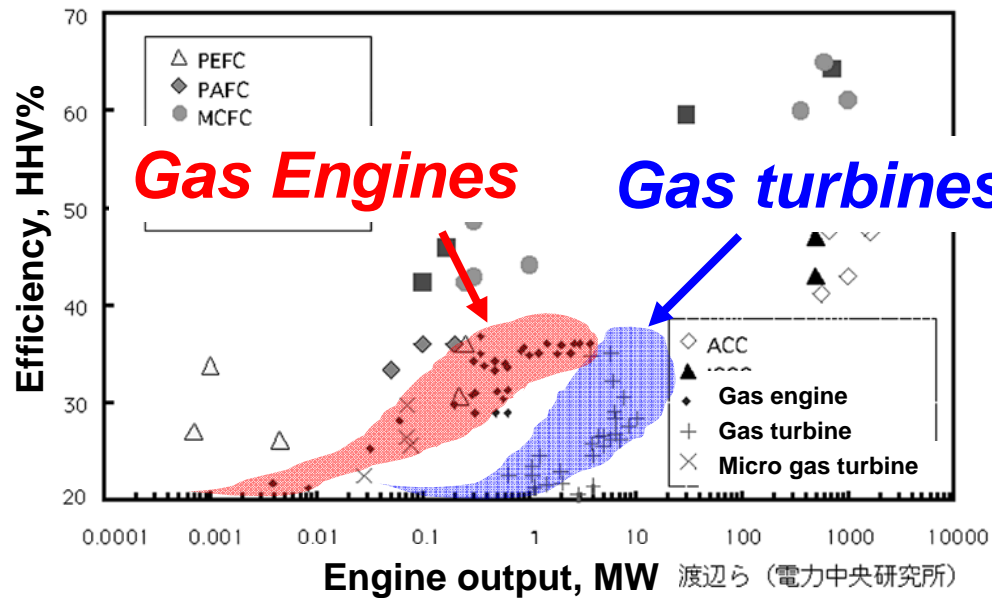
Combustion near end gas region with a high-speed video camera



A.I. → F.P.
(Auto-ignition
→ Flame
Propagation)

Combustion near end gas region with a high-speed video camera

Power generation



Reference

http://www.iae.or.jp/publish/kihou/29-1/03_7.html

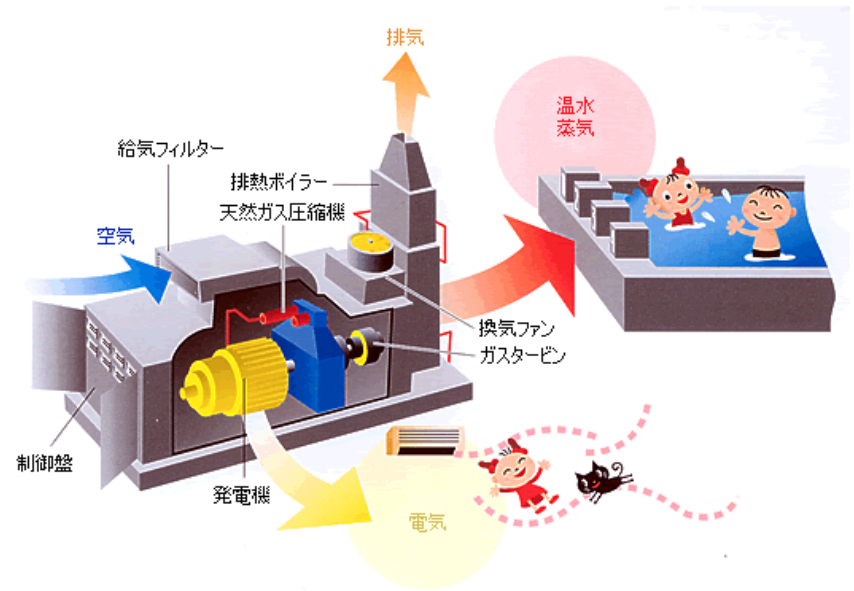
Gas Engines

Gaseous fuel



High octane number

Ignition systems



Dual-fuel gas engine

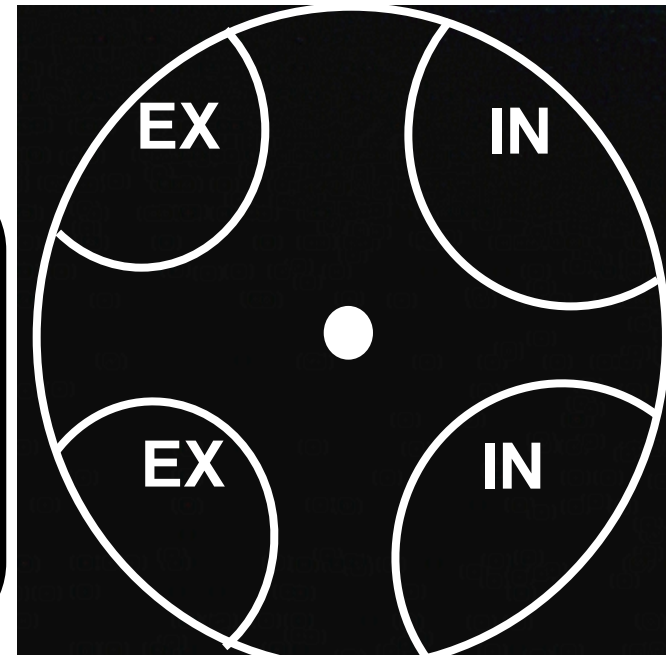
(6 cvlinders. 1000kW)

Background

Dual-fuel system

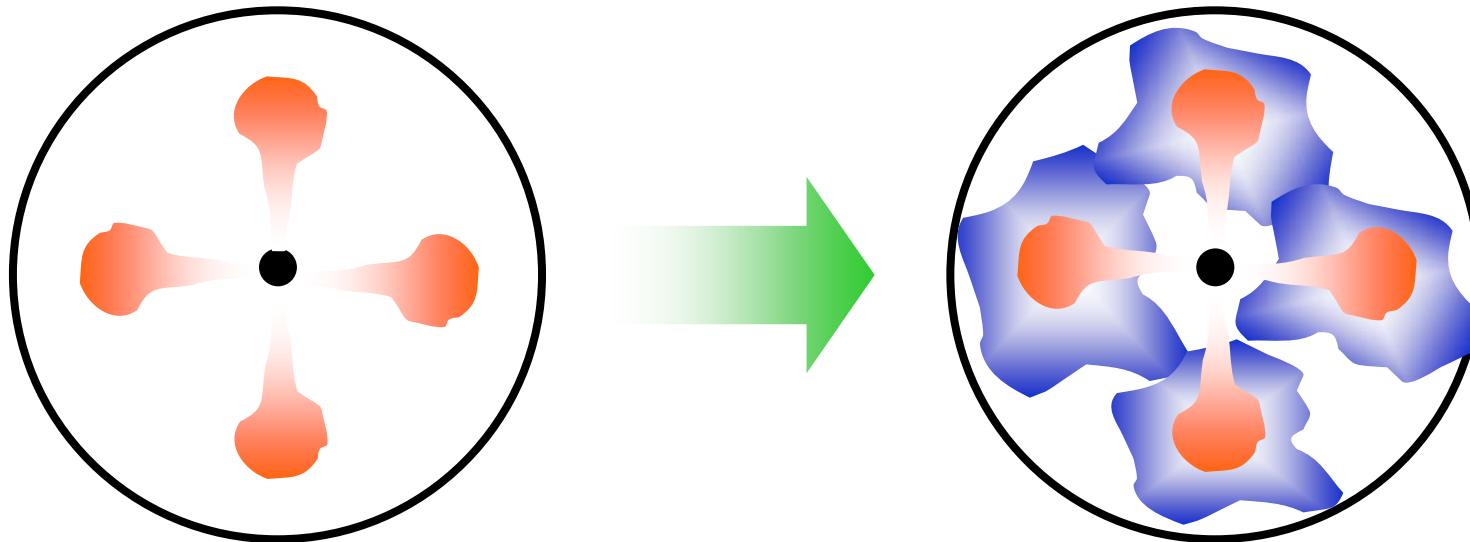
*Diesel fuel ; **ignition sources***

- *Multi-point ignition*
- *Easy control of ignition energy*
- *High power and thermal efficiency*

