

Laminar burning velocity correlation for H_2 ICE modeling

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H_2 ICE session

Problem

- Support H₂ ICE development through modeling
- Modeling turbulent combustion of H₂ requires data on laminar burning velocity u_l
- u_l : propagation speed of planar flame front in a premixed, quiescent mixture
- Literature:
 - insufficient data on H₂/air
 - hardly any engine-like conditions
 - no data on effect of residuals (EGR!)
 - limited data taking account of stretch effects

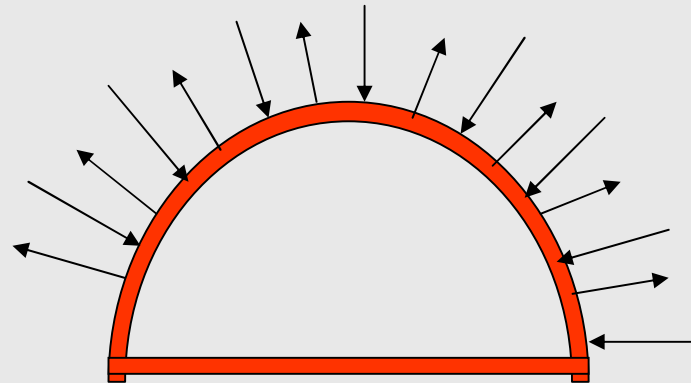
Solution?

- Calculation of u_l with 1D chemical kinetics code.
Straightforward? Unfortunately not:
 - Reaction mechanism OK at atmospheric, severe doubts at high p and T
 - Calculations seem to break down for lean mixtures and elevated p
 - Limited use (e.g. effect of residuals)
- Measurement of u_l
 - At engine-like conditions
 - Taking account of stretch effects
 - However: experimental difficulties...

Stretch

Stretch: affects the balance between diffusion of unburned gas to the flame front and heating of the unburned by the flame front

Heat flux from
flame front to
unburned, $\sim D_T$



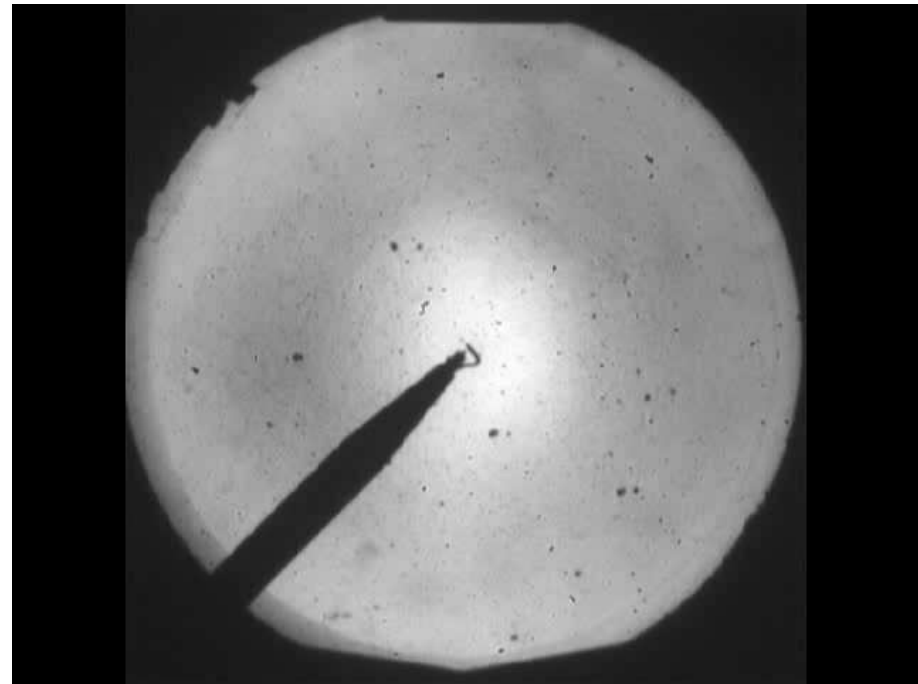
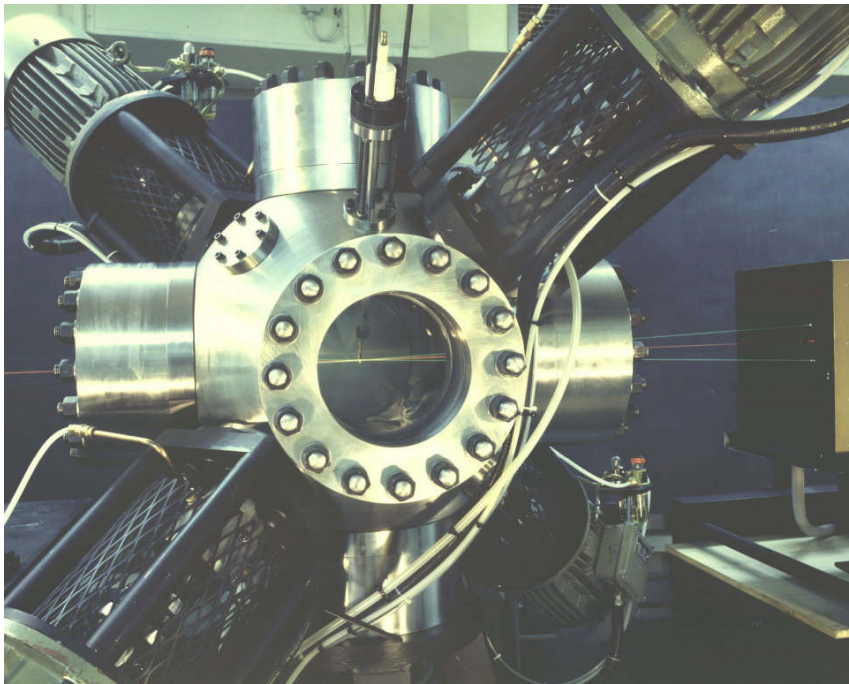
Mass diffusion of
unburned to
flamefront, $\sim D_M$

