

## **Subtask 3.1D**

# **Measurement and Analysis of Integral Length Scale and Turbulence Viscosity in a Rapid Compression/Expansion Machine Using PIV**

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## Background and Motivation of the Study - 1 of 2

- The integral length scale is one of the important factors to characterize the turbulence in engine cylinders.
- ▶  $\varepsilon = C' k^{3/2} / L$        $k$  : turbulence kinetic energy  
 $\nu_t = C_\mu^{1/4} k^{1/2} L$        $\varepsilon$  : turbulence kinetic energy dissipation rate  
    $L$  : integral length scale  
    $\nu_t$  : turbulence kinematic viscosity  
    $C' = 0.169 \sim 0.201$ ,  $C_\mu = 0.09$
- ▶ Measurements of  $k$  and  $L$  provide all other turbulence characteristics.
- There have been many  $k$  data measured in engine cylinders with HWA, LDV or PIV. The measurements of  $L$ , however, have been limited in number.

## Background and Motivation of the Study - 2 of 2

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- Cross-Correlation PIV
  - ▶ Spatial measurement of velocity
  - ▶ The Taylor hypothesis is not necessary to obtain  $L$ .
  - ▶ Free from the influence of pressure and temperature
  - ▶ Popular and well-established in measuring velocity fields.
  - ▶ The measurement of  $L$  is neither well-examined nor established.
  - ▶ Better utilization of PIV should be developed.