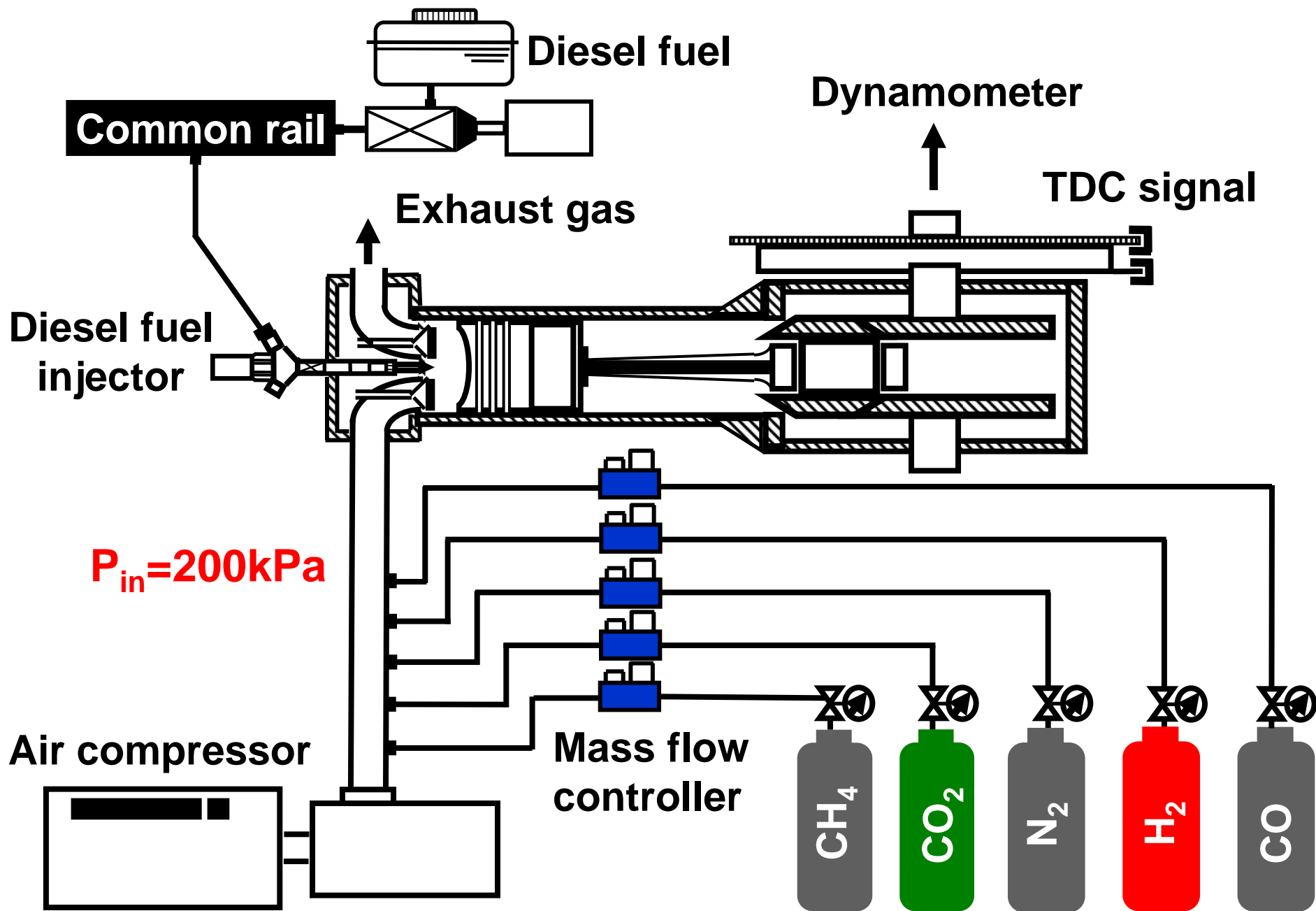


Auto-ignition of diesel fuel

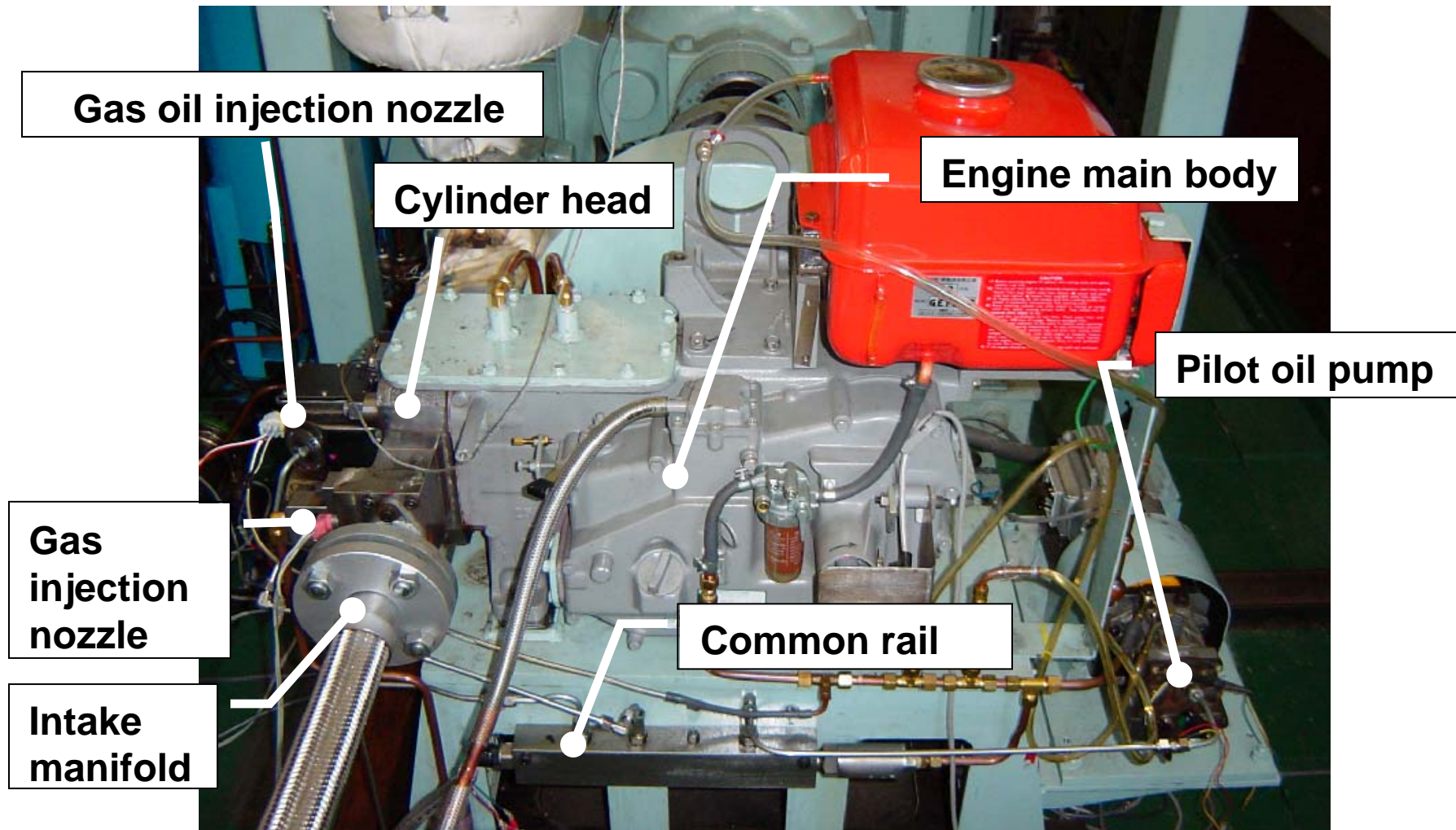
Flame development of gaseous fuel



Dual - fuel system



Experimental apparatus



Bore×Stroke 96×108 mm (782 cc)