Thus: affects flame speed!

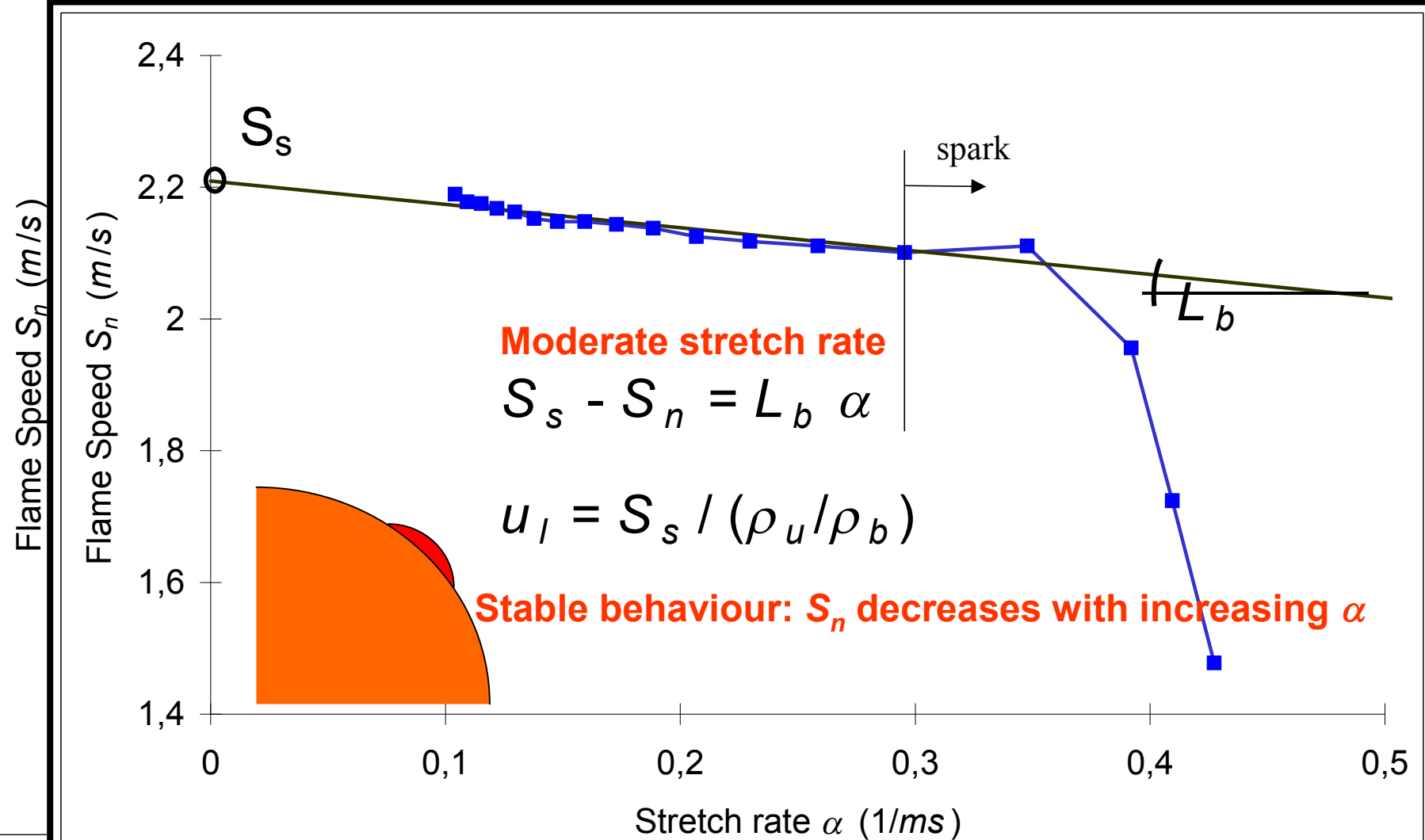
Any experimental set-up: deviation from steady, non-stretched planar geometry