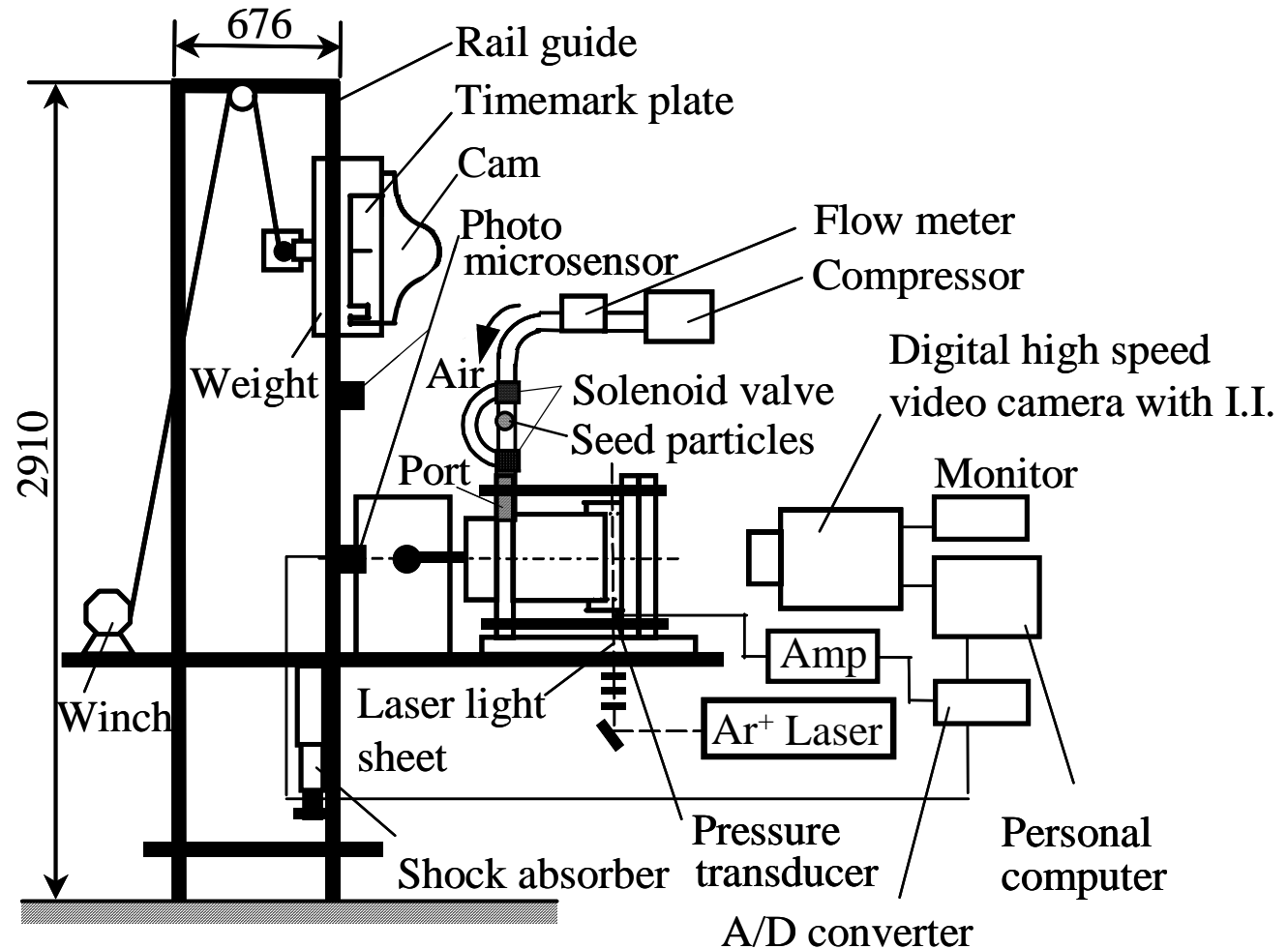
## Purpose of the Study

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- To improve the cross-correlation technique for reliable data of integral length scale  $L$  in PIV
- To compare turbulence characteristics measured in a cylinder of a rapid compression/expansion machine including the turbulence kinetic energy, integral length scale and turbulence kinematic viscosity with computational results and to validate the model for dilatation effect during compression/expansion