Compression ratio 16.0

Engine speed 1000 rpm

Intake pressure 200 kPa

| | CH ₄ [%] | CO [%] | H ₂ [%] | CO ₂ [%] | N ₂ [%] | H _{lf} [MJ/Nm ³] |
|----------|---------------------|--------|--------------------|---------------------|--------------------|---------------------------------------|
| Type1 | 22.3 | 22.3 | <u>20.0</u> | 16.8 | 39.0 | 5.65 |
| Standard | 22.3 | 22.3 | 13.7 | 16.8 | 45.3 | 4.96 |
| Type2 | 22.3 | 22.3 | 13.7 | <u>23.0</u> | 39.1 | 4.96 |

1.9

Standard : Biomass gas made of wood tips

Type□ H2-enriched

Type2: CO2-enriched

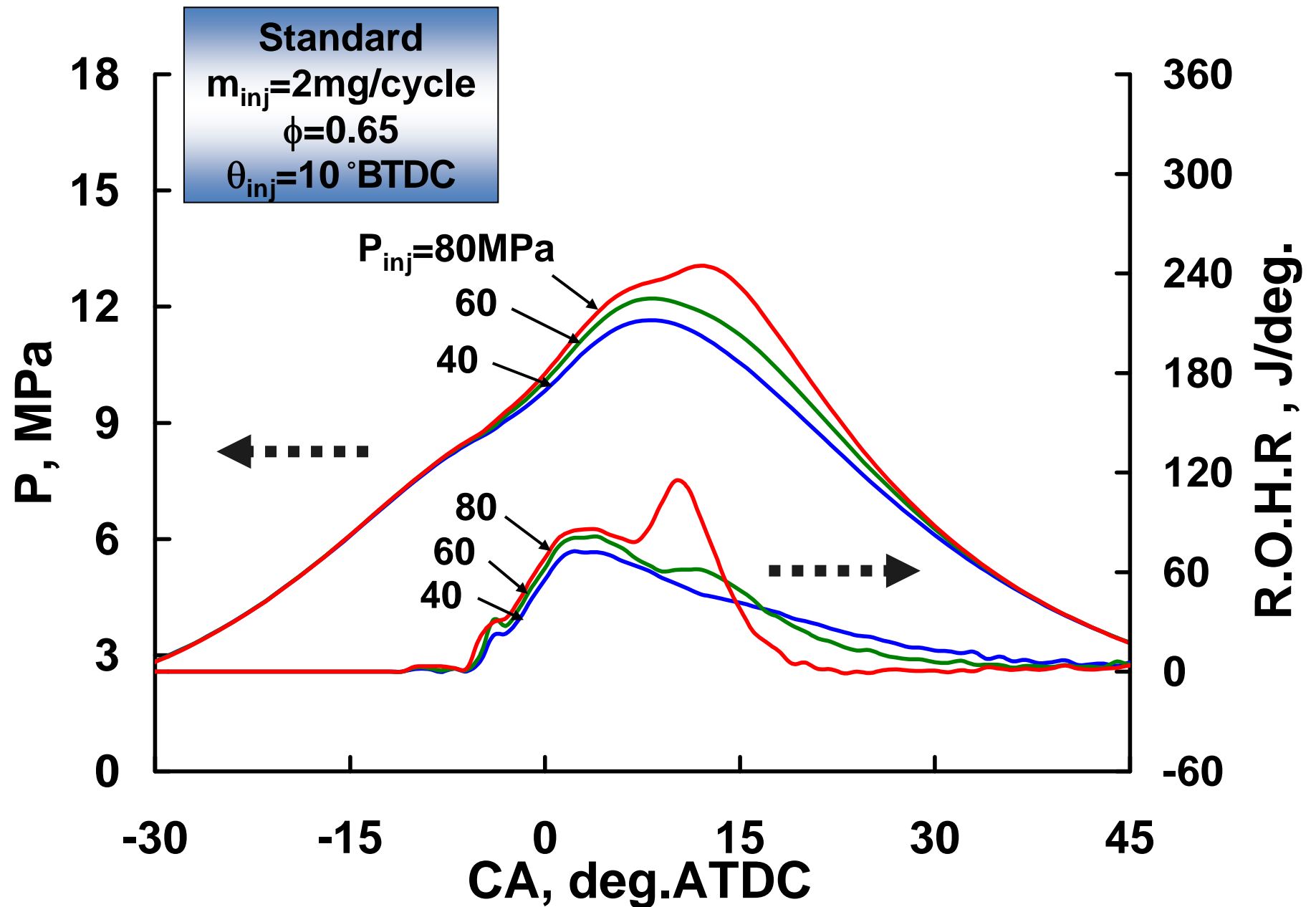
| | CH ₄ [%] | C ₂ H ₆ [%] | C ₃ H ₈ [%] | C ₄ H ₁₀ [%] | H _{lf} [MJ/Nm ³] |
|---------|---------------------|-----------------------------------|-----------------------------------|------------------------------------|---------------------------------------|
| NG(13A) | 88.9 | 6.8 | 3.1 | 1.2 | 39.2 |

