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- **Active Fuel Design and Management
for Homogeneous Charge
Compression Ignition (HCCI)**

- **Prof. Huang Zhen**
-
- **Shanghai Jiao Tong University**

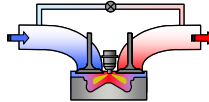
Shanghai Jiao Tong University (SJTU)



Vehicles in SJTU

Clean Engine Combustion

HCCI, PCCI, LTC

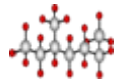


Energy strategy and policy

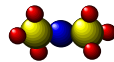
LCA, Future fuel scenario

New energy conversion system

Free Piston Linear Alternator



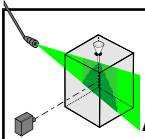
Alternative Fuels:



Coal Based fuel, Bio-fuels, Synthetic fuels, Hydrogen

Fuel injection and Spray

Atomization, Spray characteristics



Optical Measurement and Simulation of Combustion

PDPA, PIV, High speed photography, CFD, Chemkin, HCT

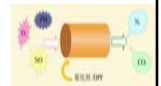


Urban Air Pollution Control

*Pollutants transport and dispersion,
Ultrafine Particle, Environmental impacts*

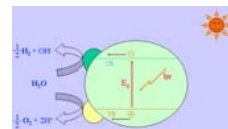
Engine Aftertreatment

*Catalyst design,
NOx-PM removal, SCR*



Hydrogen Production

Photocatalysts design, Solar energy

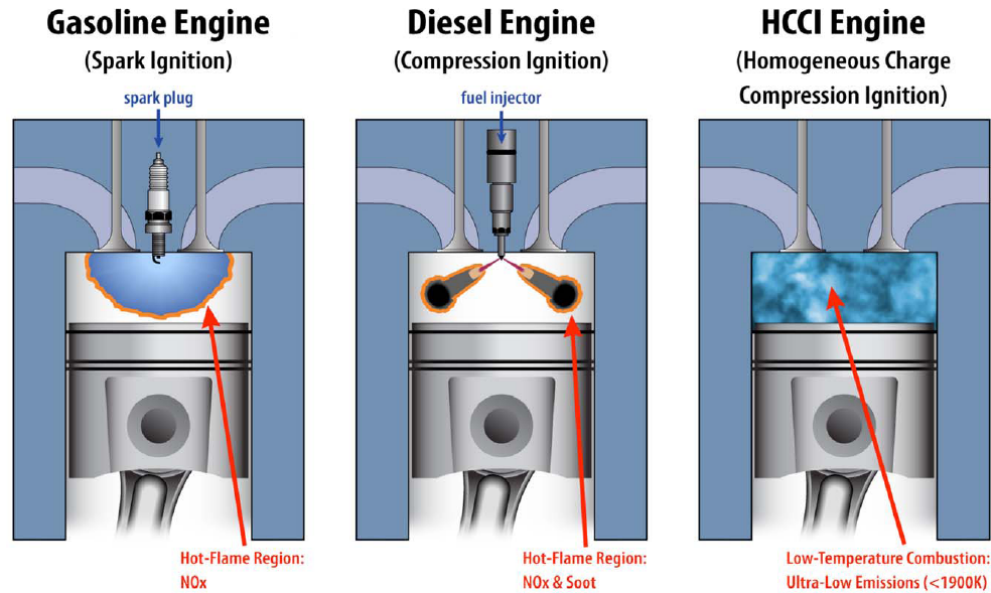


Presentation

Outline

1. **Active Fuel Design for HCCI**
2. **Active Fuel Design and Management for Hybrid Combustion**
3. **Conclusions**

HCCI Challenges



Source: www.erc.wisc.edu/symposiums/2007_Symposium/June%206%20PM-1/Mueller.pdf

- There are some difficulties and obstacles that must be overcome before applying HCCI combustion to internal combustion engine.

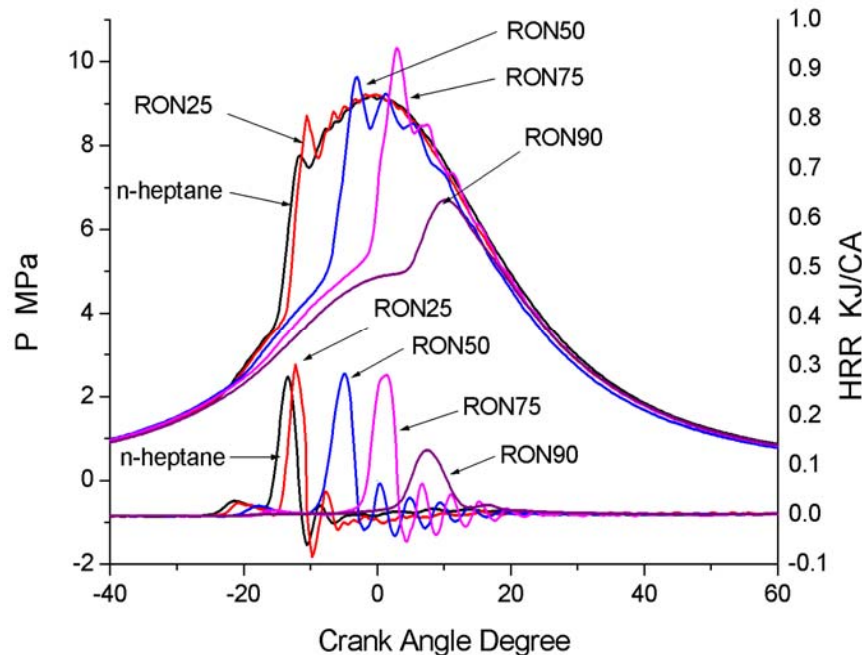
- Homogeneous mixture preparation
- Ignition control over a range of loads and speeds
- Limitation in power output
- Unburned HC and CO



Control method

- FTM (Fast Thermal Management)
- VCR (Variable Compression Ratio)
- VVA (Variable Valve Actuation)
- **AFDM (Active Fuel Design & Management)**

Effect of octane number and cetane number on HCCI combustion



$n = 1800 \text{ r/min}$ $\Phi = 0.35$

coolant temp.: 85 degree

92 degree (RON 90)

Fuel with high cetane number:

- Early auto ignition, deterioration of thermal efficiency
- Knocking problem at high load
- Limitation in power output

Fuel with high octane number:

- Difficult to compression ignition,
- Misfire or partial burn at low load.
- Limitation in power output

In terms of fuel properties, neither high cetane nor high octane number fuel is suitable for HCCI in wide operating range.

Active Fuel Design for HCCI

Active fuel design

High octane fuel

High cetane fuel



Variable cetane and octane number for optimizing fuel properties suitable for HCCI



To control ignition and combustion phase

To extend engine load

To reduce exhaust emissions

Active Fuel Design and Management for HCCI

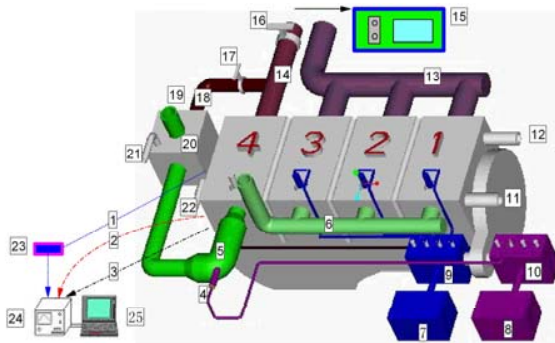
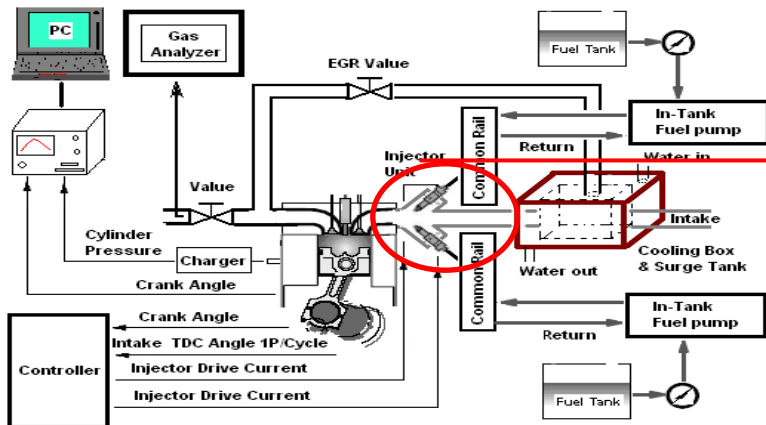
Active fuel design