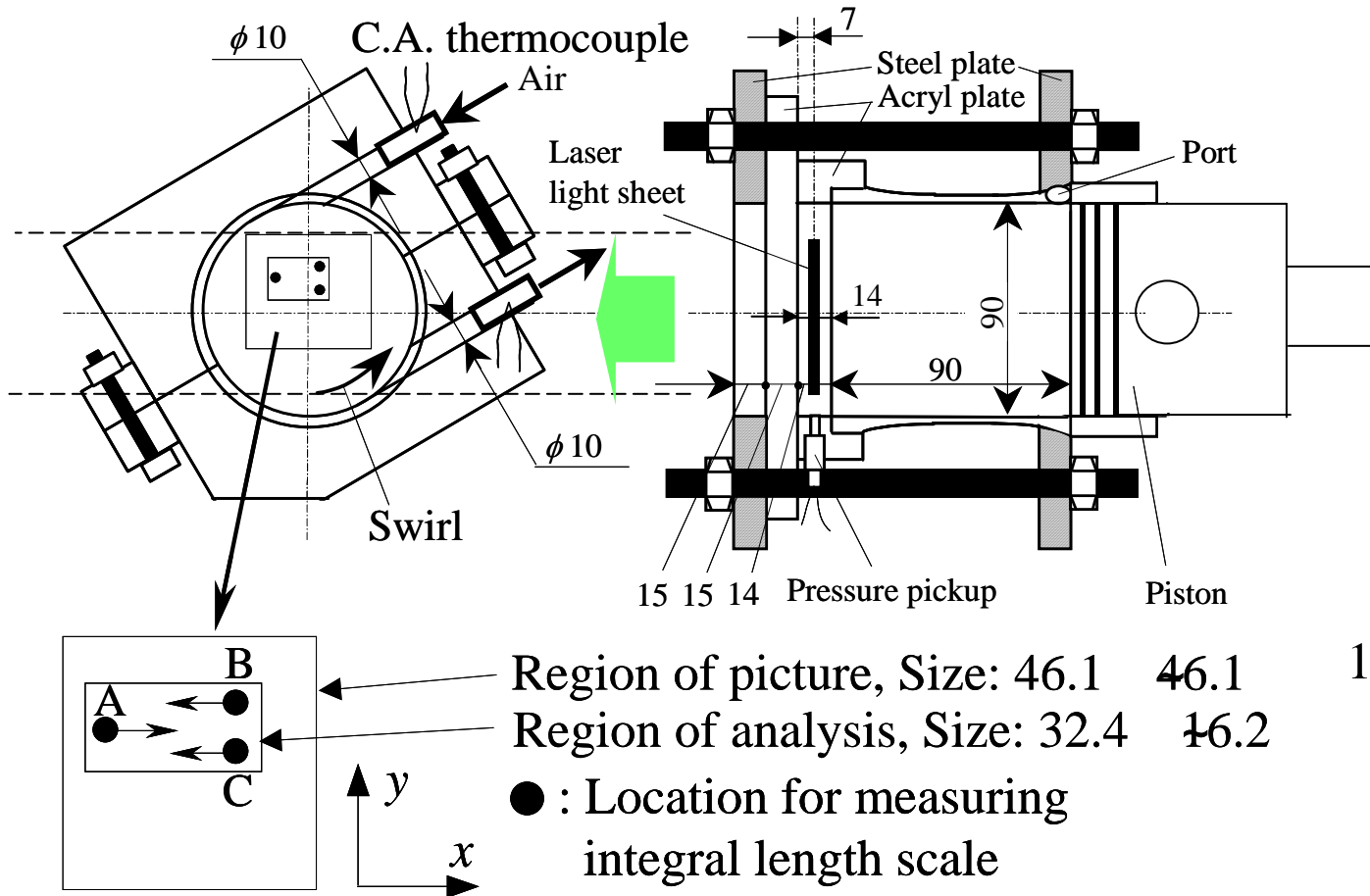
# Experimental Set-up

Equivalent  
engine speed:  
1110 rpm



Rapid compression/expansion machine and PIV system

# Experimental Set-up



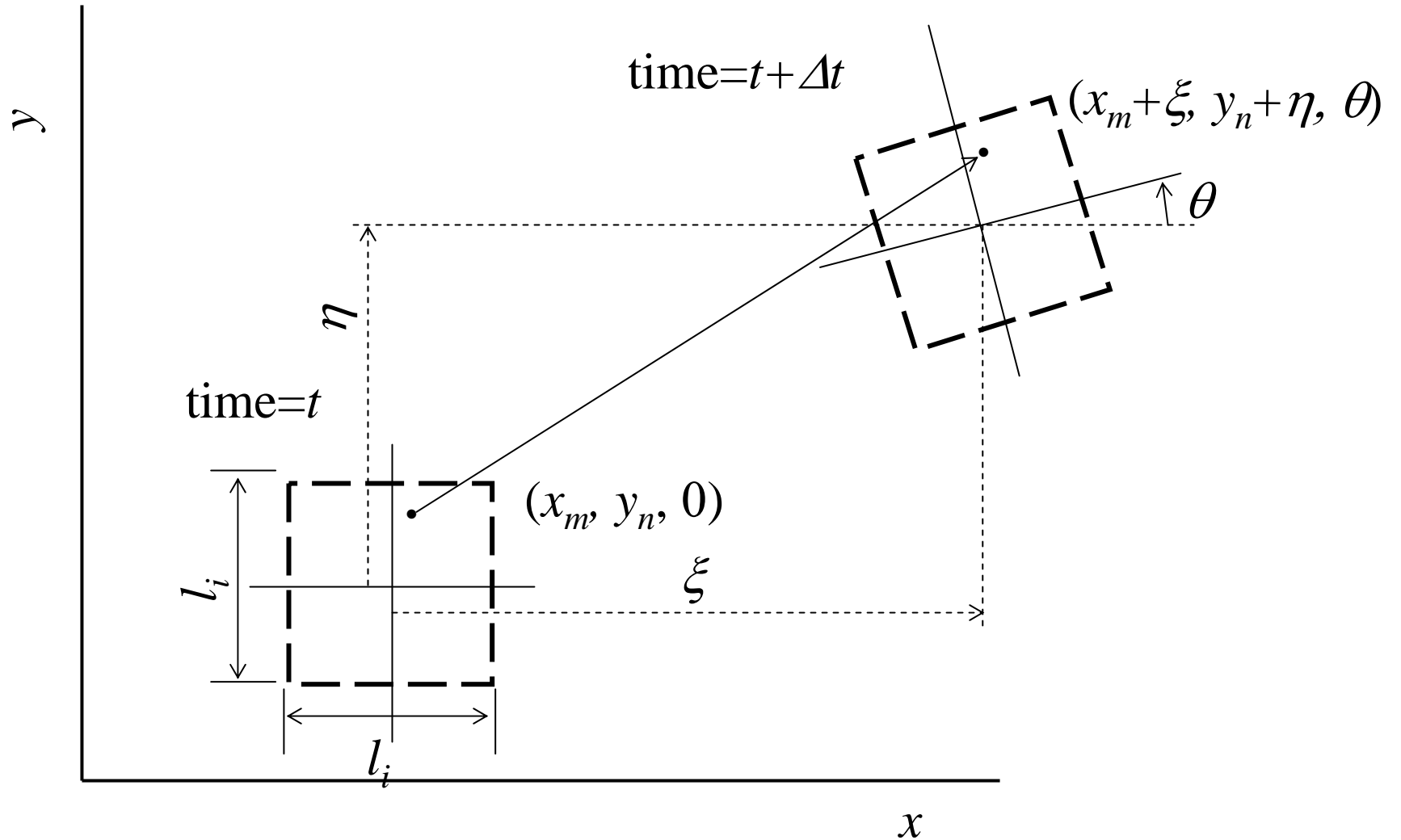
Seeding particles:  
plastic hollow sphere  
with average diameter  
of  $50 \mu\text{m}$

Thickness of Laser  
light sheet : 1 mm

1 pixel =  $0.18 \text{ mm} \times 0.18 \text{ mm}$

Cross sections of cylinder-piston assembly and three locations, A, B and C, for integral length scale measurements