Gas components

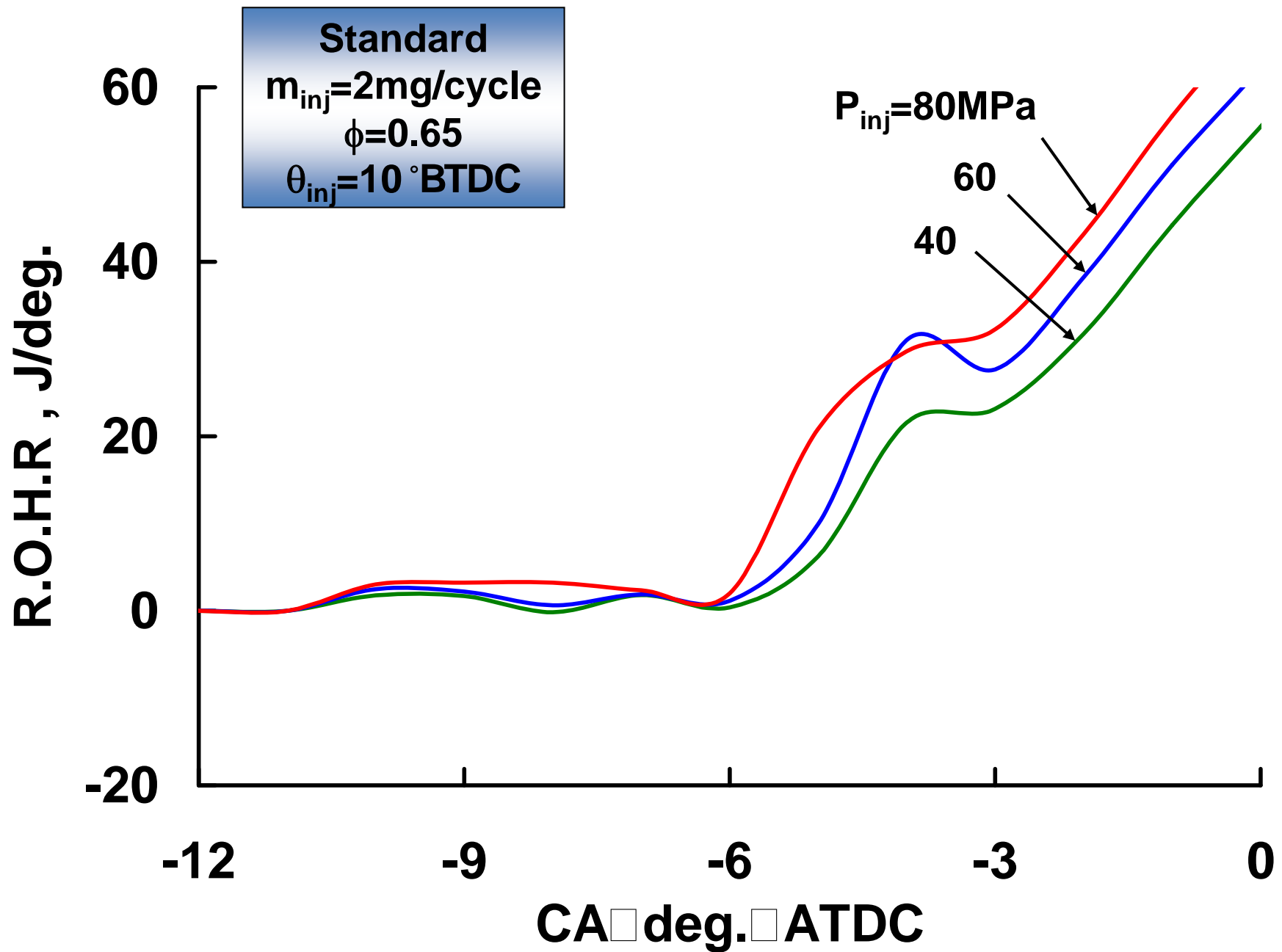
Effects of injection pressure and amount of diesel fuel
on combustion and exhaust emissions

Standard

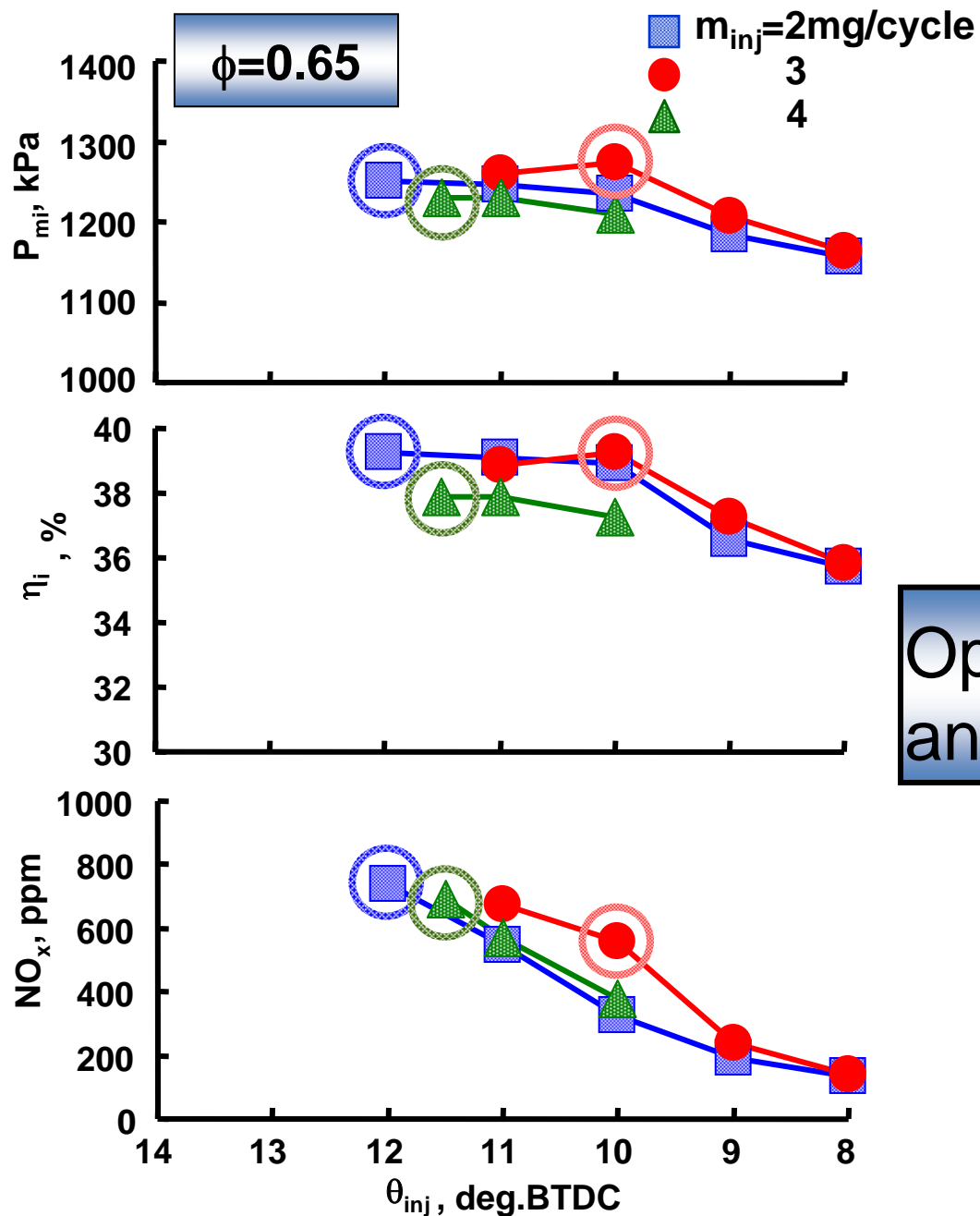
$\phi_{\square}=0.65$



Effect of injection pressure of diesel fuel ($m_{inj}=2\text{mg/cycle}$)