Stretch rate $\alpha = 1/A \, dA/dt$, relative change of flame area element

Measurement of u_i



CH₄/air, $\phi = 1$, 300 K, 1 bar



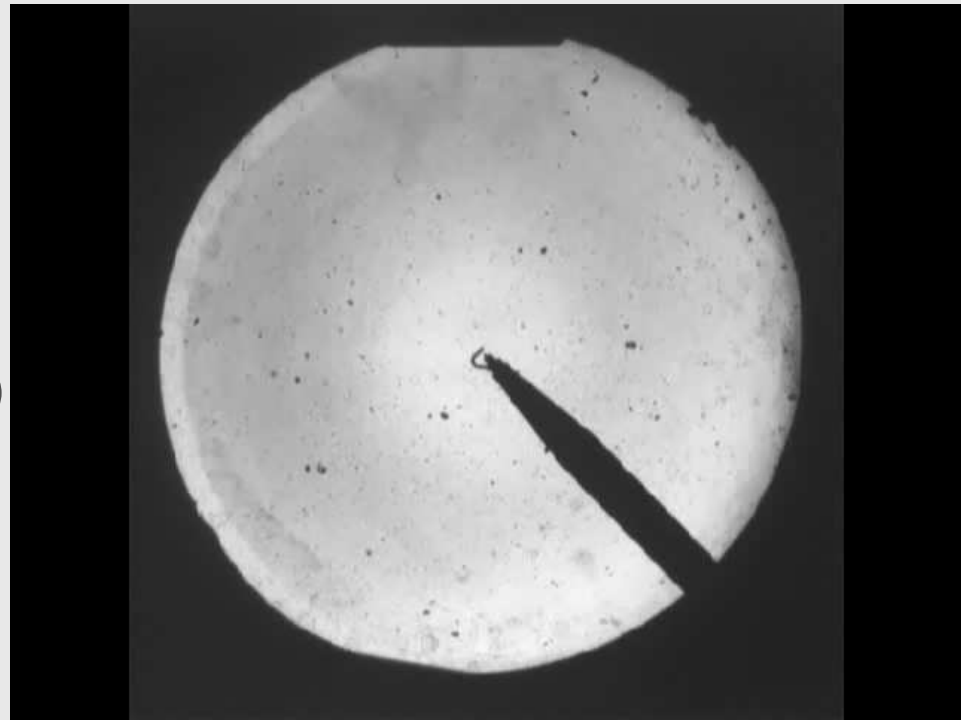
Stretch and instabilities

Dependent on mixture properties:

- flame is insensitive to flame stretch rate
- flame speed decreases for positive flame stretch (stable)
- flame speed increases for positive flame stretch (unstable)

Lean hydrogen mixture: unstable, develops cells and accelerates

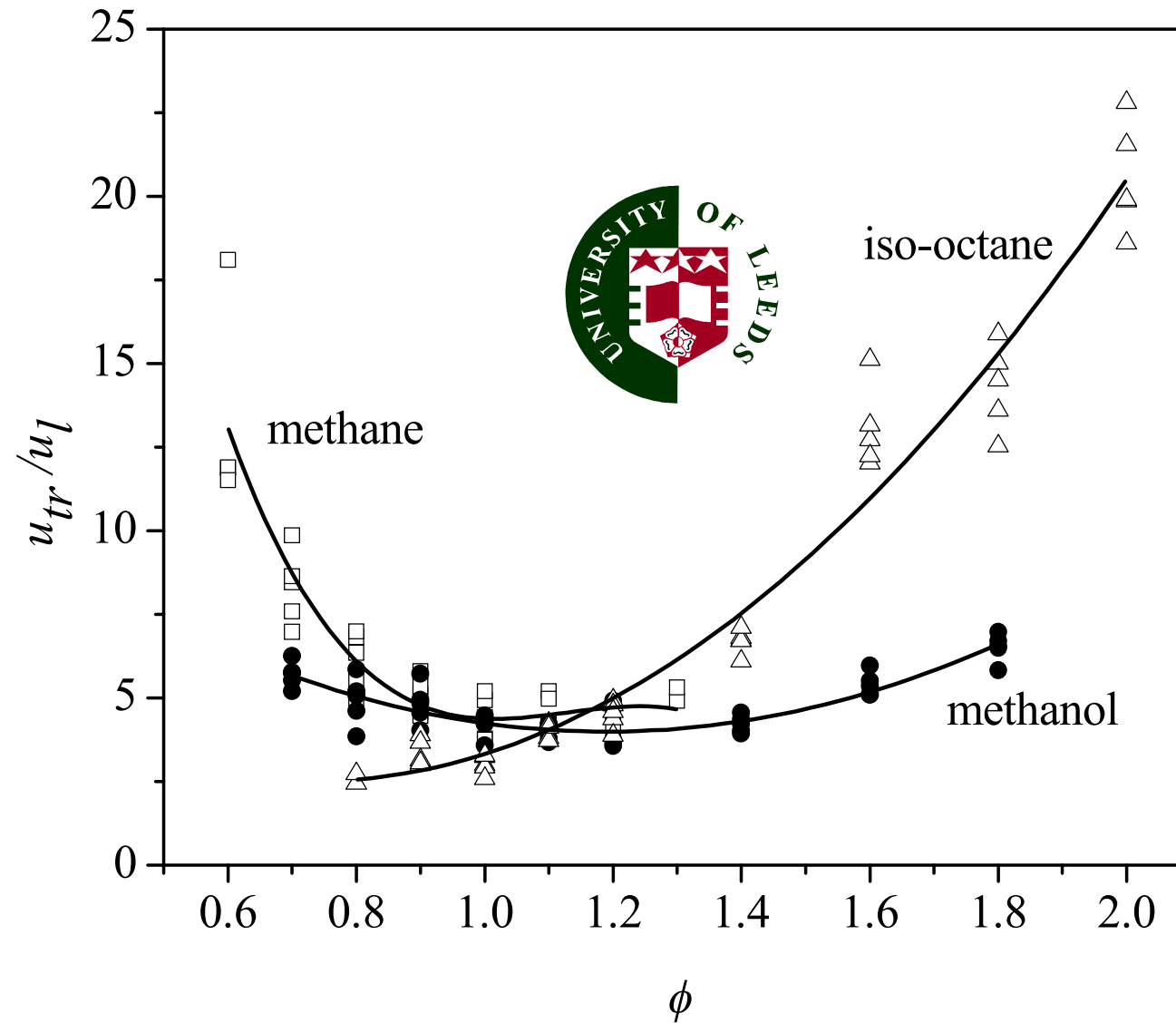
Flame observation: prerequisite to determining correct burning velocity!