# Improved Cross-Correlation Technique



# Improved Cross-Correlation

## ■ Cross-Correlation

$$R(t + \Delta t, \xi, \eta, \theta) = \frac{\sum_m \sum_n \{I(t, x_m, y_n, 0) \times I(t + \Delta t, x_m + \xi, y_n + \eta, \theta)\}}{\sqrt{\sum_m \sum_n I^2(t, x_m, y_n, 0)} \times \sqrt{\sum_m \sum_n I^2(t + \Delta t, x_m + \xi, y_n + \eta, \theta)}}$$

$I$ : local brightness of image,  $\theta$ : rotation angle

- $R_0(t+\Delta t, \xi_0, \eta_0, \theta_0)$  : maximum of  $R(t+\Delta t, \xi, \eta, \theta)$   
 $\xi_0, \eta_0$  : average parallel movement of gas blob of a template size  
 $\theta_0$  : average rotational angle of gas blob of a template size



# Definition of Turbulence Intensity

- Turbulence intensity:  
Assumption of isotropic turbulence gives,

$$u^*(x, y) = \sqrt{\frac{3}{2l_m^2} \int_{-l_m/2}^{l_m/2} \int_{-l_m/2}^{l_m/2} \{\hat{u}(x + \xi, y + \eta)\}^2 d\xi d\eta}$$

$$\hat{u}(x, y) = |\vec{u}(x, y) - \vec{U}(x, y)|$$

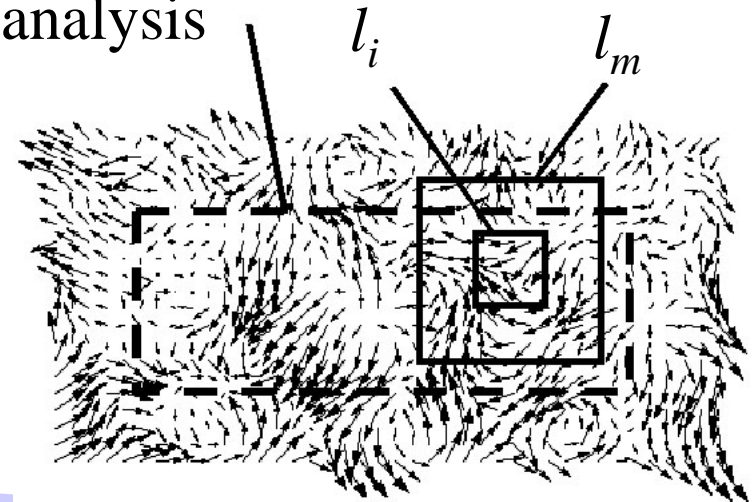
$u$  : local velocity

$U$ : spatial average velocity

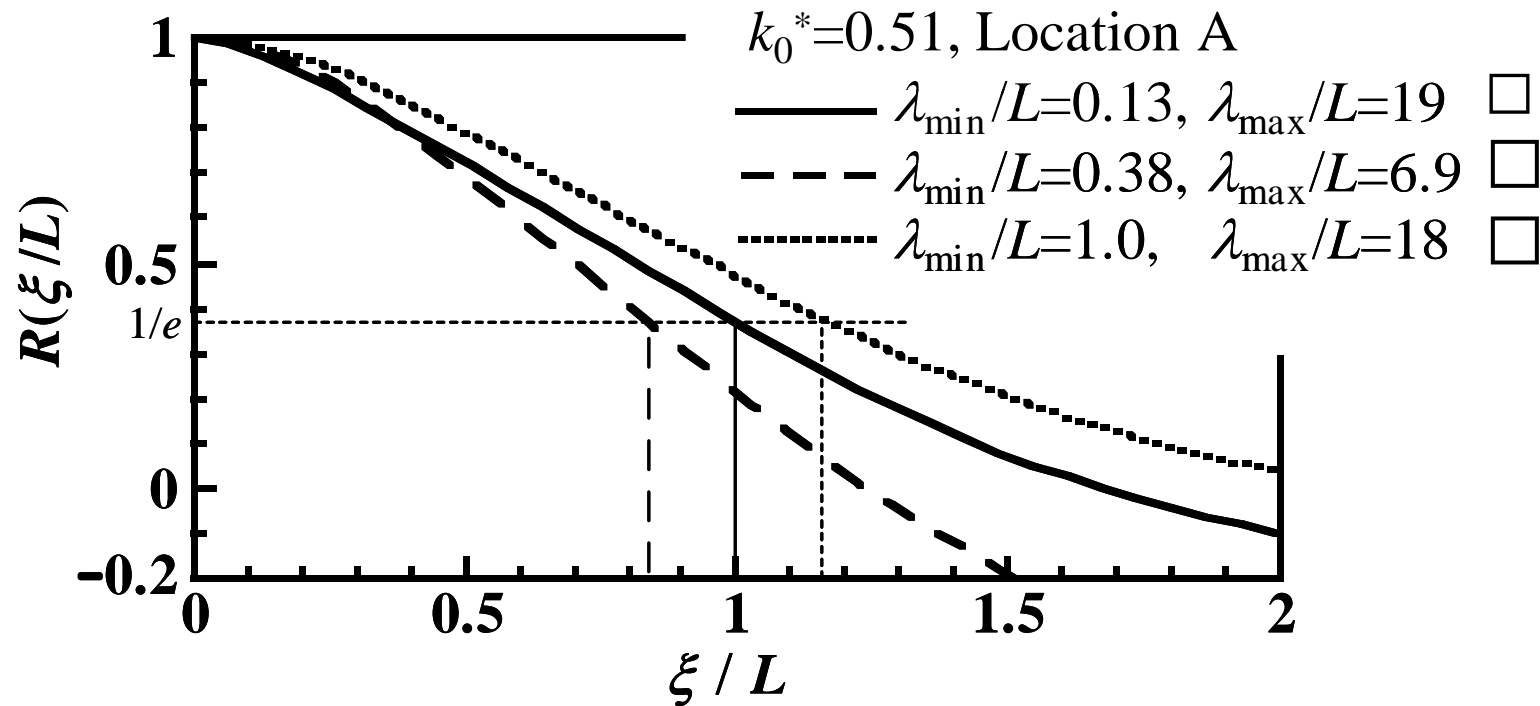
$l_i$ : size of square template for  $u$