Effect of injection pressure of diesel fuel on ROHR



IMEP

High load

Thermal efficiency

High efficiency

Optimum injection pressure
and amount of diesel fuel

$P_{inj}=80\text{MPa}$

$m_{inj}=3\text{mg/cycle}$

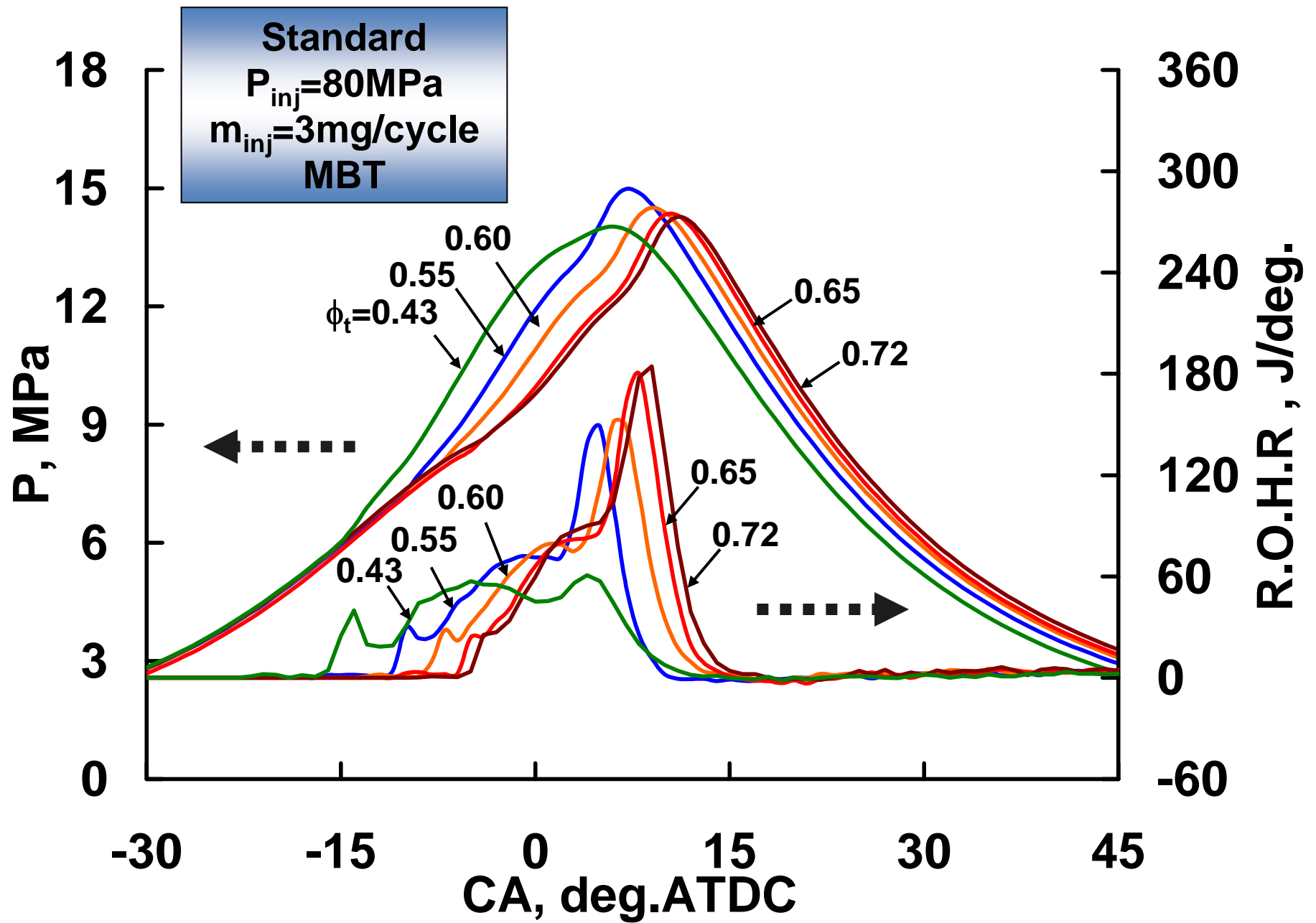
Effect of amount of diesel fuel on combustion ($P_{inj}=80\text{MPa}$)

Effect of equivalence ratio on combustion and exhaust emissions

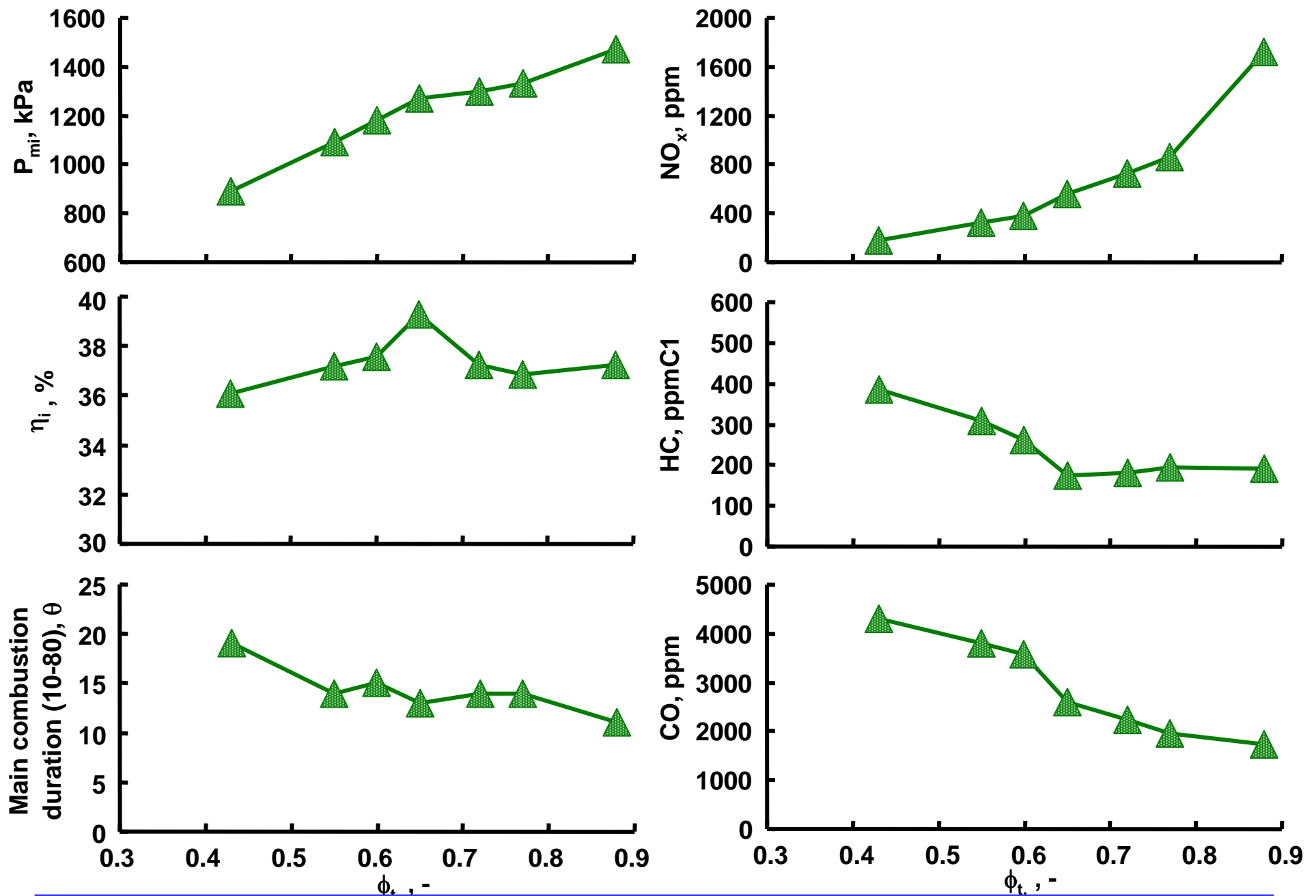
Standard

$P_{inj} = 80 \text{ MPa}$

$m_{inj} = 3 \text{ mg/cycle}$



Effect of equivalence ratio on pressure history and ROHR



Effect of equivalence ratio on engine performance (Standard)

Effect of equivalence ratio on engine performance and exhaust emissions

$$P_{inj} = 80 \text{ MPa}$$

$$m_{inj} = 3 \text{ mg/cycle}$$

Standard, Type1, Type2

| | CH ₄ [%] | CO [%] | H ₂ [%] | CO ₂ [%] | N ₂ [%] | H _{lf} [MJ/Nm ³] |
|----------|---------------------|--------|--------------------|---------------------|--------------------|---------------------------------------|
| Type1 | 22.3 | 22.3 | 20.0 | 16.8 | 39.0 | 5.65 |
| Standard | 22.3 | 22.3 | 13.7 | 16.8 | 45.3 | 4.96 |
| Type2 | 22.3 | 22.3 | 13.7 | 23.0 | 39.1 | 4.96 |