Stretch and instabilities

Relevance to engine combustion:

- Flames get increasingly unstable for higher pressures
- Existing u_f correlations mostly pressure-derived, thus influenced by stretch! e.g. iso-octane/air correlations of Metghalchi&Keck
- It is very likely that for all practical fuel/air mixtures, the laminar flames are unstable at engine conditions
- But: a number of turbulent combustion models assume the turbulent motion 'erases' the flame instabilities, so that these have no effect on the turbulent burning velocity
- Others assume the effect of instabilities is only important at low u' / u_f



Lawes, Ormsby, Sheppard, Woolley, CS&T 177:1273-1289

Database u_l H_2 mixtures

Measurements of H_2 /air/residuals u_l 's at:

- 300, 365 and 430 K
- 1, 5 and 10 bar
- Residual concentrations up to 30 vol%
- Equivalence ratios ϕ between 0.25 and 1.0

However, at 5 and 10 bar: no u_l 's!

Methodology: use of $u_{n,10mm}$ to determine trends

- Indication of burning velocity
- Fixed condition, repeatable
- 10 mm: compromise ignition – cellular acceleration
- Parallel work: stability analysis (see later)

u_l correlation for engine code

$$u_n = u_{n0} \left(\frac{T}{T_0} \right)^{\alpha_T} \left(\frac{p}{p_0} \right)^{\beta_p} (1 - \gamma f)$$

- Based on measurements of cellular flames at elevated pressure
- Effects of residual gas: new, can be added to other correlations
- Compared with existing correlation (Iijima&Takeno, C&F1986) in engine code

Result: nonphysical results with existing correlation, good results with ours

Refs: - PhD Verhelst, <http://hdl.handle.net/1854/3378>
- Verhelst, Woolley, Lawes, Sierens, 30th Comb Symp p209-216