$l_m$ : size of square template for  $U$

Region of  
analysis



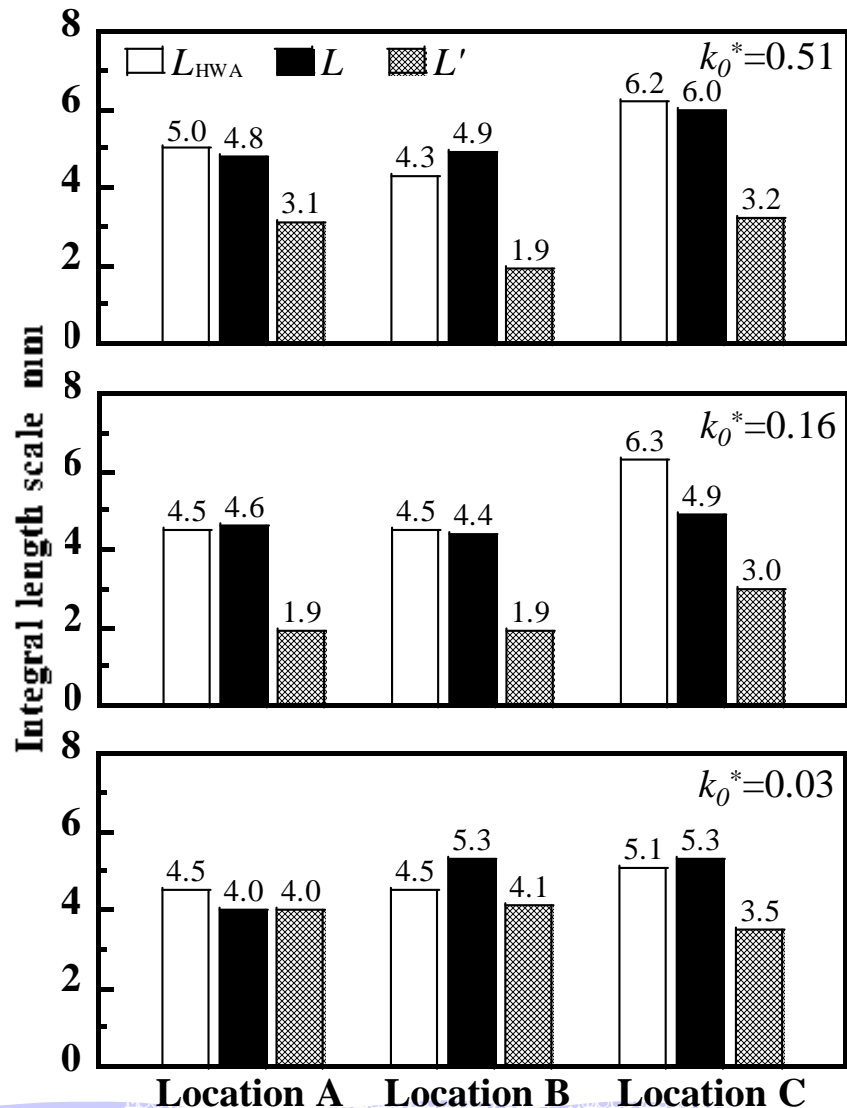
# Estimation of Errors in Integral Length Scale measurements