1.9

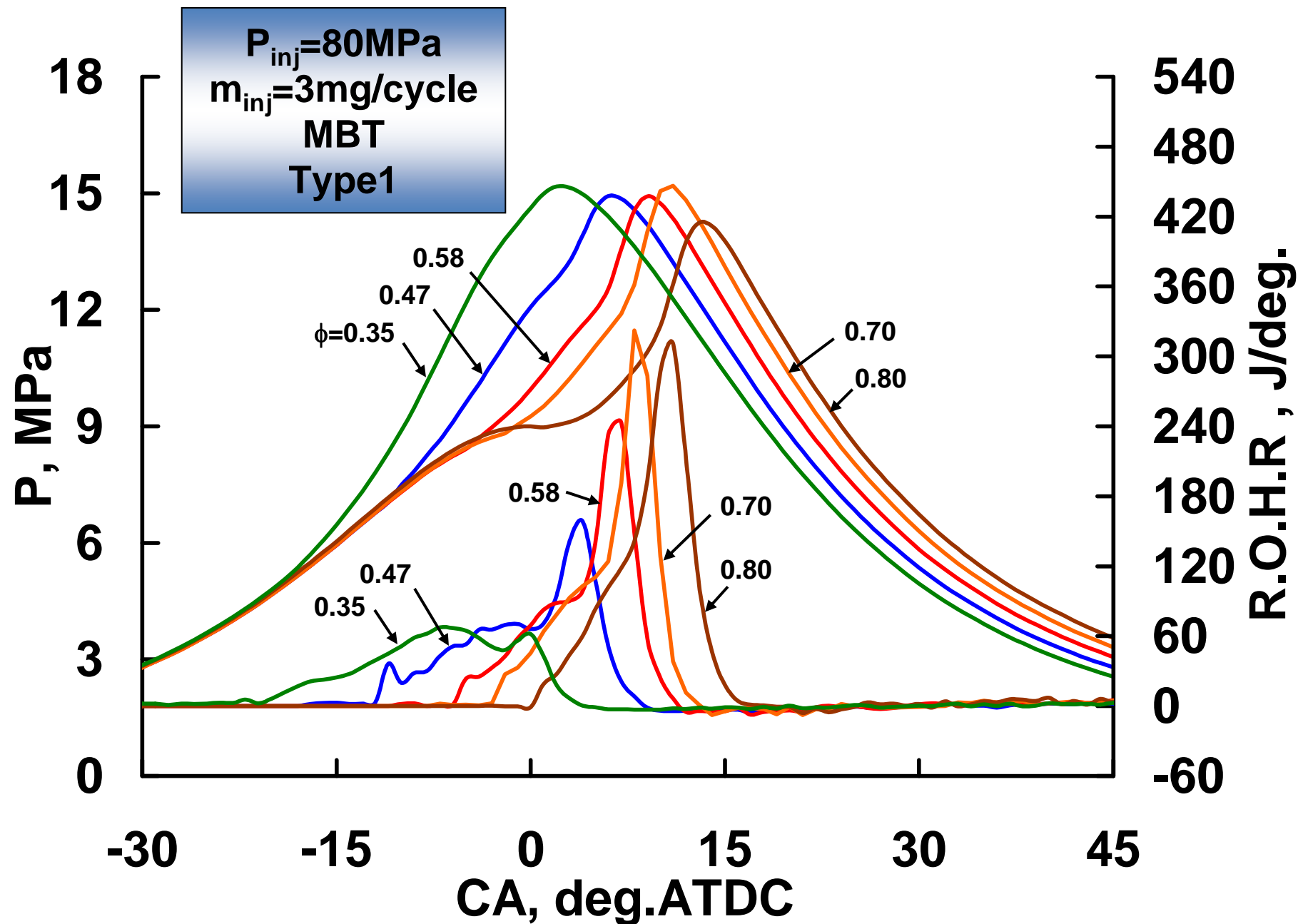
Standard : Biomass gas made of wood tips