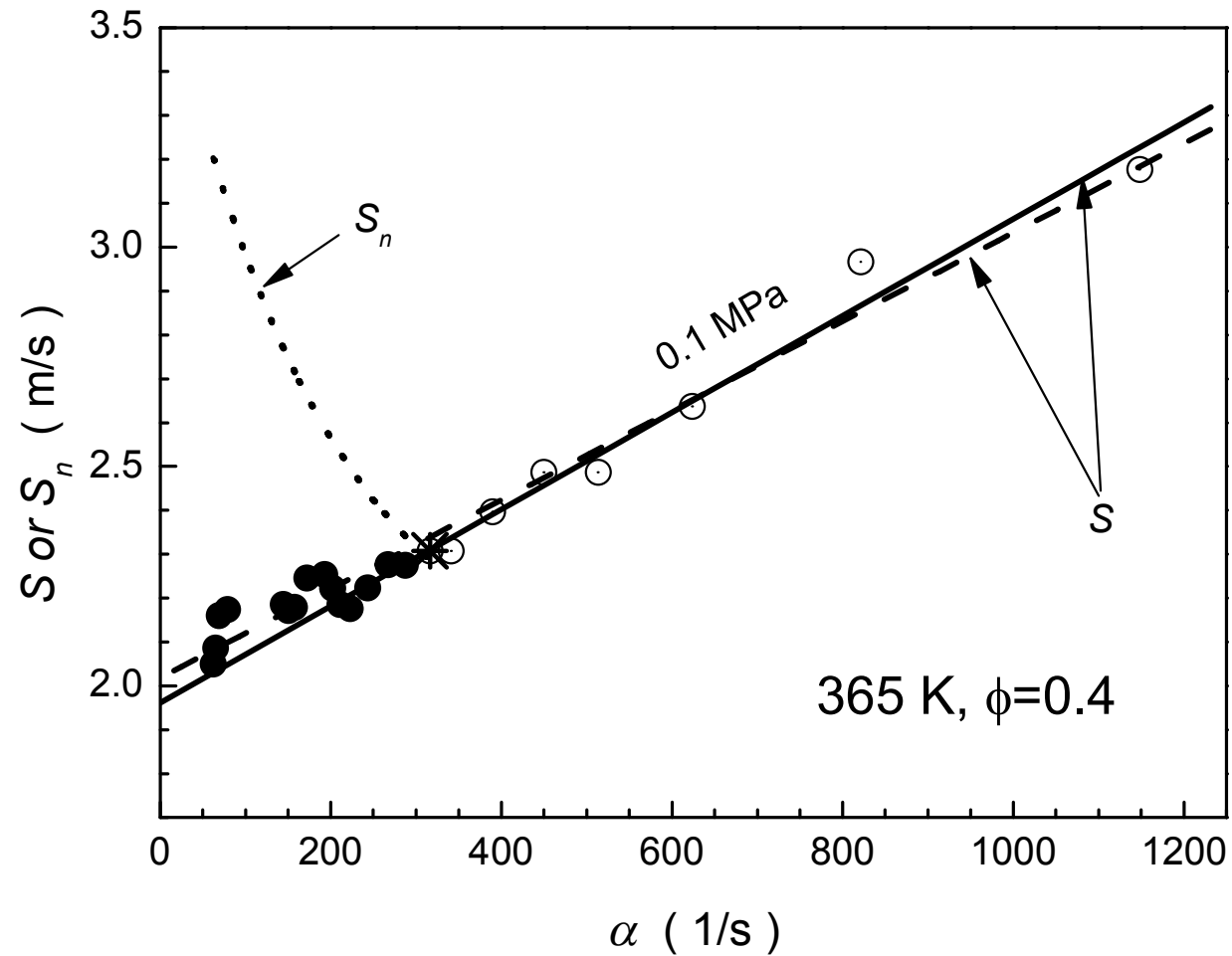
Extension

- Correlation is for stoichiometric to lean mixtures
- Current interest in H₂ DI engines: also data on rich mixtures needed
- Correlation was extended by IFP in the framework of the EU HyICE programme
 - Used by BMW and IFP

Refs: Proceedings 1st Int Symp on H₂ ICEs
- Gerke, Boulouchos, Wimmer p94-106
- Benkenida, Colin, Jay, Knop p195-206

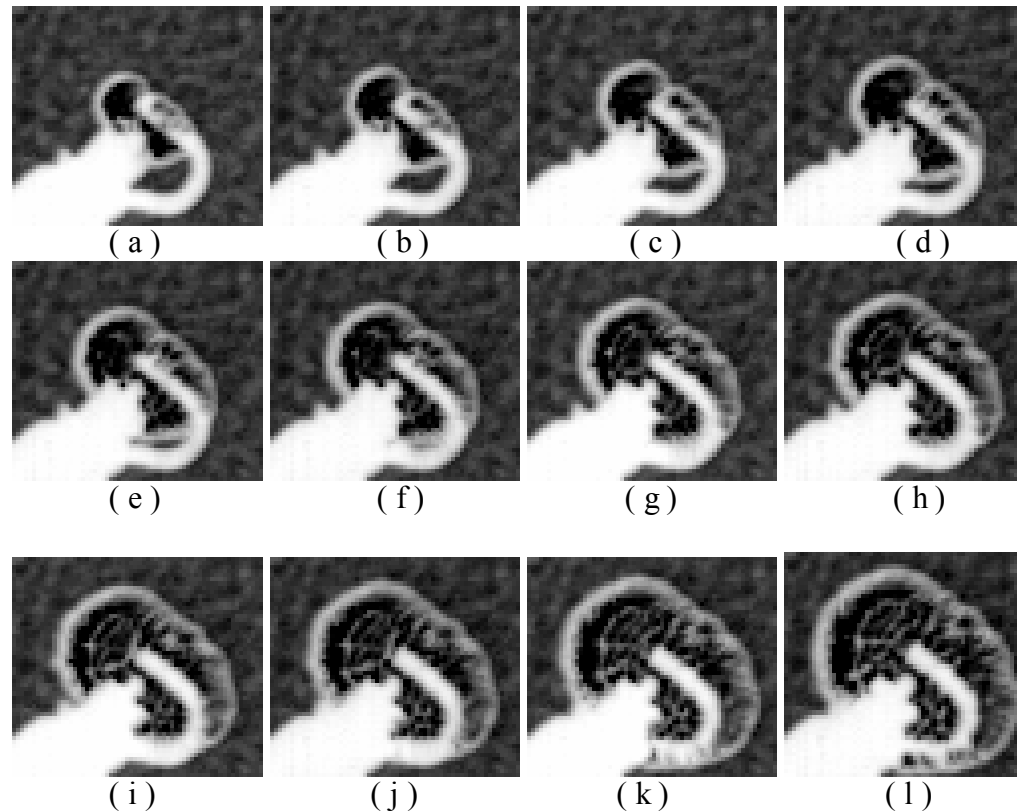
Stability analysis

- Ideally: $u_n = I_0 u_l$ in engine code, I_0 : stretch model
However: currently impossible, u_l ? I_0 ?
- Cellularity = ordered, reproducible
 - Use fractal considerations to determine surface of smooth flame from surface of cellular flame, ratio of flame speeds of cellular flame to 'smooth' flame equals ratio of flame areas
 - Determine inner and outer cutoff scales from range of wavelengths inducing instability
Inner cutoff: given by start of cellularity
Outer cutoff: flame size