$\lambda_{\min}$ : min. wave length,  $\lambda_{\max}$ : max. wave length,  $L$ : integral length scale

- Spatial velocity data obtained from HWA data using Taylor hypothesis for steady flow at BDC position; the range of wave length is enough
- cut longer wave length
- cut shorter wave length

# Comparison of Integral Length Scale



Integral length scales measured in steady flow test at BDC position by three different methods;

$L_{HWA}$ : measured with HWA

$L$  : taking  $\theta$  into consideration

$L'$  : leaving  $\theta$  out of consideration ( $\theta=0$ )

$$k_0^* = k_0 / C_m^2$$

## Standard $k$ - $\varepsilon$ two equation turbulence model

$$\frac{\partial(\rho k)}{\partial t} + \nabla \cdot (\rho \vec{u} k) = D_k + S_k$$

$$D_k = \nabla \cdot \left( \frac{\mu_e}{\sigma_k} \nabla k \right)$$

$$\frac{\partial(\rho \varepsilon)}{\partial t} + \nabla \cdot (\rho \vec{u} \varepsilon) = D_\varepsilon + S_\varepsilon$$

$$D_\varepsilon = \nabla \cdot \left( \frac{\mu_e}{\sigma_\varepsilon} \nabla \varepsilon \right)$$

$$S_k = 2\mu_t S_{ij} S_{ij} - \frac{2}{3}(\nabla \cdot \vec{u})\{\mu_e(\nabla \cdot \vec{u}) + \rho k\} - \rho \varepsilon$$

$$S_\varepsilon = \frac{\varepsilon}{k} \left[ 2C_1\mu_t S_{ij} S_{ij} - \frac{2}{3}(\nabla \cdot \vec{u})\{C_1'\mu_e(\nabla \cdot \vec{u}) + C_1''\rho k\} - C_2\rho \varepsilon \right] + \frac{C_3\rho \varepsilon(\nabla \cdot \vec{u})}{\text{dilatation term}}$$

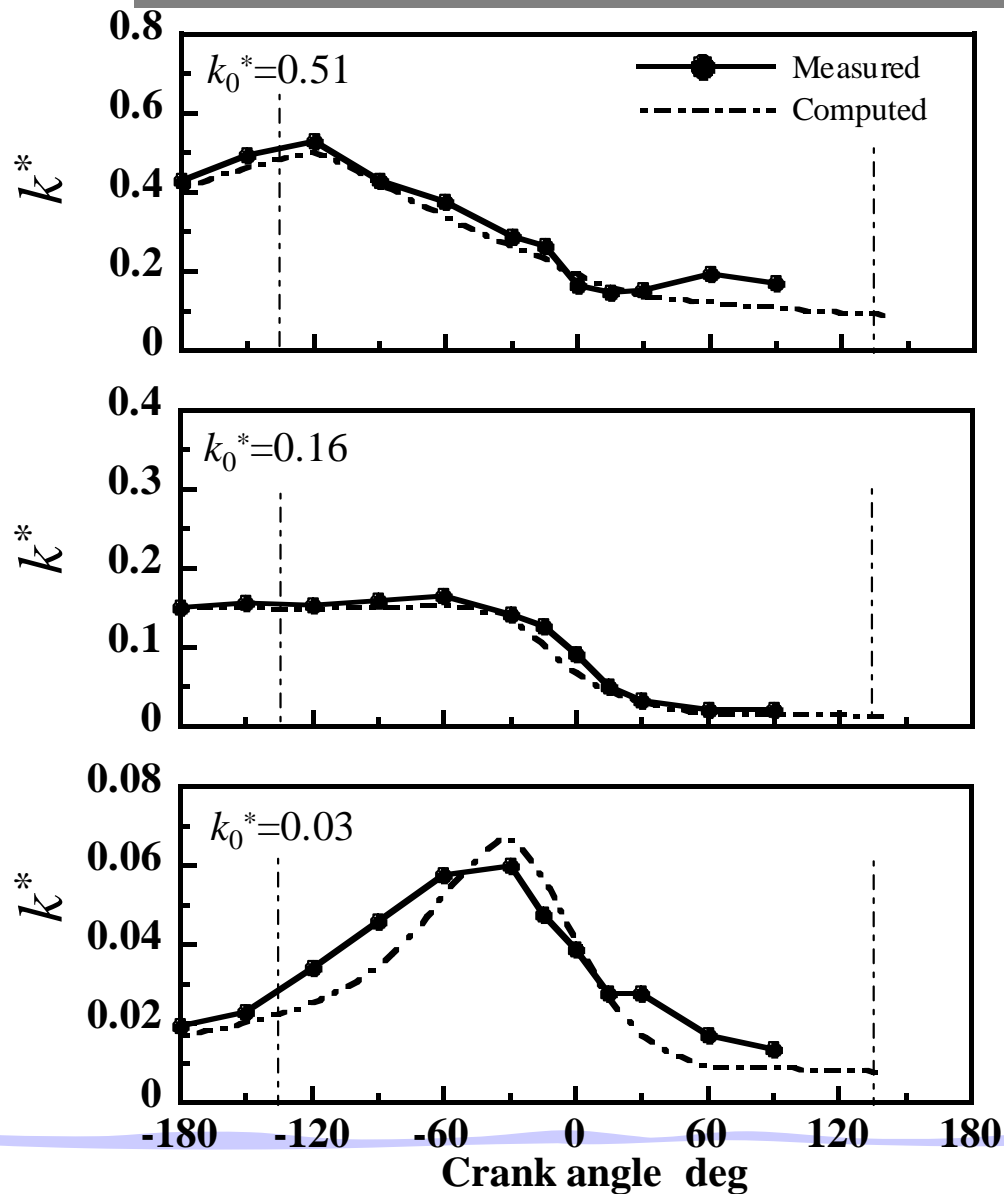
$$S_{ij} = \frac{1}{2} \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