Type□ H2-enriched

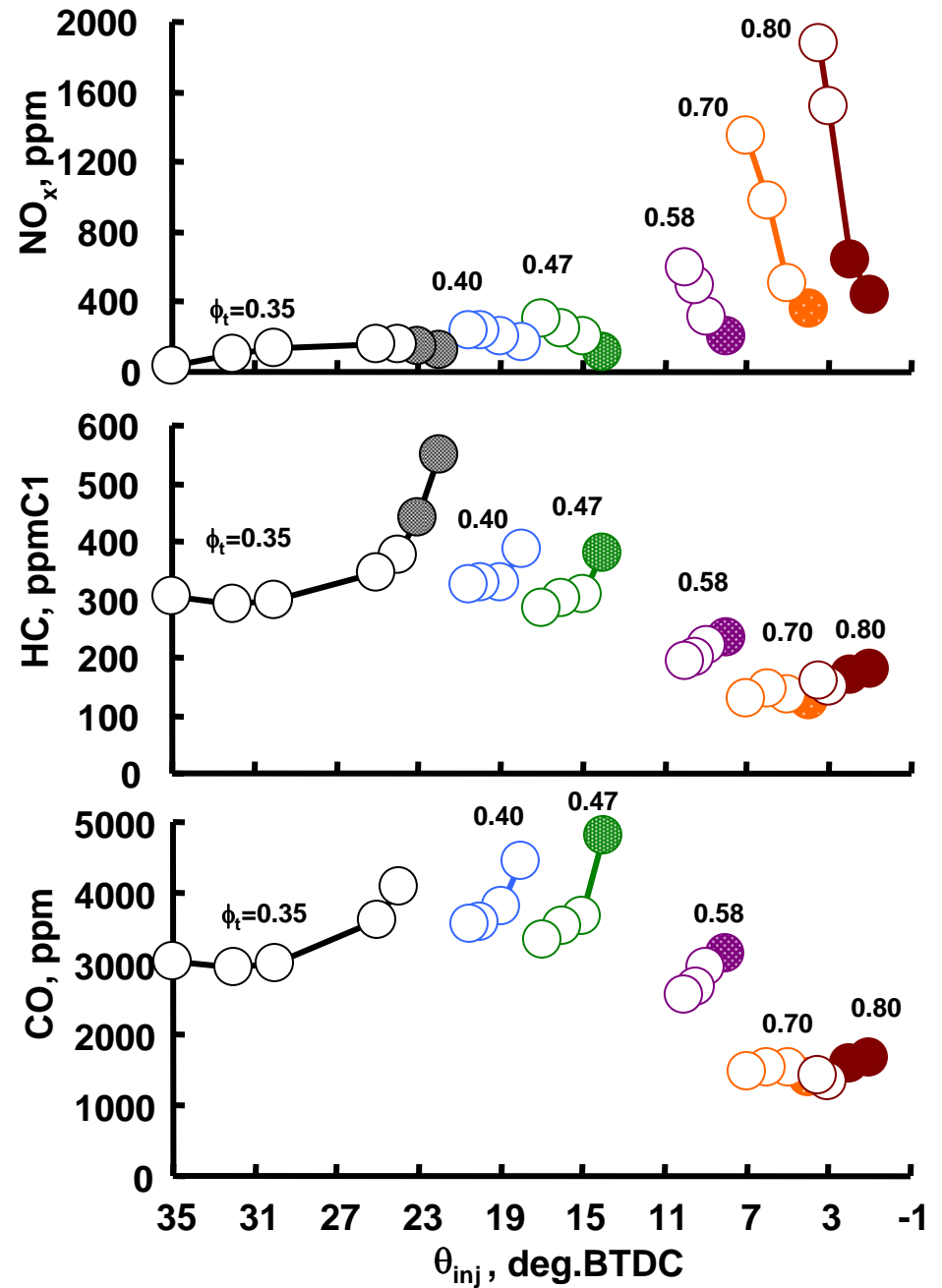
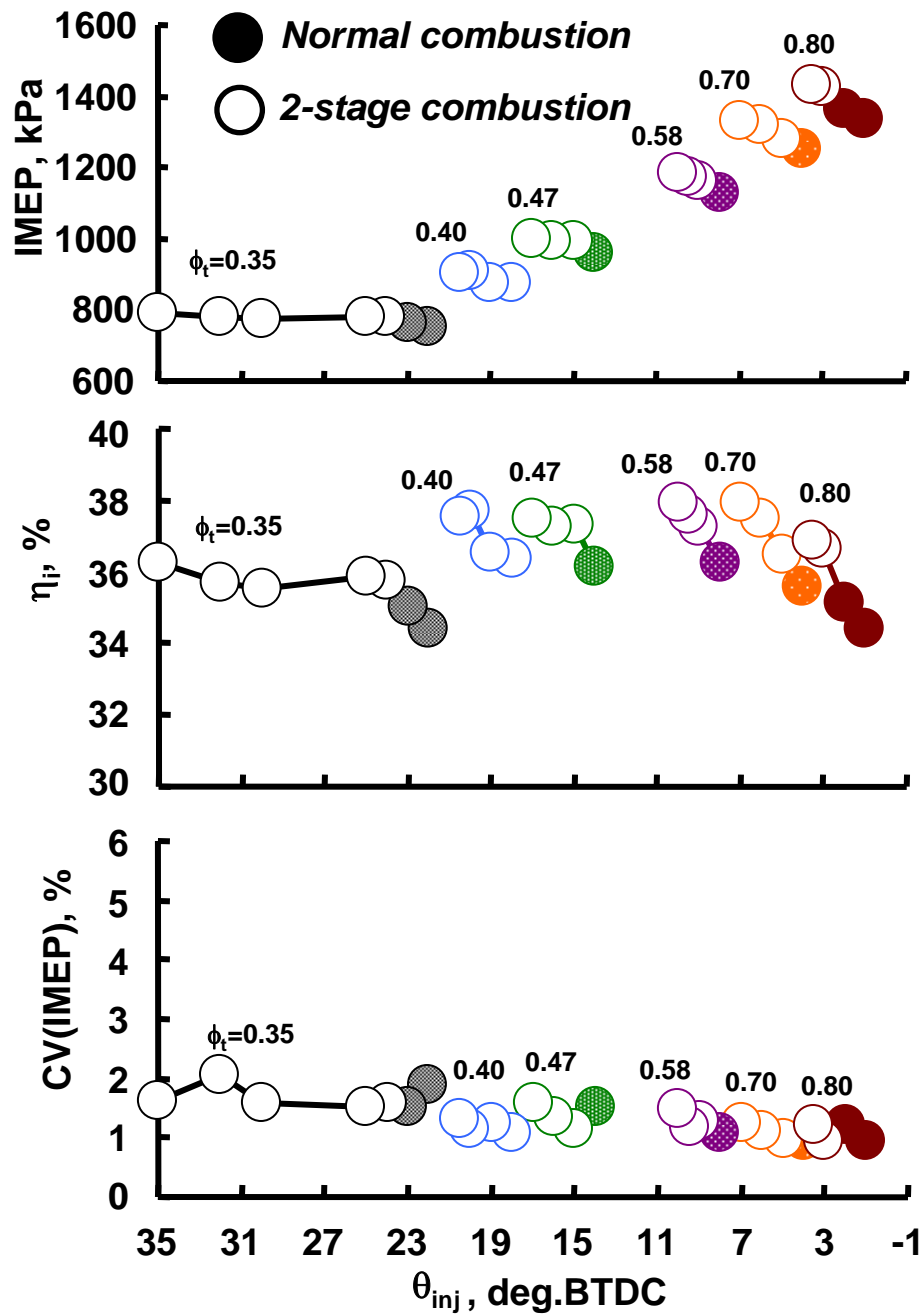
Type2: CO2-enriched

| | CH ₄ [%] | C ₂ H ₆ [%] | C ₃ H ₈ [%] | C ₄ H ₁₀ [%] | H _{lf} [MJ/Nm ³] |
|---------|---------------------|-----------------------------------|-----------------------------------|------------------------------------|---------------------------------------|
| NG(13A) | 88.9 | 6.8 | 3.1 | 1.2 | 39.2 |