iso octane

n-haptane

Fuel injection management

Port Injection



Engine Type

4-stroke, water-cooled

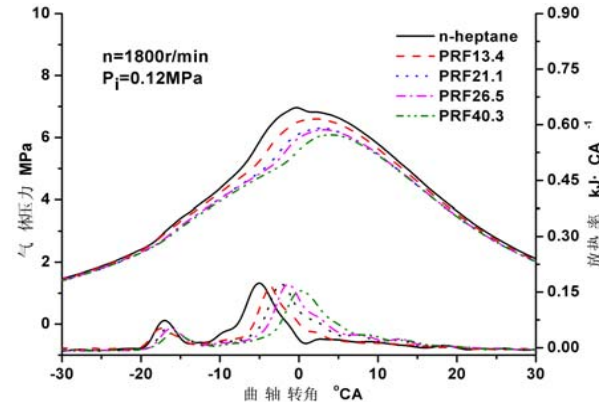
Cylinder diameter/stroke

98mm×105mm

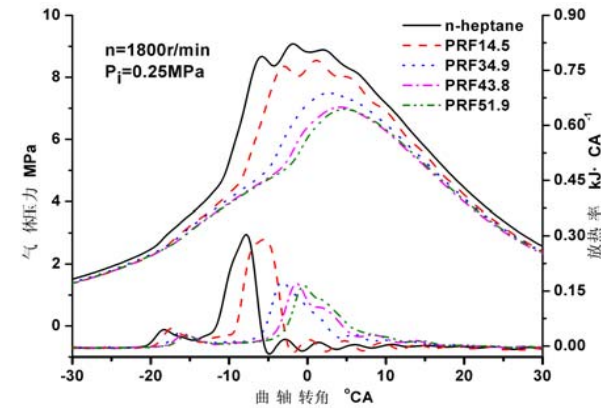
Compression ratio

18.5

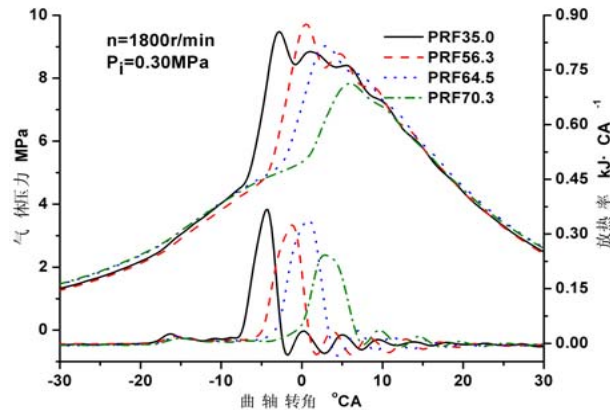
means of AFDM



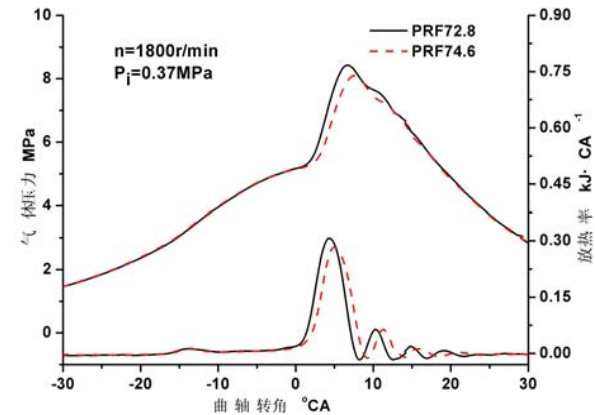
Pi 0.12MPa



Pi 0.25MPa



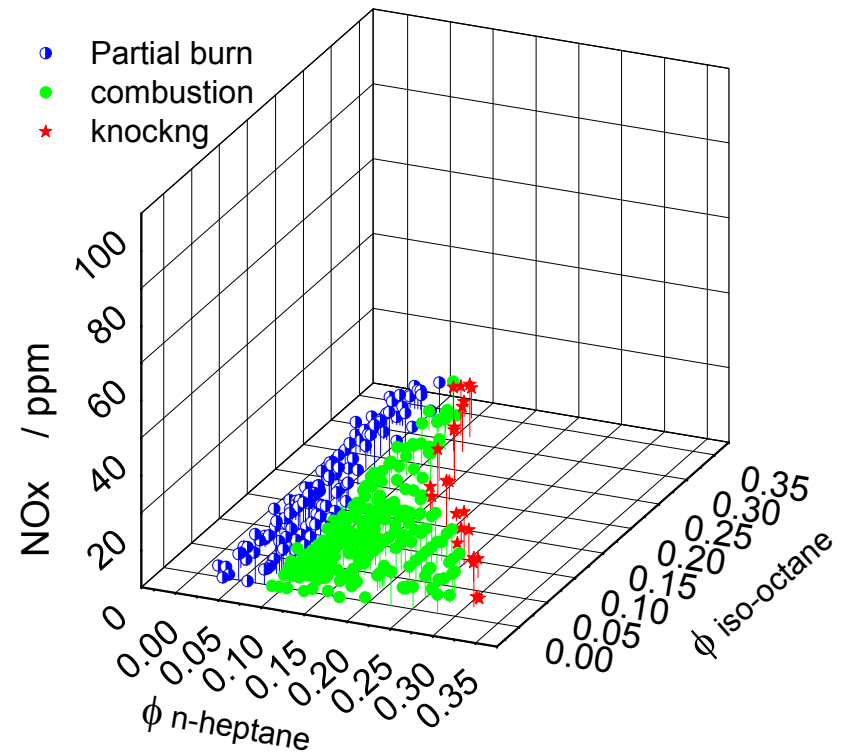
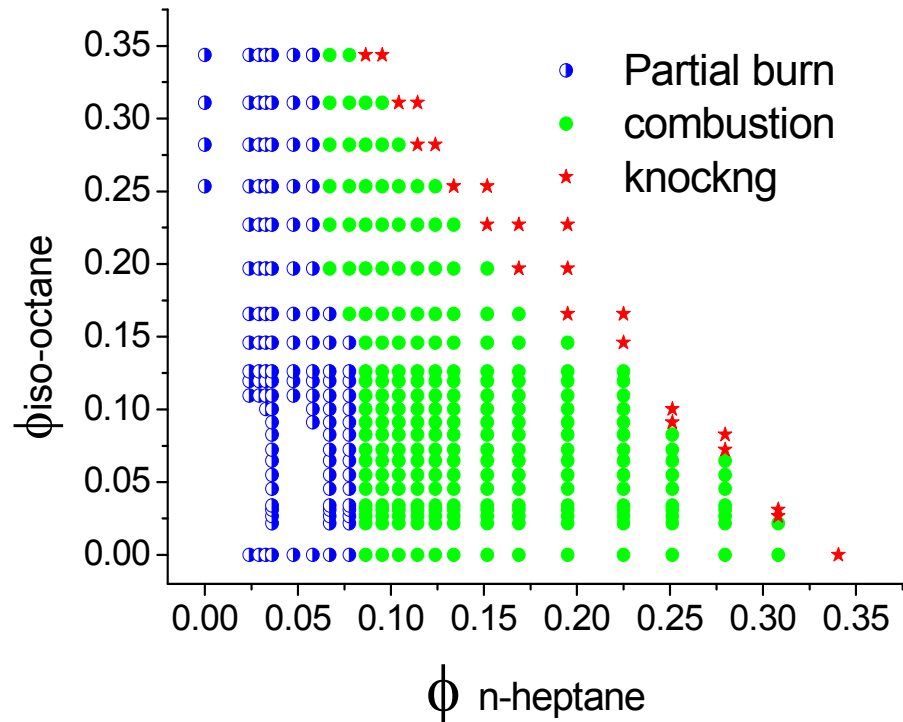
Pi 0.30MPa



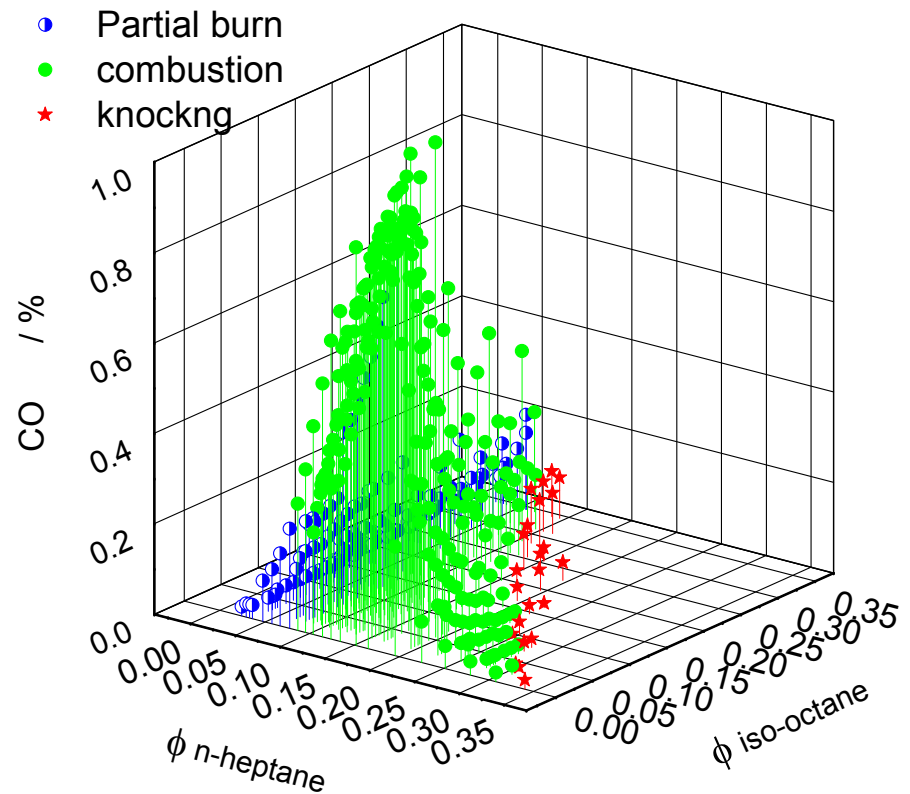
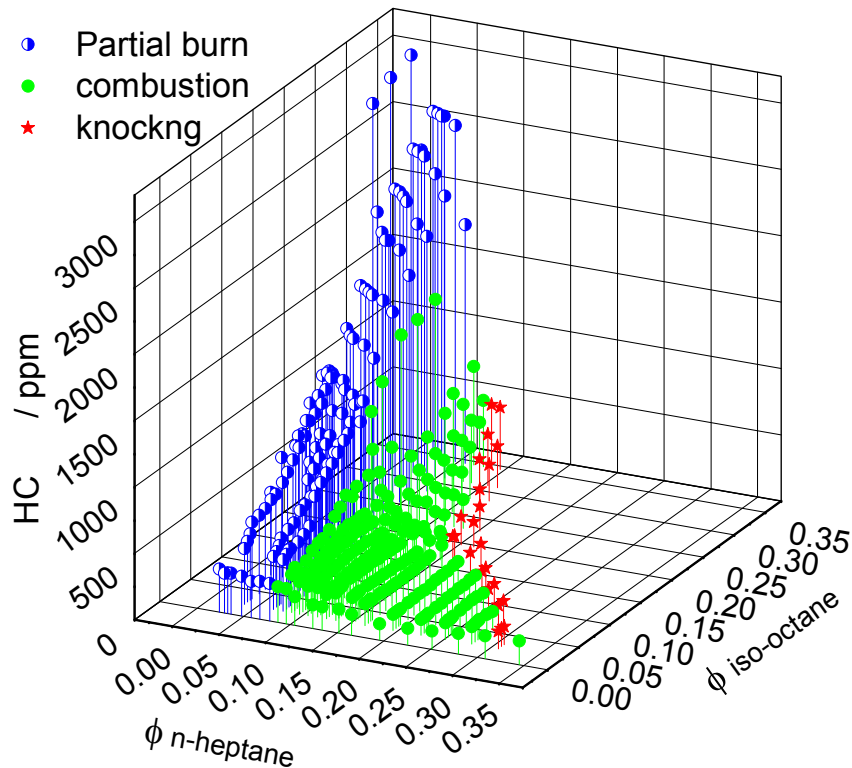
Pi 0.37MPa