$$C_1=1.44 \quad C_1'=1.32 \quad C_1''=4.50 \quad C_2=1.92$$

$$\nabla \cdot \vec{u} = S_{ii}$$

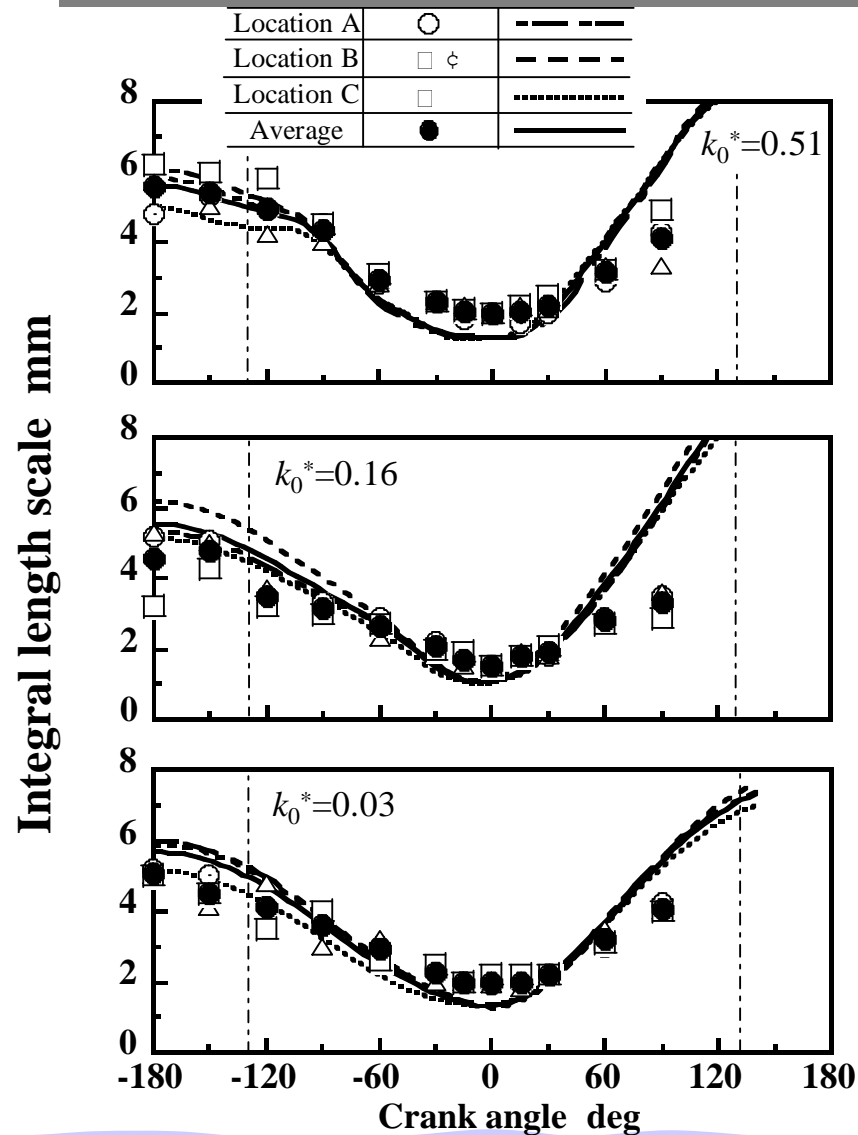
$C_3=1.0$  : Morel-Mansour model for one-dimensional comp./exp.