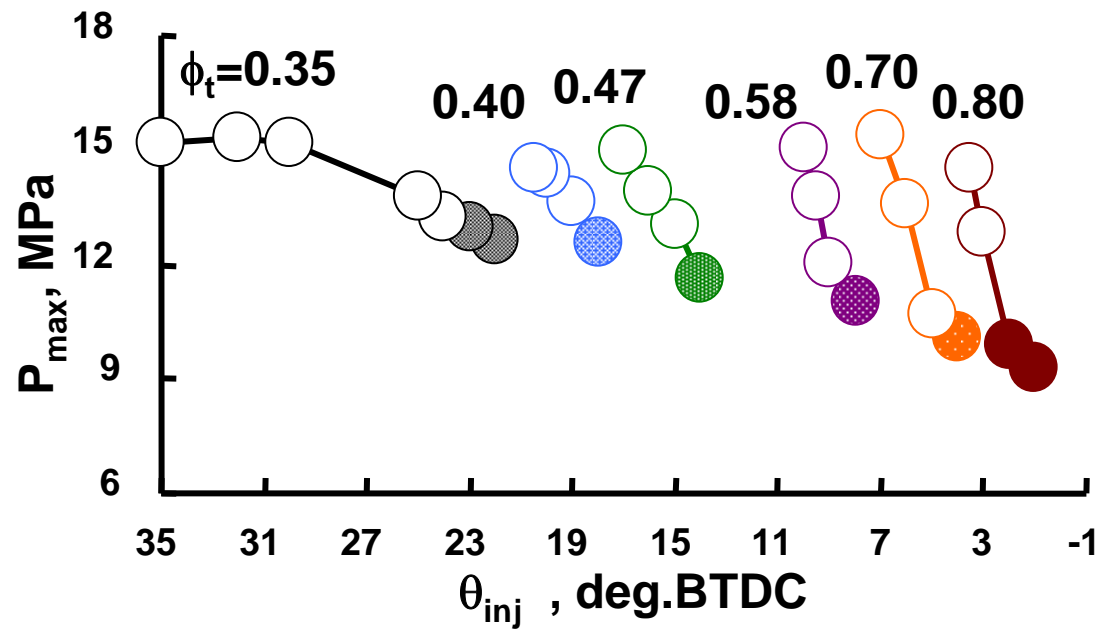
Gas components



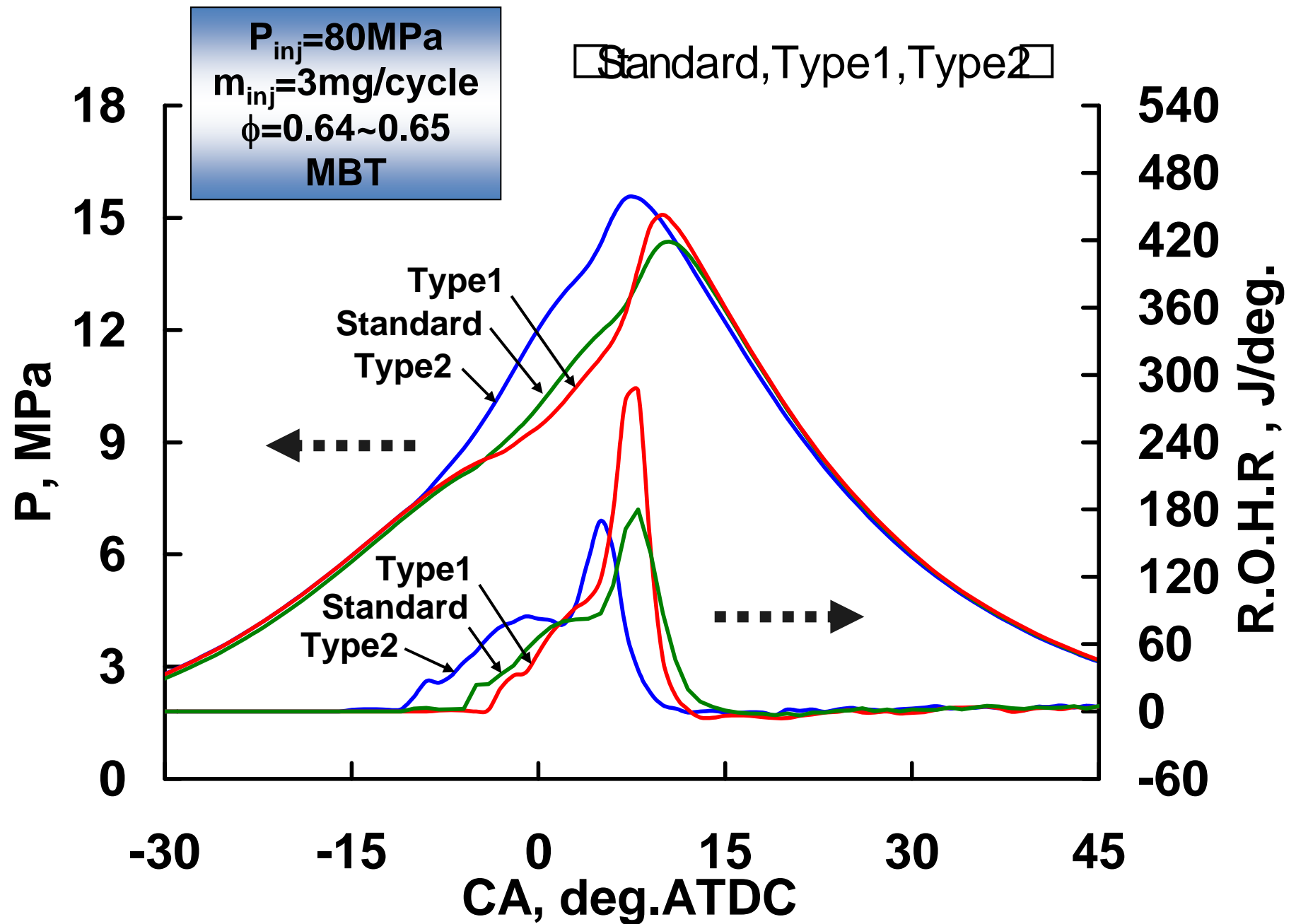
Pressure history and ROHR (Type 1; H2-enriched)



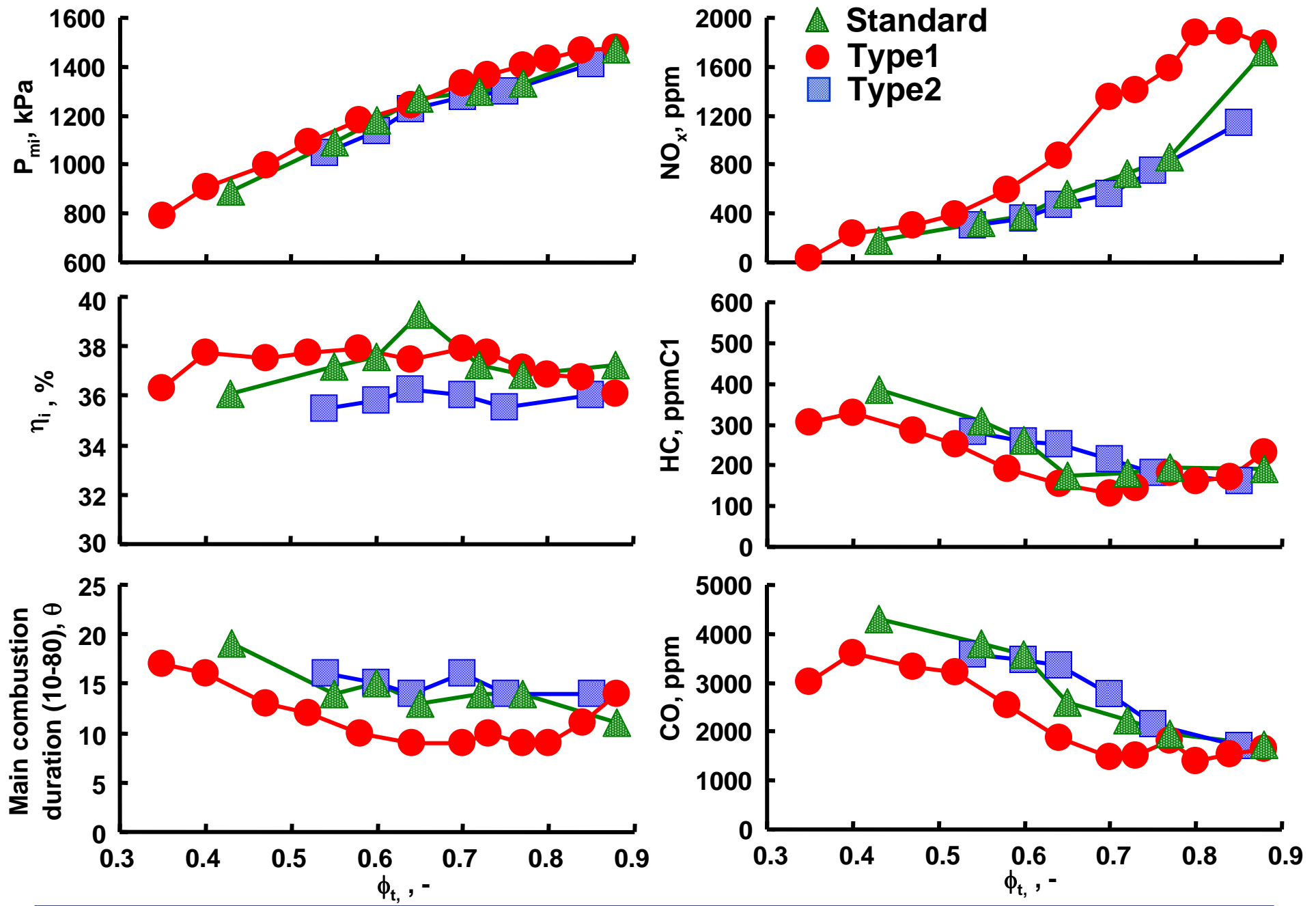
$P_{inj}=80\text{MPa}$, $m_{inj}=3\text{mg/cycle}$, Type1; H2-enriched



$P_{\text{inj}}=80\text{MPa}$, $m_{\text{inj}}=3\text{mg/cycle}$, Type1; H2-enriched



Effect of gas component on pressure history and ROHR



Effect of gas component on performance and exhaust emissions

- (1) A broader window of fuel–air equivalence ratio ($\phi=0.42\text{--}0.79$) was obtained using high H₂-content producer gas. On the other hand, with low H₂-content producer gas, the optimum window of fuel–air equivalence ratio was narrower ($\phi= 0.52\text{--}0.68$).
- (2) Two-stage combustion was an indicator of maximum power conditions as well as a precursor of knock for producer gases. The main combustion (10–80% MFB) with two-stage combustion cycles took less than half the time of normal combustion. In addition, high H₂-content gas reduced the main combustion compared to the case with low H₂-content gas in both normal and two-stage combustion.

Summary