AFDM

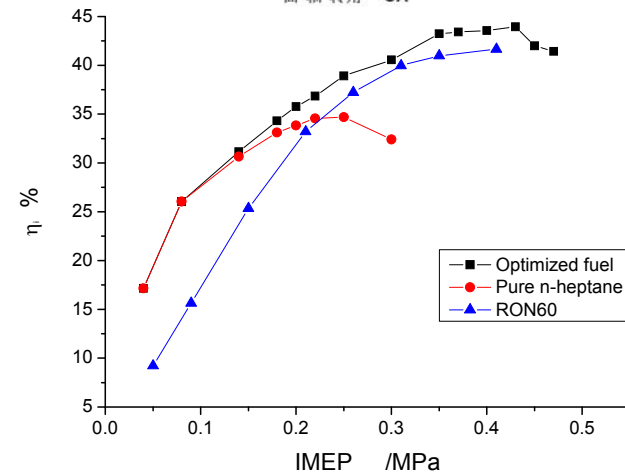
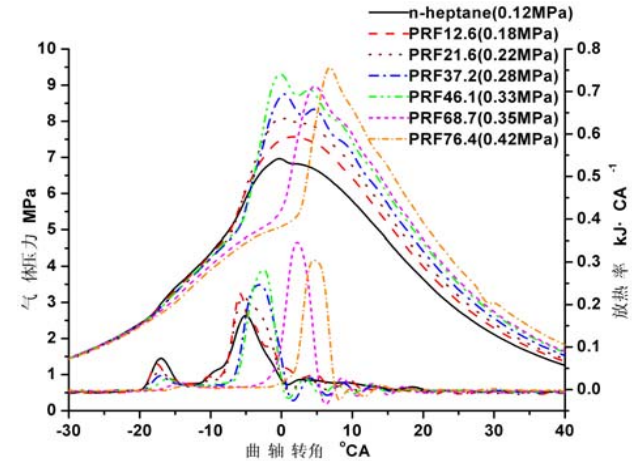
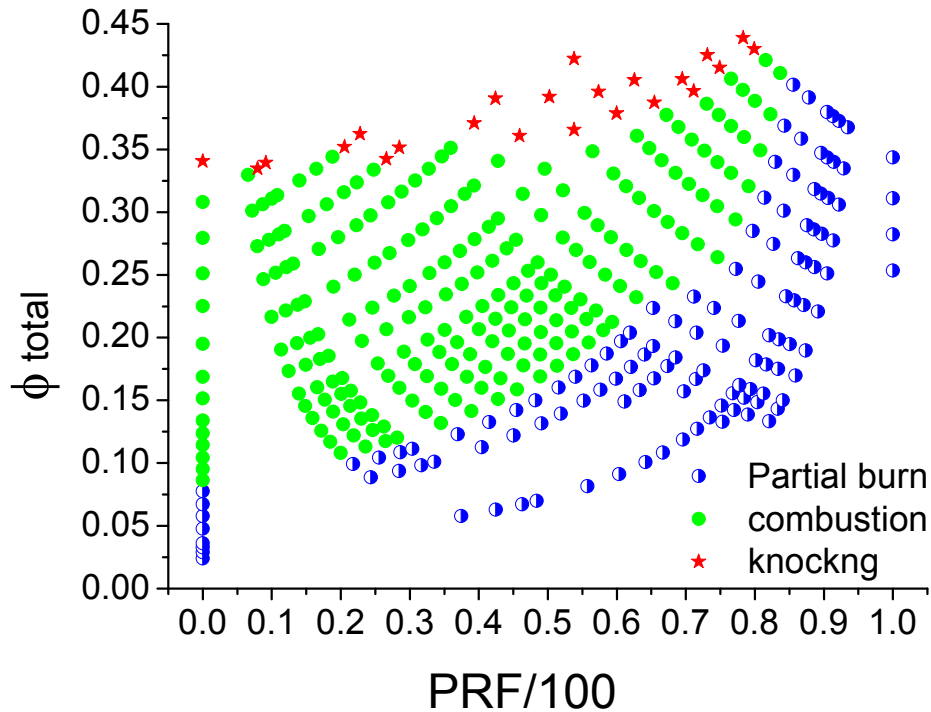
(parametric investigation)



CO and HC emission by means of the AFDM



by the AFDM



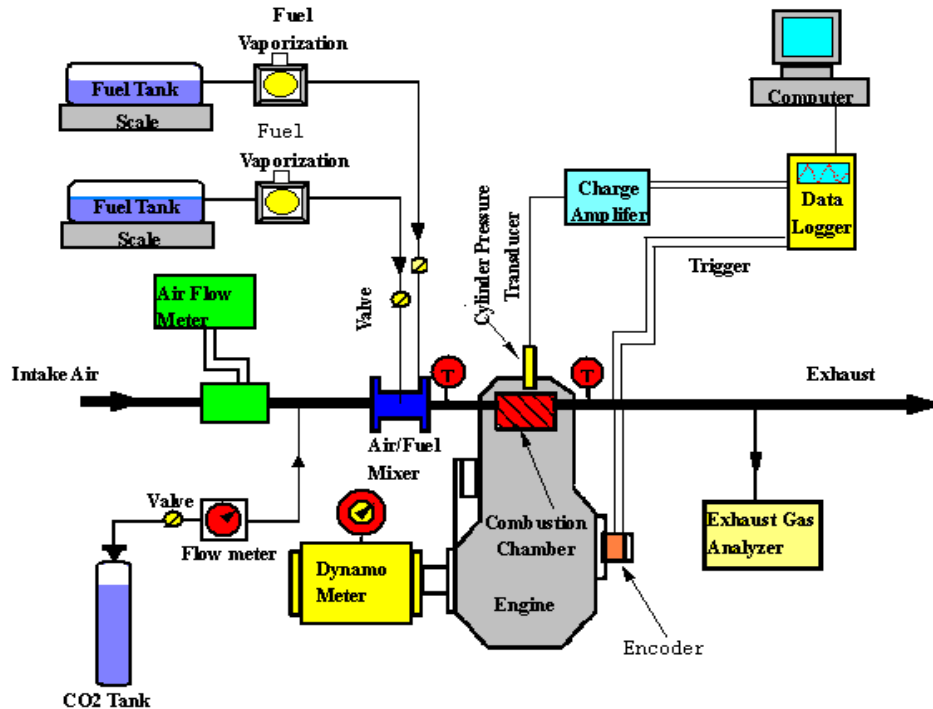
According to engine load, by means of parametric investigation and optimization of fuel blending ratio through dual fuel port injection, engine load is increased by 80%. Thermal efficiency is improved. HC and CO emissions decrease.