# Comparison of Turbulence Kinetic Energy

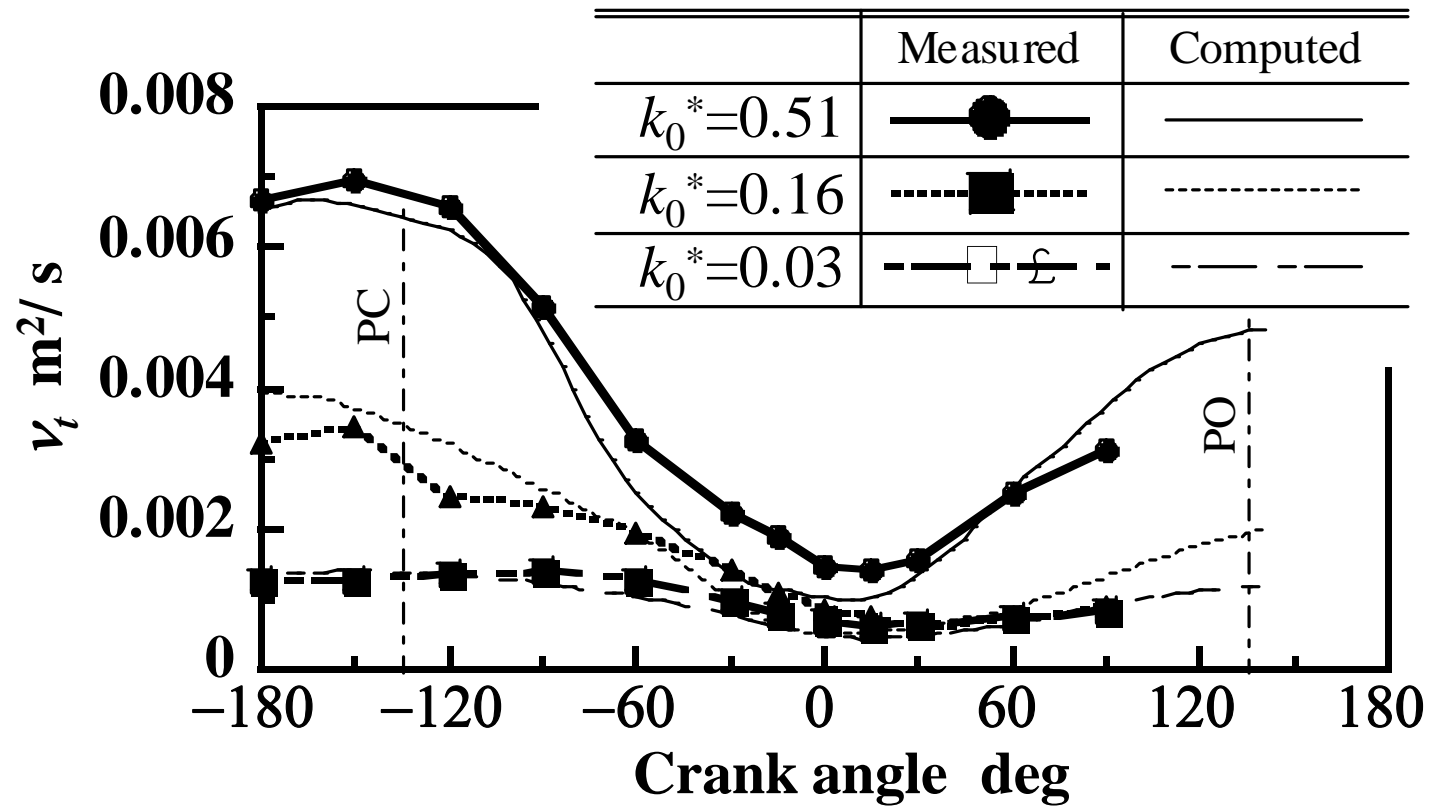


Measured and computed  
turbulence kinetic energies

# Comparison of Integral Length Scale



Measured and computed  
integral length scales



Measured and computed turbulence kinematic viscosity

## Conclusions

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- Average rotation of a template in addition to average parallel movement improves the accuracy of integral length scale measurements when making cross-correlation of brightness of PIV image.
- Errors in measurement of integral length scale due to the limited range of wave length in PIV are estimated. The result shows that the errors are not considerable from a practical stand point.
- Measured and computed turbulence characteristics, including turbulence kinetic energy, integral length scale and turbulence kinematic viscosity, were compared for swirling turbulent flows in a rapid compression/expansion machine. The results show a good agreement and validate the dilatation effect.



## Conclusions - cont'd

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- The improved cross-correlation technique will be a better tool for providing turbulence characteristics in engine combustion chamber, in which compression/expansion is not always one-dimensional including compression of unburned gas during combustion.



**Thank you for your attention**