Bradley, Lawes, Liu, Verhelst, Woolley, C&F 149:162-172

Experimental difficulties keep haunting us...



$p=0.5$ MPa, $T=365$ K, $\phi=0.6$, time interval 0.04 ms (25000 fps)

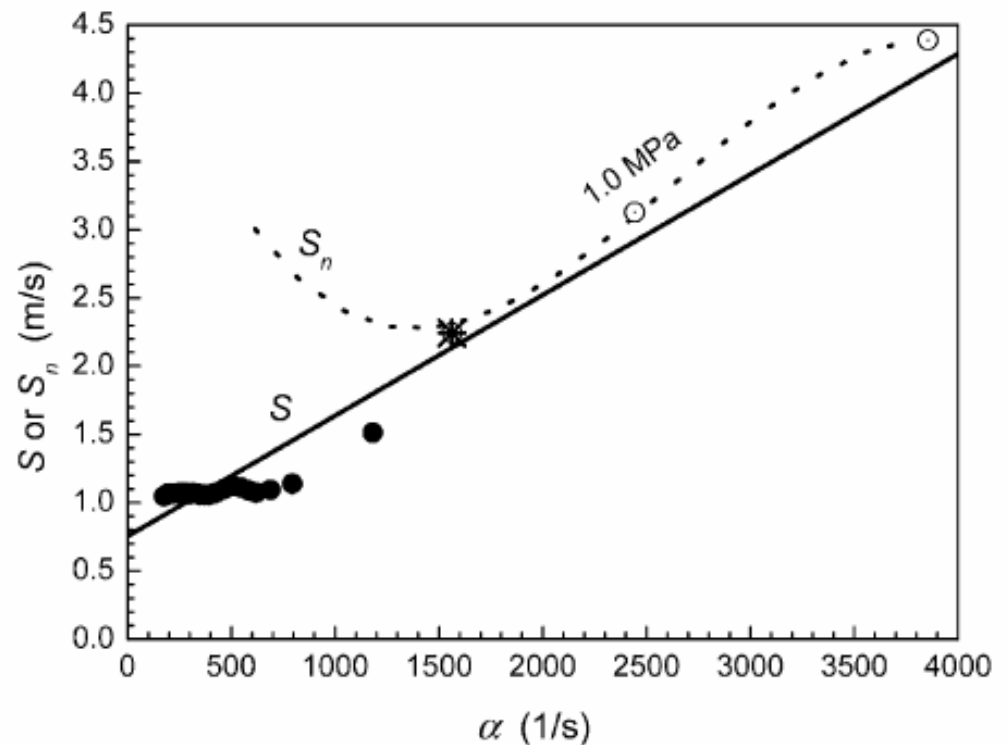
Bradley, Lawes, Liu, Verhelst, Woolley, C&F 149:162-172

Experimental difficulties

- Implications primarily for determination of Markstein numbers:

$$\frac{u_l - u_{nr}}{u_l} = K_s Ma_{sr} + K_c Ma_{cr}$$

- Large uncertainties on Markstein numbers
- I_0 model would require data on Ma
- High p : determination u_l also problematic