Active Fuel Design and Management for HCCI

Active fuel design

DME

LPG



Engine Type

Natural aspiration

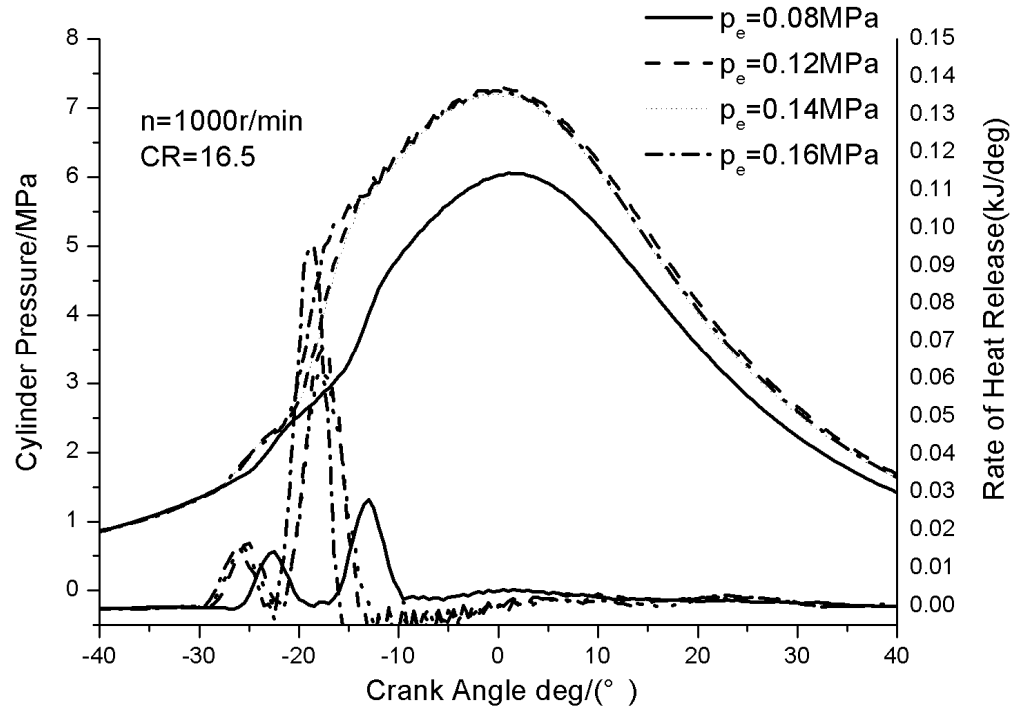
Cylinder diameter/stroke

135mm×145mm

Compression ratio

16.5, 12.2

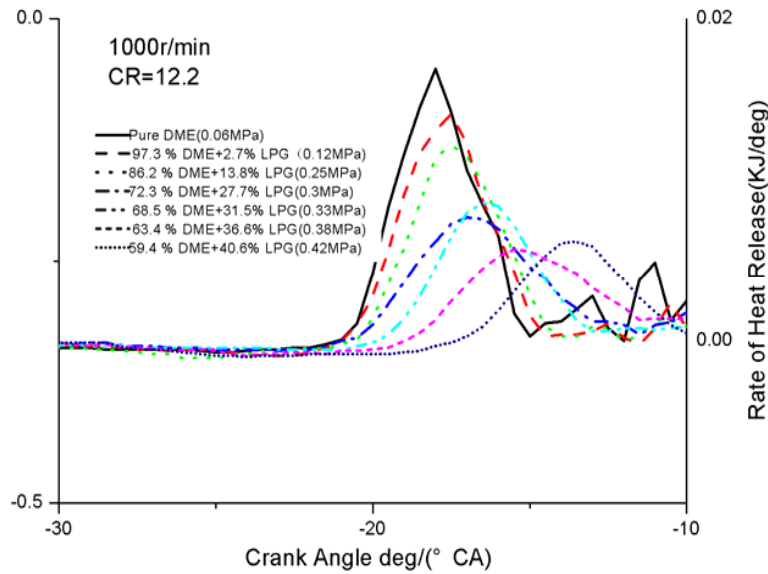
DME HCCI Combustion



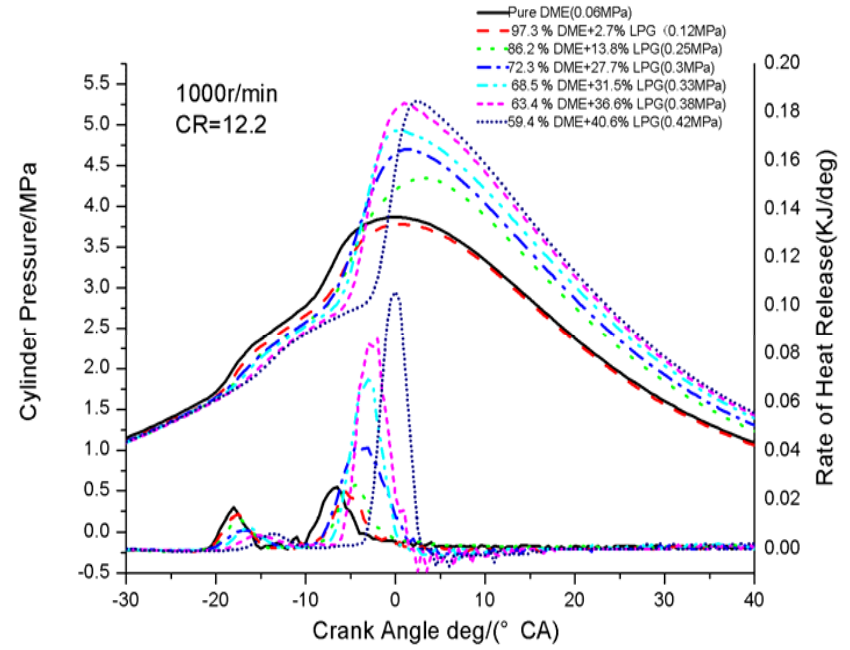
Variation of cylinder pressure and heat release rate with engine load

For HCCI combustion of DME, engine operation range is very narrow.

HCCI combustion with optimized DME/LPG ratio



Low-temperature kinetic reactions

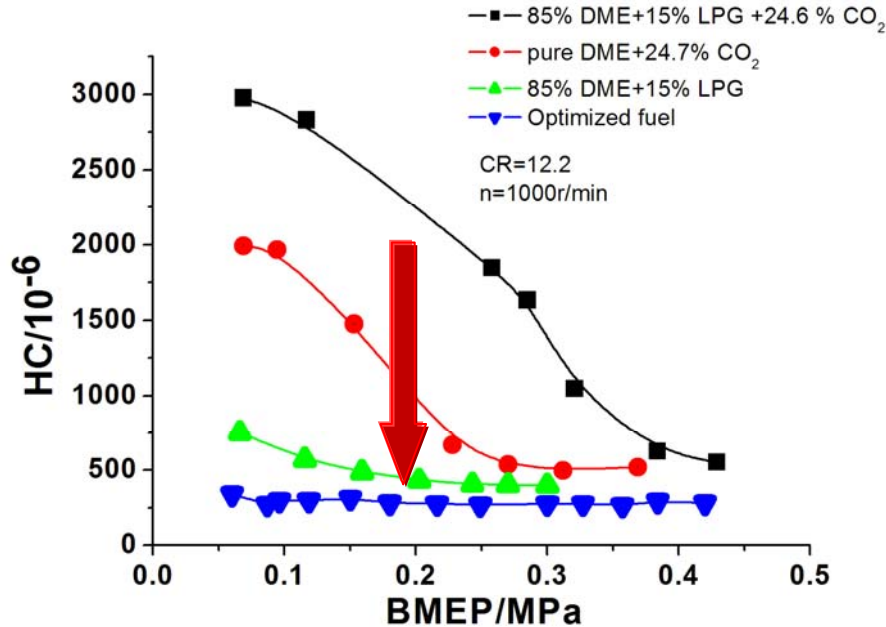


High-temperature reactions

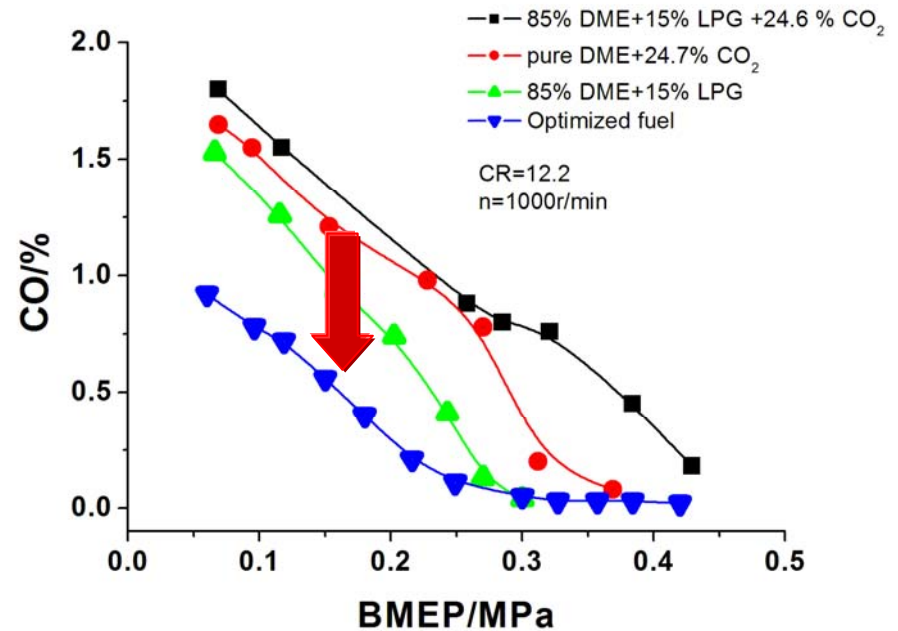
Variations of cylinder pressure and heat release rate with engine load at optimized DME/LPG blending ratio

Through parametric investigation, optimal HCCI combustion was obtained by variable DME/LPG blending ratio.

Beneficial effect of optimized DME/LPG ratio on engine exhaust emissions

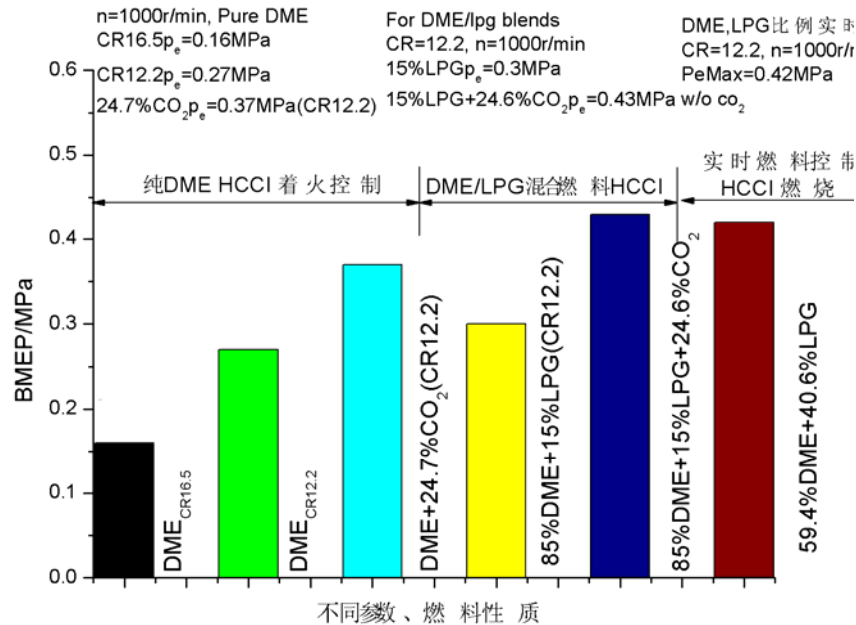


a HC

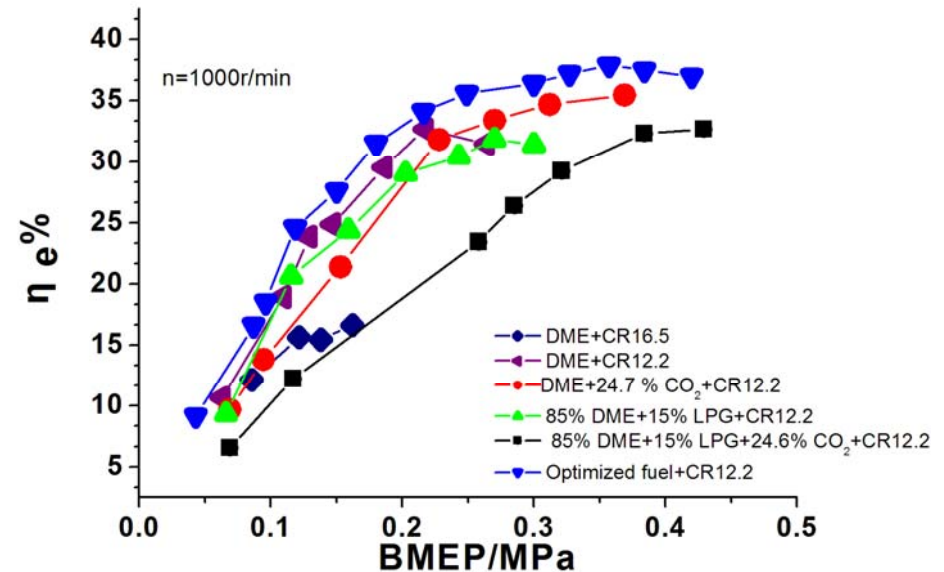


b CO

Beneficial effect of optimized DME/LPG ratio on engine thermal efficiency and load extending



Extend of engine load



Improvement of engine thermal efficiency

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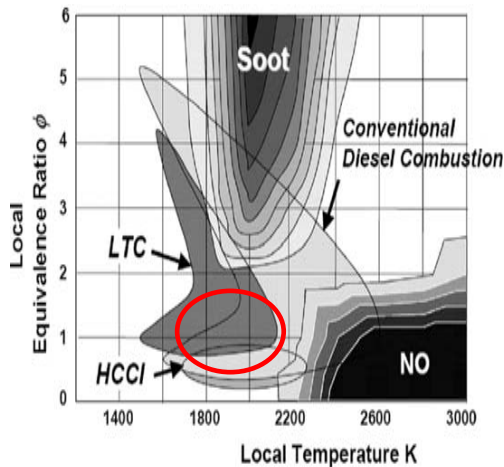
Active Fuel Design and Management