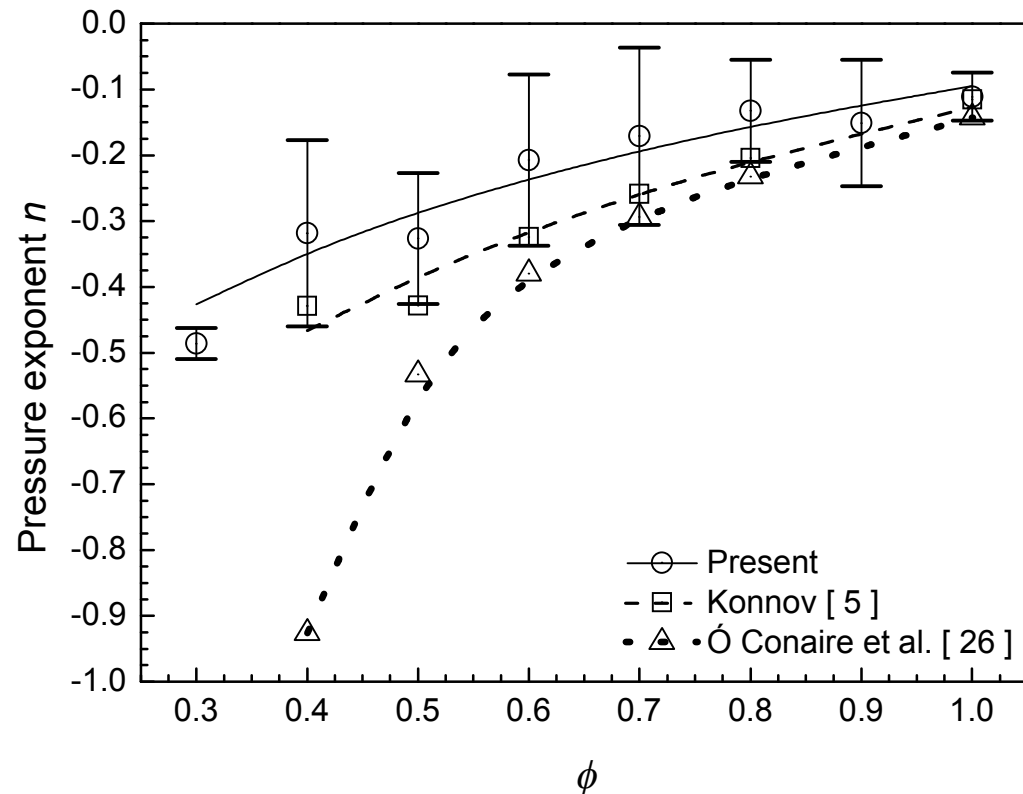
Encouraging results

- Pressure exponent
 $u_l \sim p^n$

- Uncertainty on kinetics:



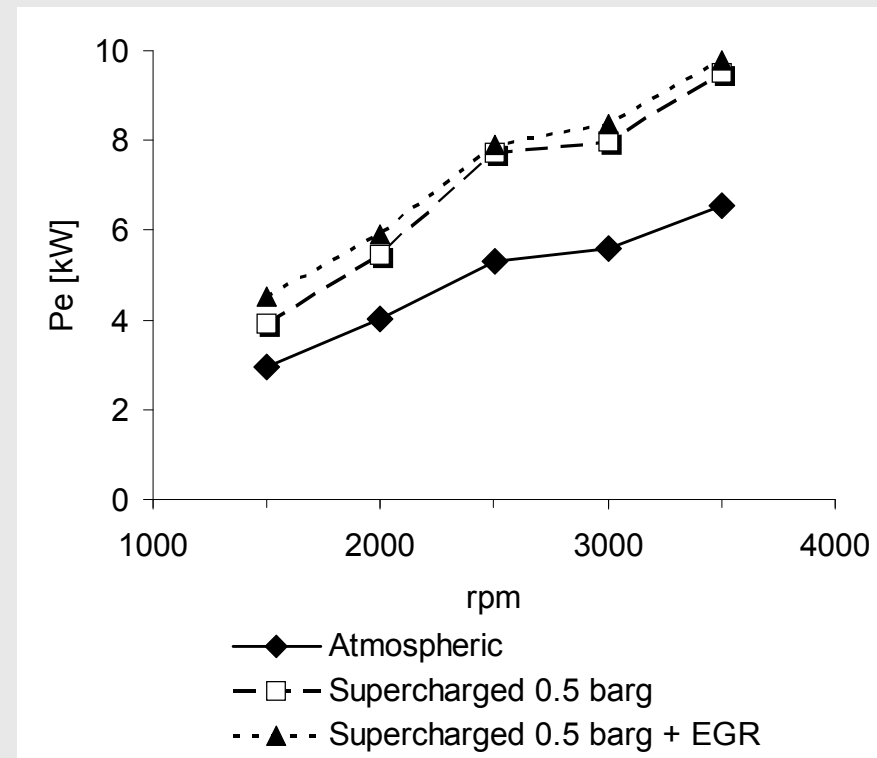
C&F 149:162-172

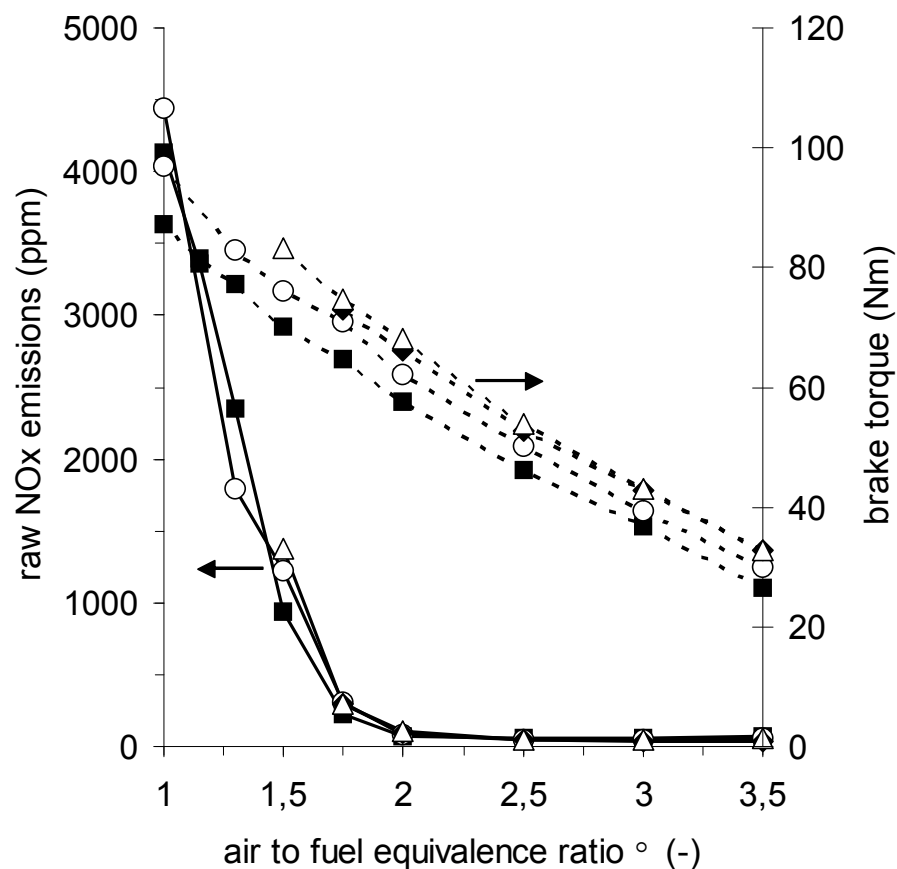


Rate constant	Pressure		
	0.1 MPa	0.5 MPa	1.0 MPa
$k_2/1.6$	2.63 m/s	2.19 m/s	
k_2	2.87 m/s	2.52 m/s	2.16 m/s
$1.6k_2$	3.04 m/s	2.79 m/s	2.46 m/s

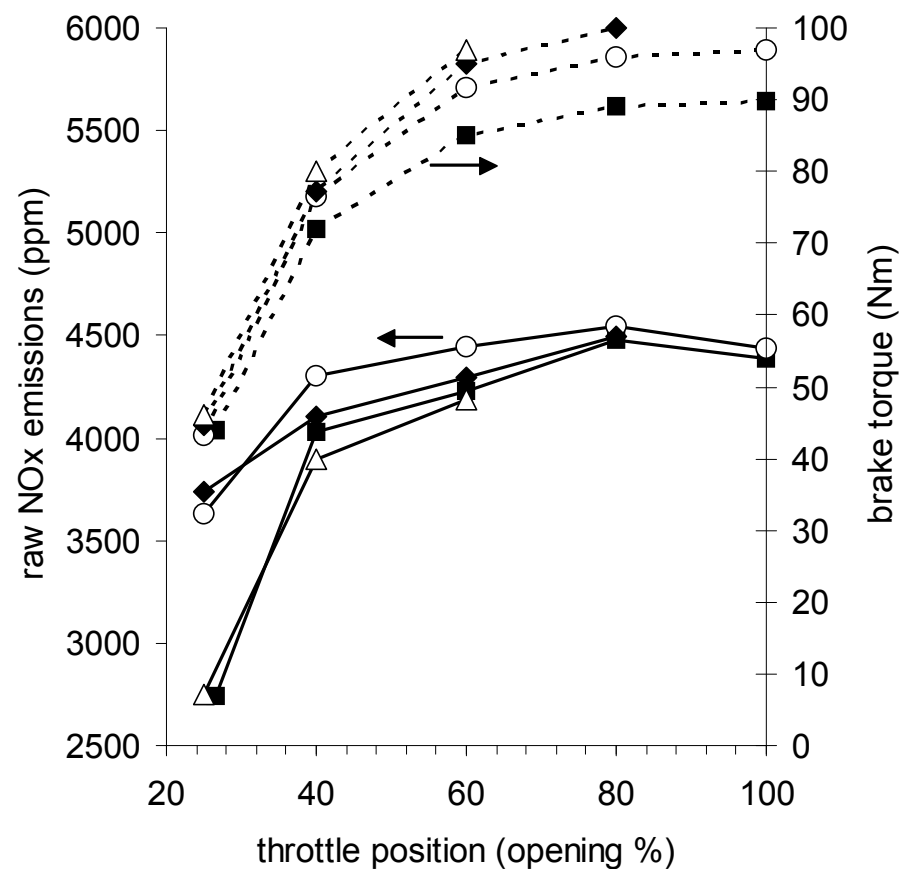
Other work

- Numerical: H₂ ICE code (quasi-dimensional) – see PhD
- Experimental
 - Supercharging+EGR on single cylinder engine
 - Variable valve timing on four cylinder engine
 - SAE World 2008 paper





- raw NOx at 4°ca IVO advance
- raw NOx at 16°ca IVO advance
- ◆— raw NOx at 28°ca IVO advance
- △— raw NOx at 40°ca IVO advance
- -■- - Brake torque at 4°ca IVO advance
- -○- - Brake torque at 16°ca IVO advance
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Thank you!

Further information:

See www.FloHeaCom.UGent.be/H2

By the way: BMW Hydrogen 7 comes to
Ghent University tomorrow at 2 pm!