Active fuel design

Octane number

Cetane number

Fuel injection management



Source: Neely, G.D

Full load with high efficiency
and ultra-low emissions

Port injection

+

In cylinder
direction injection

HCCI

+

Third stage combustion

Variable octane number

Direct injection timing

Premixed ratio

Ignition timing

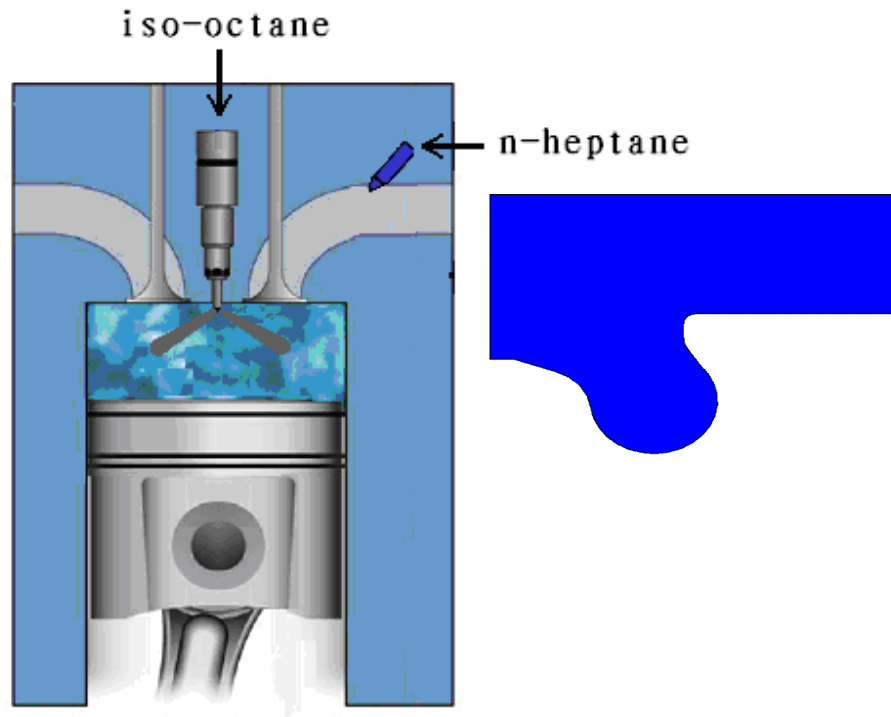
Combustion phase

Distributed heat release – hybrid combustion

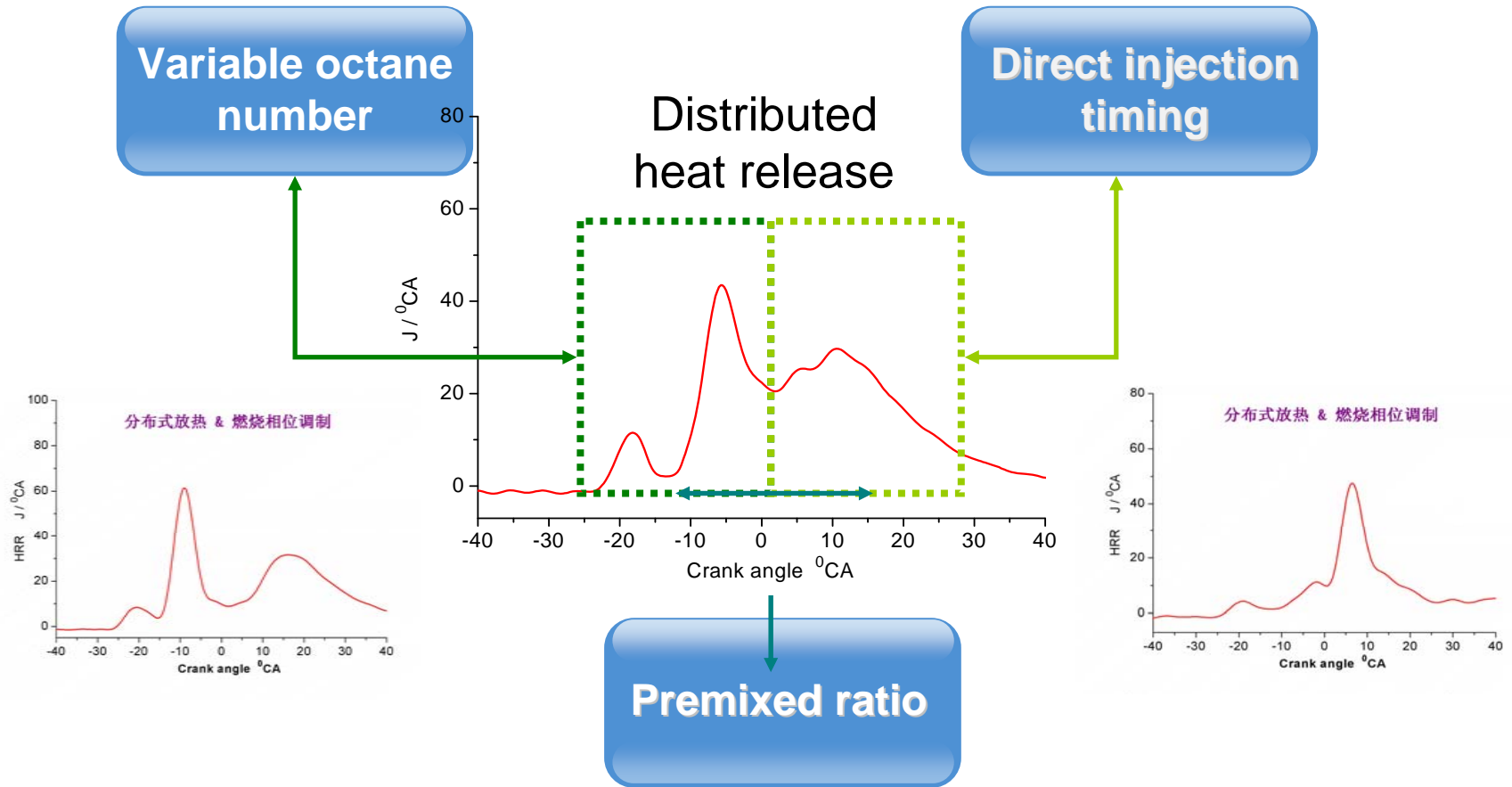
Active Fuel Design and Management

Port injection – variable octane number, Direct injection - n-heptane

HCCI/DI Engine



Active Fuel Design and Management

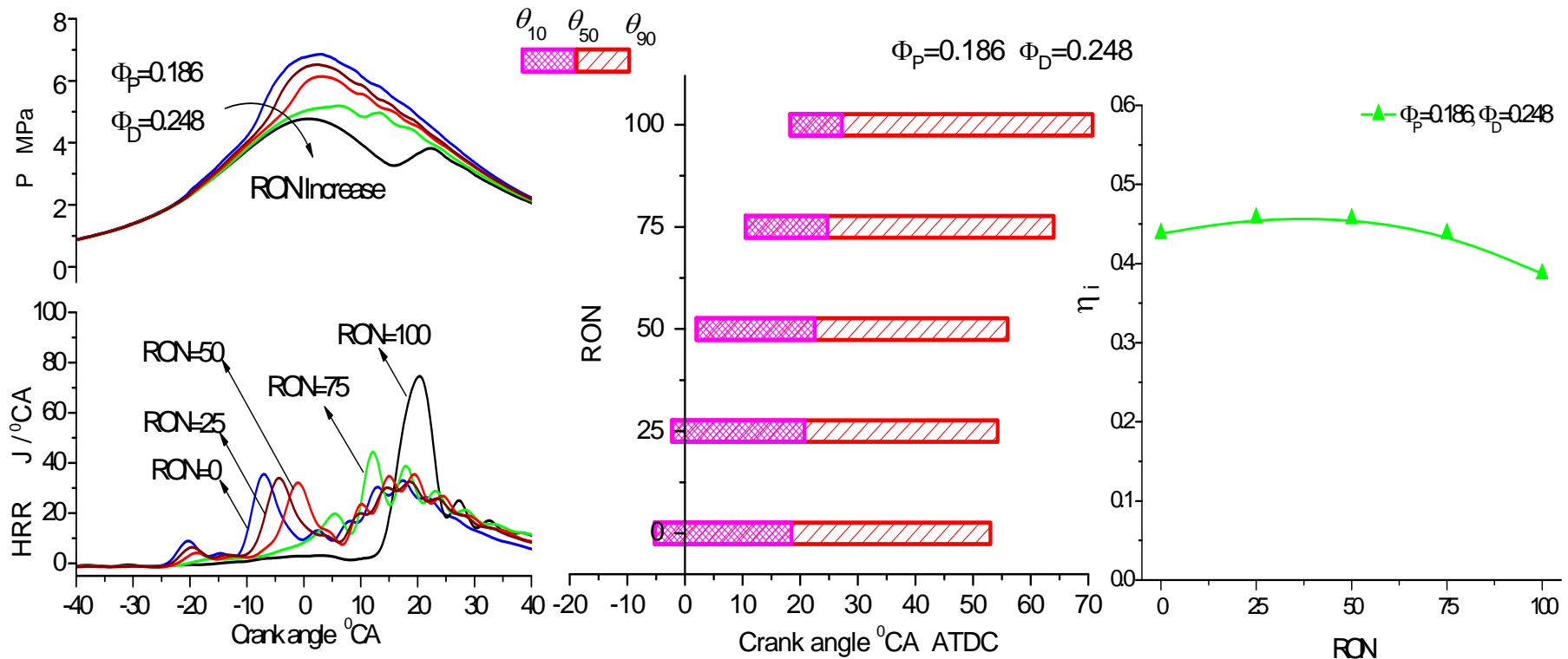


Heat release and combustion
mode modulation



Combustion and
emission control

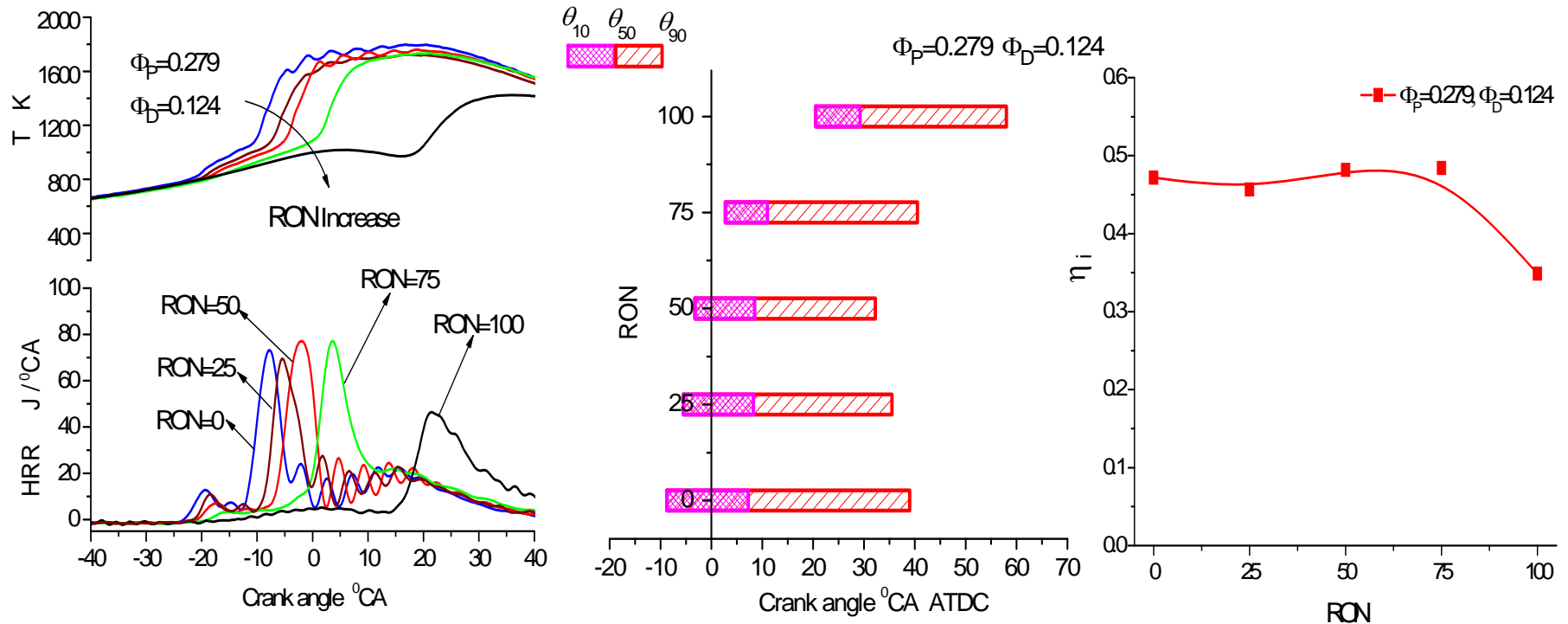
Effect of Fuel Octane Number of Port Injection on Indicated Thermal Efficiency



Port injection – variable octane number, Direct injection - n-heptane

Fuel octane number of port injection has importance influence on distributed heat release and combustion pattern.

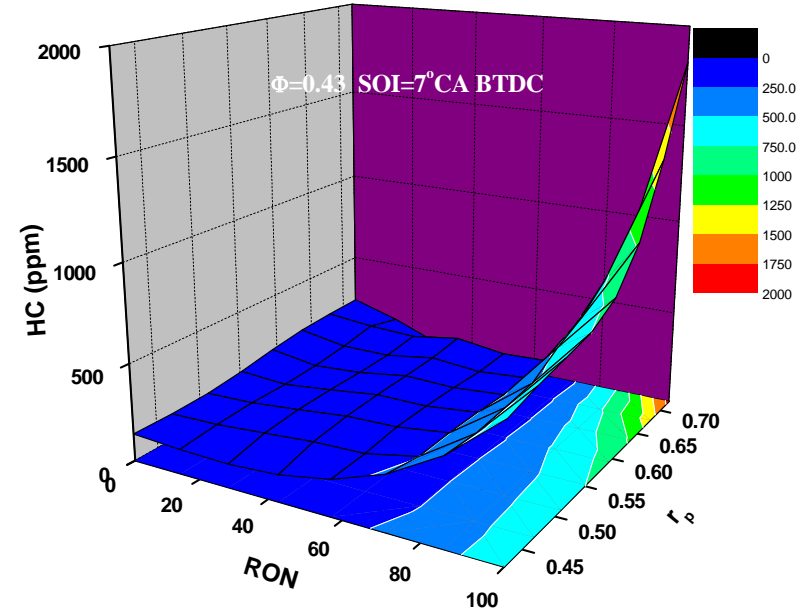
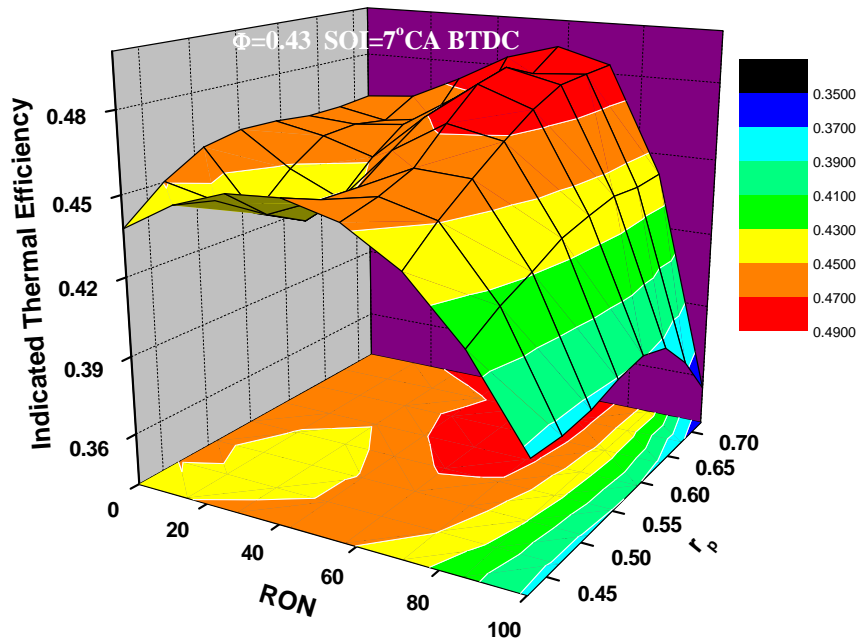
Effect of Fuel Octane Number of Port Injection on Indicated Thermal Efficiency



Port injection – variable octane number, Direct injection - n-heptane

The distributed heat release and combustion pattern determine engine thermal efficiency.

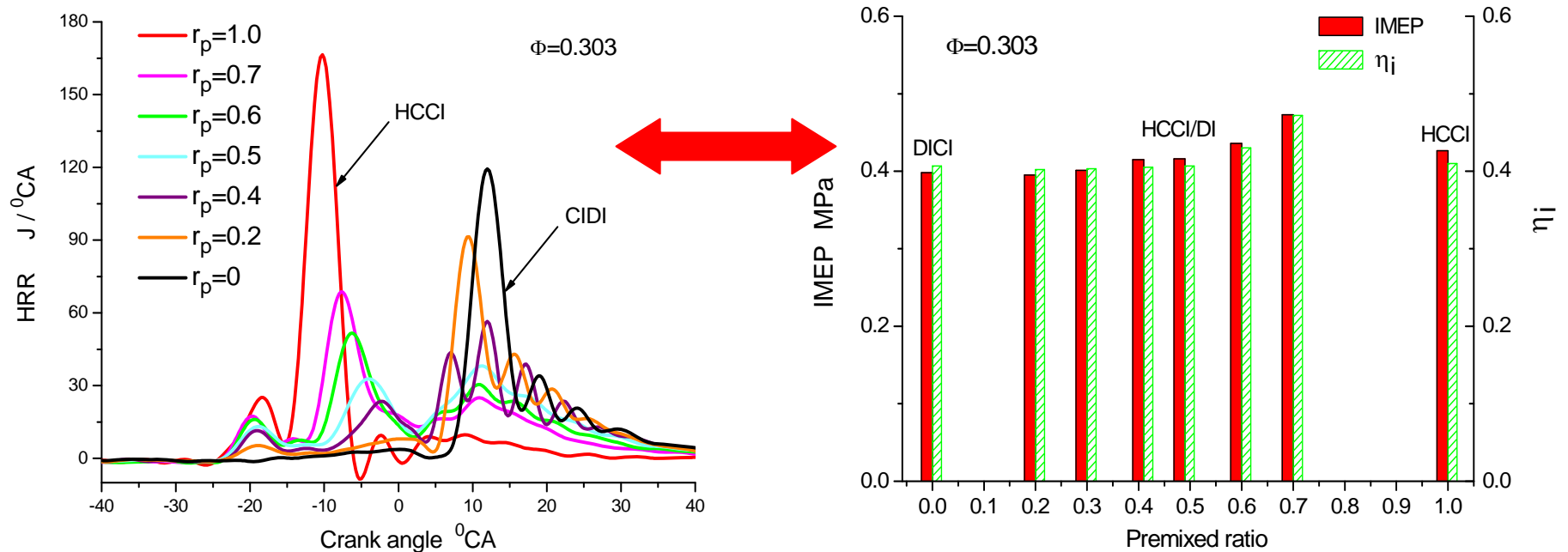
Effect of Fuel Octane Number of Port Injection on Indicated Thermal Efficiency and HC emission



Port injection – variable octane number, Direct injection - n-heptane

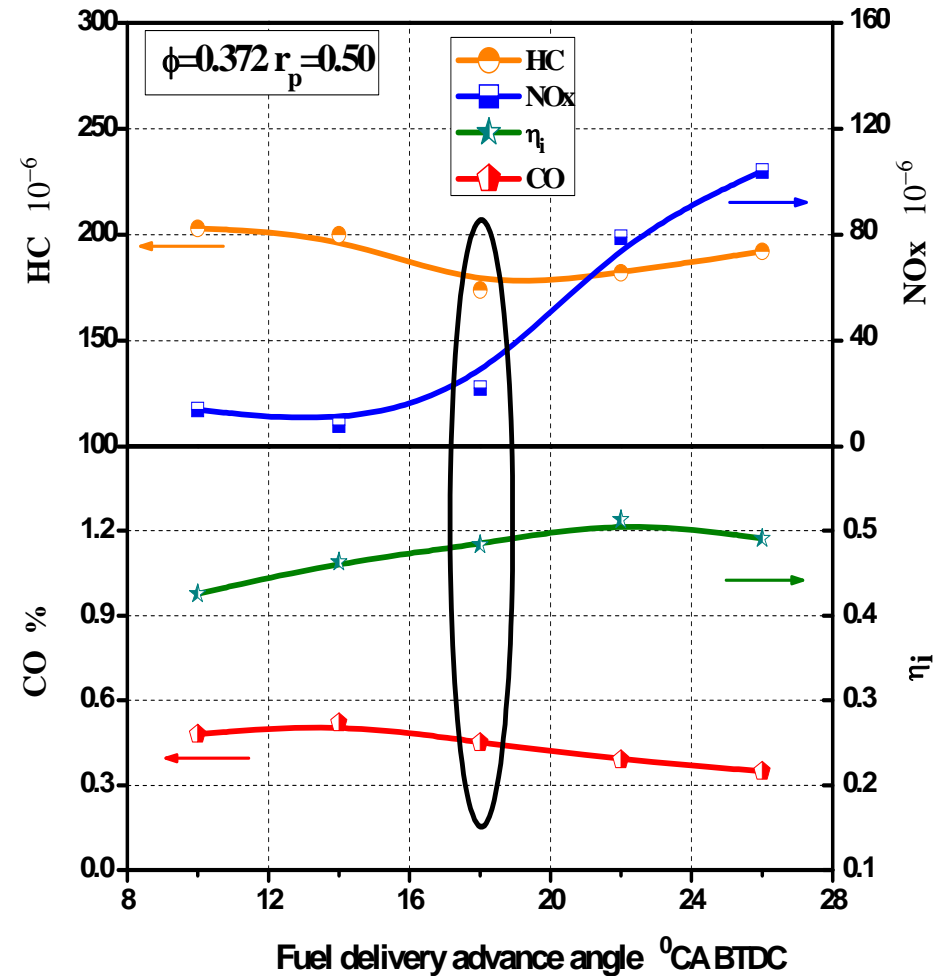
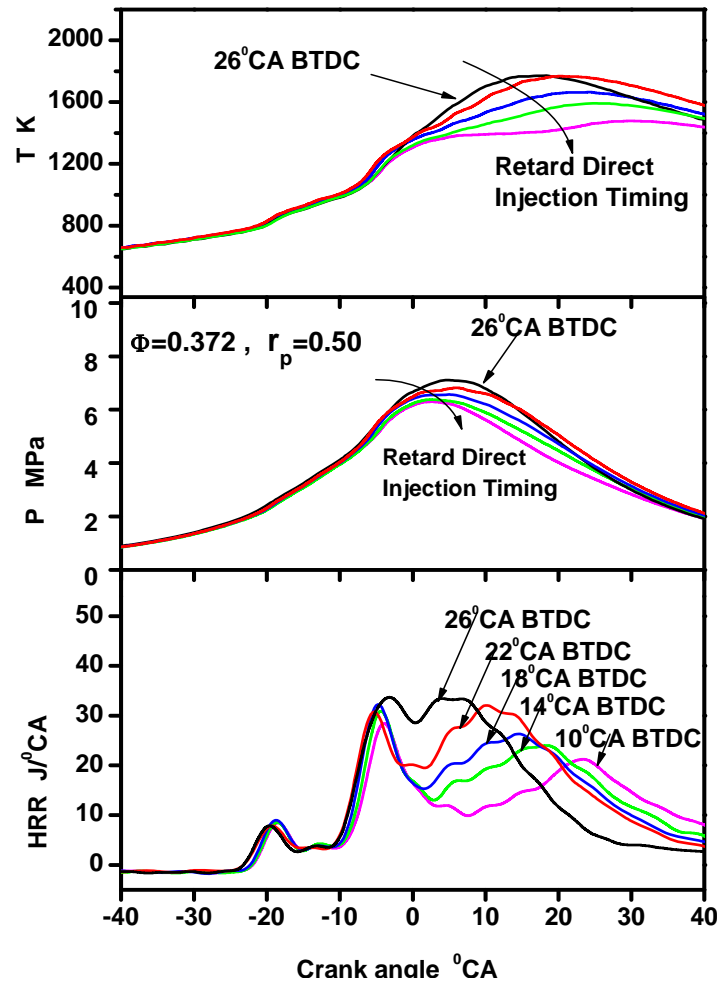
Fuel with RON 50 has highest indicated thermal efficiency and low HC emission

Effect of Premixed ratio on on Indicated Thermal Efficiency



Port injection - n-heptane, Direct injection - n-heptane

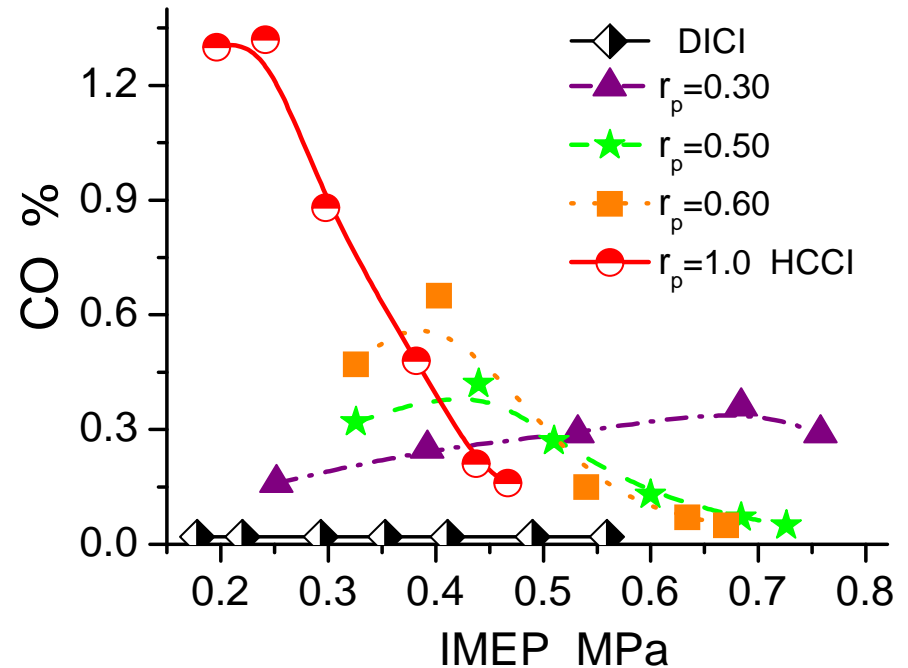
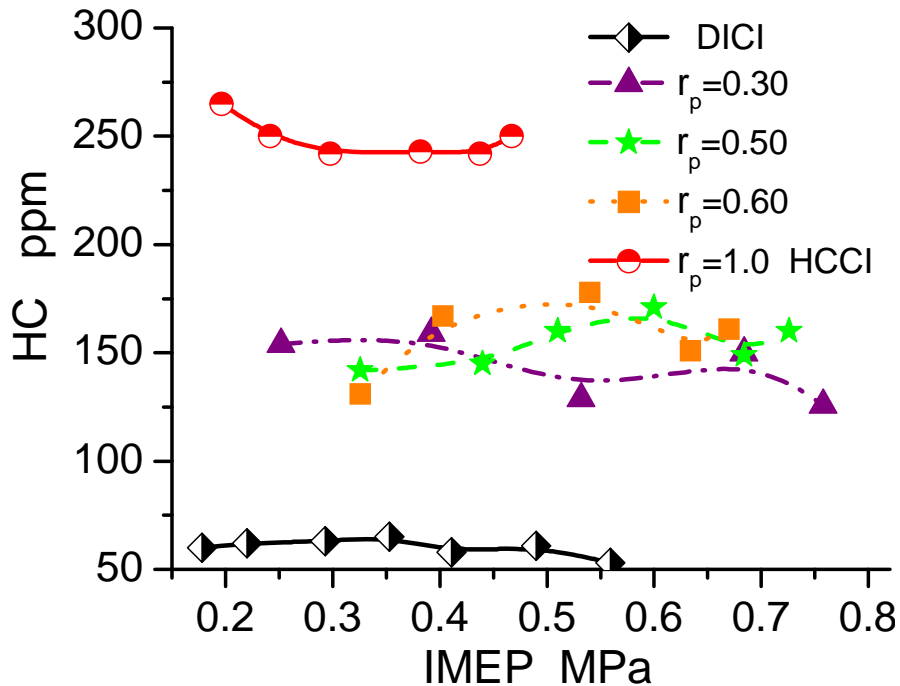
Effect of In Cylinder Direct Injection Timing on Indicated Thermal Efficiency and Exhaust Emissions



Port injection - n-heptane, Direct injection - n-heptane

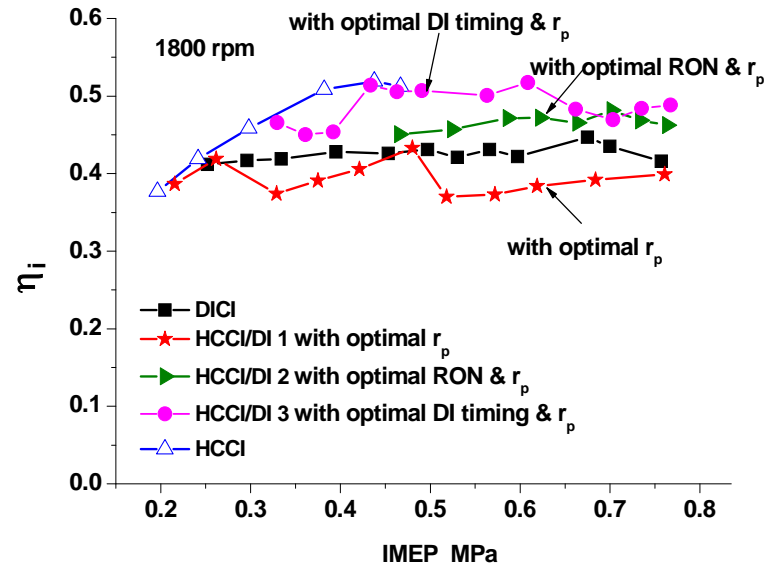
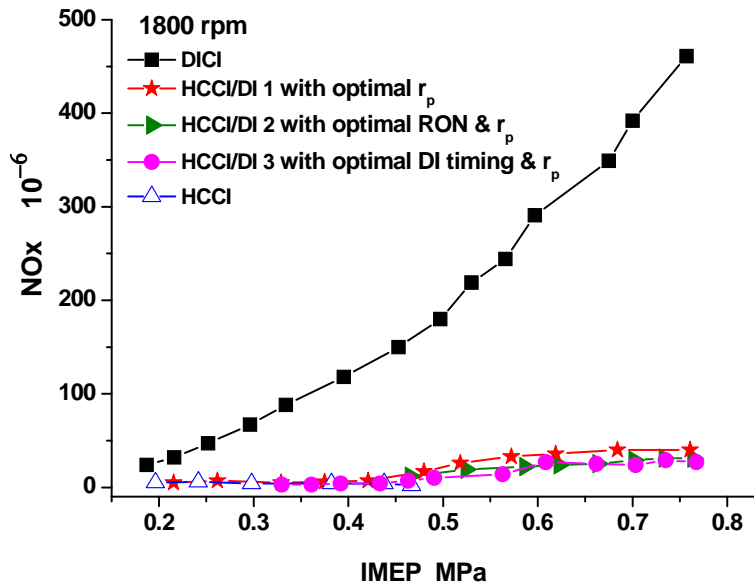
Comparison of HC and CO emissions among HCCI, PCCI and CIDI

Port injection - n-heptane, Direct injection - n-heptane



With optimization of premixed ratio, CO and HC emissions of PCCI is much lower than that of HCCI, is higher than that of CIDI.

Comparison of indicated thermal efficiency and NOx emission among HCCI, hybrid combustion and CIDI



	DICI	HCCI/DI 1	HCCI/DI 2	HCCI/DI 3	HCCI
Port Injection	N/A	n-heptane	RON	n-heptane	n-heptane
Direct Injection	Diesel	n-heptane	n-heptane	n-heptane	N/A

□ With optimization of premixed ratio, fuel octane number of port injection and direct injection timing, indicated thermal efficiency could be improved and NOx emission of engine could be decreased substantially, compared with CIDI. Engine could extend to fuel load with low NOx emission.

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1. Active Fuel Design for HCCI
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3. **Conclusions**

Conclusions

- By means of variable fuel properties and injection strategy, the active fuel design and management (AFDM) offers important advantages for load extension, thermal efficiency improvement and exhaust emission reduction for

1. For HCCI

- ❑ Ignition control
- ❑ Engine load extension
- ❑ CO and HC emission reduction
- ❑ Thermal efficiency improvement

3. For engine control

- ❑ Fast response
- ❑ Cycle to cycle control
- ❑ Closed-loop control

2. For hybrid combustion

- ❑ Ignition control
- ❑ Combustion phase control
- ❑ Full load operation
- ❑ Misfire and knocking avoidance
- ❑ Thermal efficiency improvement
- ❑ Low CO and HC, **Compared with HCCI**
- ❑ Low NOx, **Compared with CIDI**

Acknowledgements

- **This work was supported by the National Fundamental Research Program.**
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- ***Thank You!***

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